

Fusion Nuclear Technology Development and the Role of CTF toward DEMO

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Seminar at General Atomics

December 9, 2002

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Fusion Nuclear Technology (FNT)

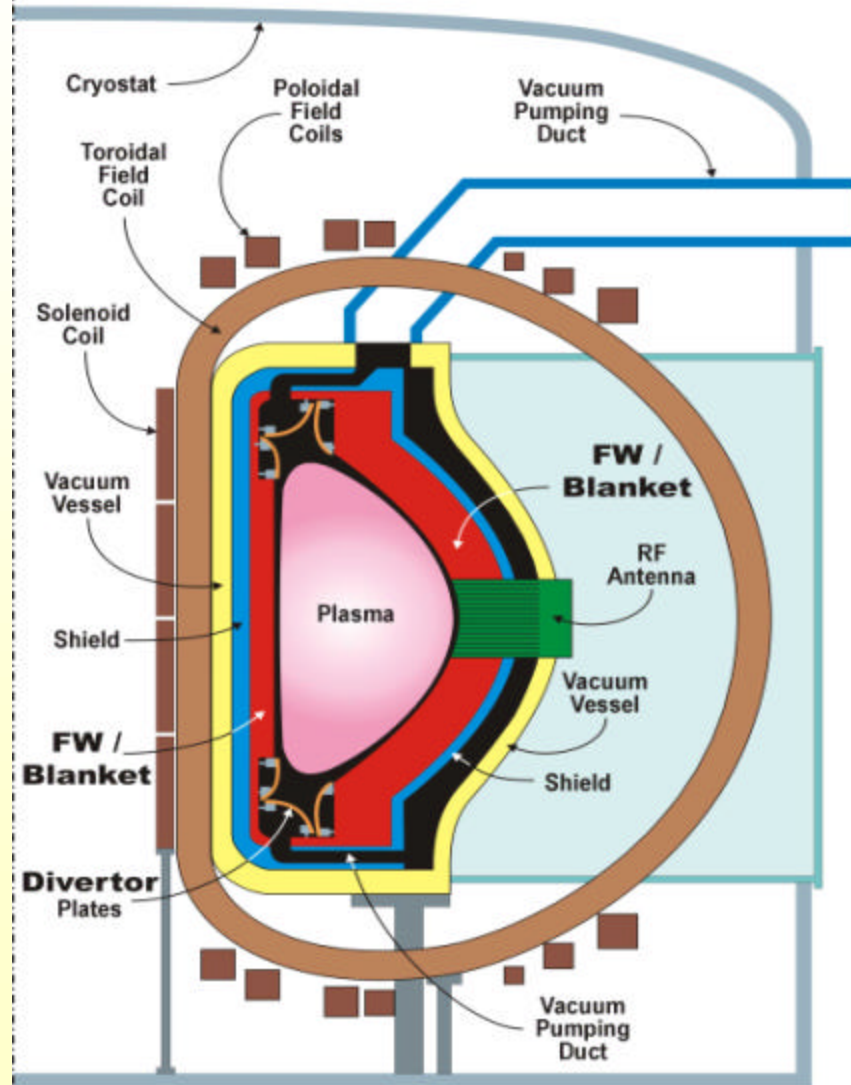
Fusion Power & Fuel Cycle Technology

FNT Components from the edge of the Plasma to TF Coils (Reactor “Core”)

1. Blanket Components
2. Plasma Interactive and High Heat Flux Components
 - a. divertor, limiter
 - b. rf antennas, launchers, wave guides, etc.
3. Vacuum Vessel & Shield Components

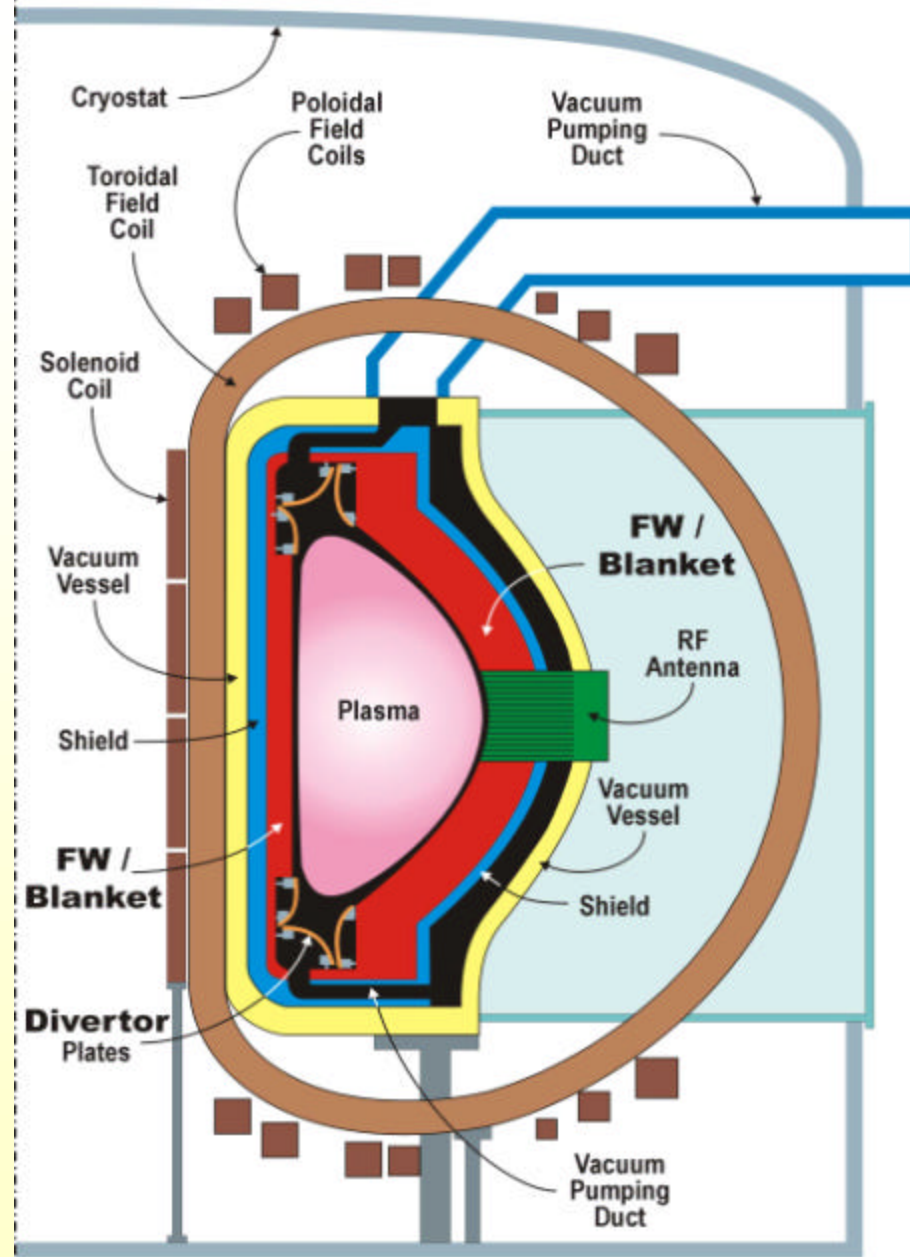
Other Components affected by the Nuclear Environment

4. Tritium Processing Systems
5. Instrumentation and Control Systems
6. Remote Maintenance Components
7. Heat Transport and Power Conversion Systems



Notes on FNT:

- The Vacuum Vessel is outside the Blanket (/Shield). It is in a low-radiation field.
- Vacuum Vessel Development for DEMO should be in good shape from ITER experience.
- The Key Issues are for Blanket / PFC.
- Note that the first wall is an **integral** part of the blanket (ideas for a separate first wall were discarded in the 1980's). The term "**Blanket**" now implicitly includes first wall.
- Since the Blanket is inside of the vacuum vessel, many failures (e.g. coolant leak from module) require immediate shutdown and repair/replacement.



Adaptation from ARIES-AT Design

Summary of Critical R&D Issues for Fusion Nuclear Technology

1. D-T fuel cycle **tritium self-sufficiency** in a practical system depends on many physics and engineering parameters / details: e.g. fractional burn-up in plasma, tritium inventories, FW thickness, penetrations, passive coils, etc.
2. **Tritium extraction and inventory** in the solid/liquid breeders under actual operating conditions
3. **Thermomechanical** loadings and response of blanket and PFC components under normal and off-normal operation
4. Materials **interactions and compatibility**
5. Identification and characterization of **failure modes, effects, and rates** in blankets and PFC's
6. Engineering feasibility and reliability of electric (MHD) **insulators** and **tritium permeation barriers** under thermal / mechanical / electrical / magnetic / nuclear loadings with high temperature and stress gradients
7. **Tritium permeation, control and inventory** in blanket and PFC
8. **Lifetime** of blanket, PFC, and other FNT components
9. **Remote maintenance** with acceptable machine shutdown time.

What is DEMO?

(Excerpts from FESAC Panel Interim Report)

The goal of the plan is operation of a US demonstration power plant (Demo), which will enable the commercialization of fusion energy.

The target date is about 35 years. Early in its operation the Demo will show net electric power production, and ultimately it will demonstrate the commercial practicality of fusion power. It is anticipated that several such fusion demonstration devices will be built around the world. In order for a future US fusion industry to be competitive, the US Demo must:

- a. be safe and environmentally attractive,
- b. extrapolate to competitive cost for electricity in the US market, as well as for other applications of fusion power such as hydrogen production,
- c. use the same physics and technology as the first generation of competitive commercial power plants to follow, and
- d. ultimately achieve availability of ~ 50%, and extrapolate to commercially practical levels.

R&D Tasks to be Accomplished Prior to Demo

1) Plasma

- Confinement/Burn
- Disruption Control
- Current Drive/Steady State
- Edge Control

2) Plasma Support Systems

- Superconducting Magnets
- Fueling
- Heating

3) Fusion Nuclear Technology Components and Materials

[Blanket, First Wall, High Performance Divertors, rf Launchers]

- Materials combination selection and configuration optimization
- Performance verification and concept validation
- Show that the fuel cycle can be closed (tritium self-sufficiency)
- Failure modes and effects
- Remote maintenance demonstration
- Reliability growth
- Component lifetime

4) Systems Integration

Where Will These Tasks be Done?!

- Burning Plasma Facility (ITER) and other plasma devices will address 1, 2, & much of 4
- Fusion Nuclear Technology (FNT) components and materials require dedicated fusion facility(ies) parallel to ITER (prior to DEMO)

International studies and experts have concluded that extensive testing of fusion nuclear components in FUSION testing facilities is **REQUIRED** prior to DEMO

- Non-fusion facilities cannot fully resolve any of the critical issues for blankets or PFC's
- There are critical issues for which no significant information can be obtained from testing in non-fusion facilities (An example is identification and characterization of failure modes, effects and rates)
- The Feasibility of Blanket/PFC Concepts can NOT be established prior to testing in fusion facilities**

Note: Non-fusion facilities can and should be used to narrow material and design concept options and to reduce the costs and risks of the more costly and complex tests in the fusion environment. Extensive R&D programs on non-fusion facilities should start now.

Key Fusion Environmental Conditions for Testing Fusion Nuclear Components

Neutrons (fluence, spectrum, spatial and temporal gradients)

- Radiation Effects
(at relevant temperatures, stresses, loading conditions)
- Bulk Heating
- Tritium Production
- Activation

Heat Sources (magnitude, gradient)

- Bulk (from neutrons)
- Surface

Particle Flux (energy and density, gradients)

Magnetic Field (3-component with gradients)

- Steady Field
- Time-Varying Field

Mechanical Forces

- Normal
- Off-Normal

Thermal/Chemical/Mechanical/Electrical/Magnetic Interactions

Synergistic Effects

- Combined environmental loading conditions
- Interactions among physical elements of components

FNT Requirements for Major Parameters for Testing in Fusion Facilities with Emphasis on Testing Needs to Construct DEMO Blanket

- These requirements have been extensively studied over the past 20 years, and they have been agreed to internationally (FINESSE, ITER Blanket Testing Working Group, IEA-VNS, etc.)
- Many Journal Papers have been published (>35)
- Below is the Table from the IEA-VNS Study Paper (Fusion Technology, Vol. 29, Jan 96)

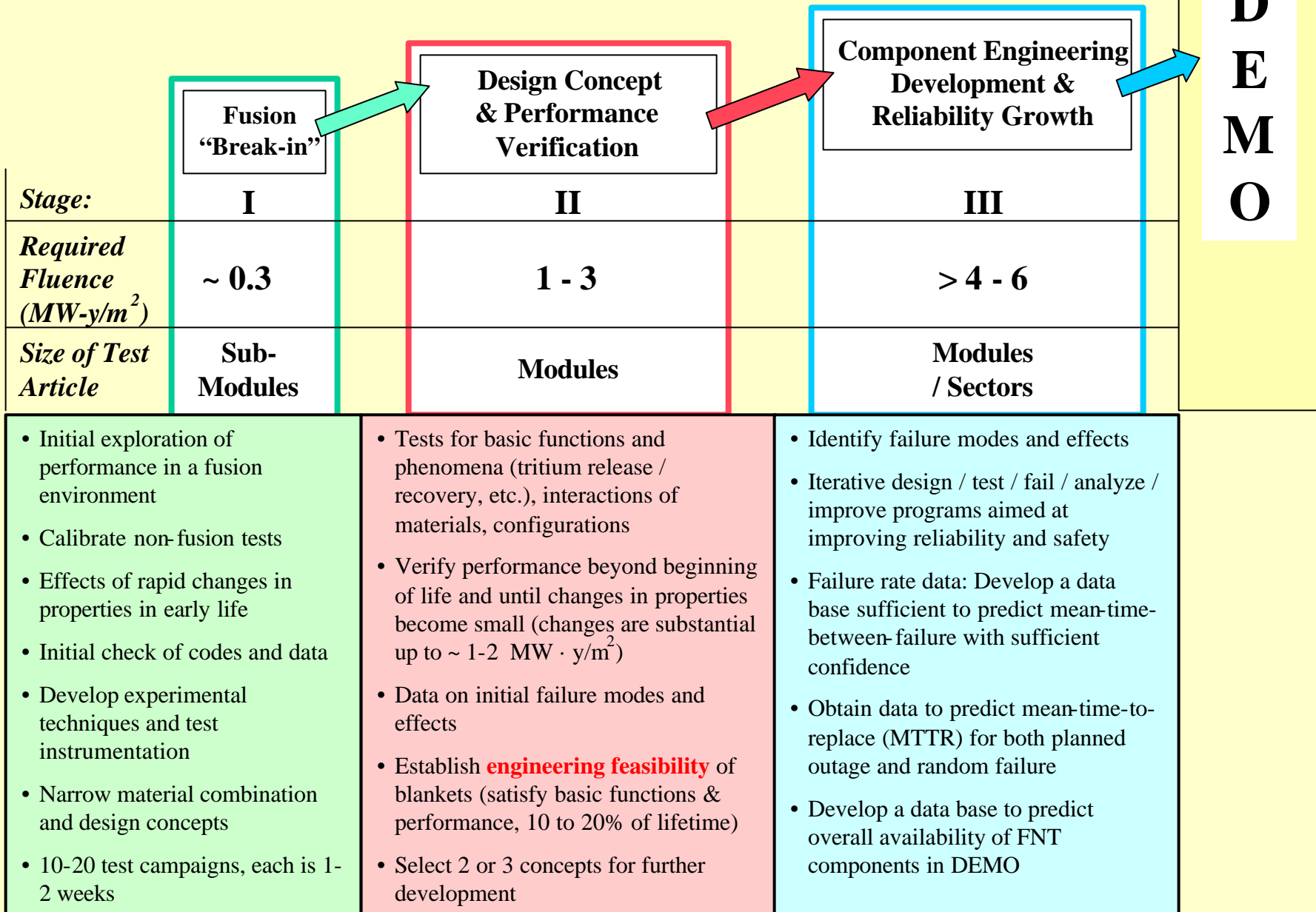
Parameter	Value
Neutron wall load ^a (MW/m ²)	1 to 2
Plasma mode of operation	Steady State ^b
Minimum COT (periods with 100% availability) (weeks)	1 to 2
Neutron fluence at test module (MW·y/m ²)	
Stage I: initial fusion break-in	0.3
Stage II: concept performance verification (engineering feasibility)	1 to 3
Stage III ^c : component engineering development and reliability growth	4 to 6 ^c
Total neutron fluence for test device (MW·y/m ²)	>6
Total test area (m ²)	>10
Total test volume (m ³)	>5
Magnetic field strength (T)	>4

a - Prototypical surface heat flux (exposure of first wall to plasma is critical)

b - If steady state is unattainable, the alternative is long plasma burn with plasma duty cycle >80%

c - Note that the fluence is not an accumulated fluence on “the same test article”; rather it is derived from testing “time” on “successive” test articles dictated by “reliability growth” requirements

Stages of FNT Testing in Fusion Facilities



Critical Factors in Deciding where to do Blanket / PFC / FNT Testing

- Tritium Consumption / Supply Issue
- Reliability / Maintainability / Availability Issue
- Cost
- Risk
- Schedule

Fundamental Considerations in Deciding where to do Blanket / PFC / FNT Fusion Testing

- The FNT Testing Requirements are
 - Fusion Power only 20-30 MW
 - Over about 10m² of surface area (with exposure to plasma)
 - With Steady State Plasma Operation (or plasma cycle >80%)
 - Testing Time on successive test articles equivalent to neutron fluence of 6 MW • y/m²
- **Tritium Consumption / Tritium Supply** issue dictates that any fusion facility that performs FNT testing must internally breed all (or most) of its own tritium
 - If TBR <1, Larger Power Devices require larger TBR
 - For a given TBR, the FW area required for breeding is much larger than for small devices
- FNT Testing involves **RISKS** to the fusion testing device
 - unvalidated technology with direct exposure to plasma
 - frequent failures are expected
 - considerable amounts of tritium and activated materials
 - These risks are much greater for large power devices because of the much larger area for tritium breeding
- Cost
 - Frequent failures will require frequent replacements: **COST** will be much higher for the larger power, larger area devices
 - **COST** of operation to higher fluence is larger for larger devices

What is CTF?

- The idea of CTF is to build a **small size, low fusion power** DT plasma-based device in which Fusion Nuclear Technology experiments can be performed in the relevant fusion environment at the smallest possible scale, cost, and risk.
 - In MFE: small-size, low fusion power can be obtained in a low-Q plasma device.
 - Equivalent in IFE: reduced target yield and smaller chamber radius
- This is a faster, much less expensive approach than testing in a large, ignited/high Q plasma device for which tritium consumption, and cost of operating to high fluence are very high (unaffordable!, not practical).

CTF MISSION is integrated testing and development of fusion power and fuel cycle technologies (FNT) in prototypical fusion power conditions

Scope of Testing in CTF

- **Information Obtained from Basic Device**
 - Divertor Operation
 - Heating and Current Drive Systems PFC
 - Partial to full breeding, high temperature blanket (staged operation and breeding)
 - Neutronics and Shielding
 - Tritium Fuel Cycle
- **Demonstration of Remote Maintenance Operations**
 - through frequent changeout of various test articles
 - through repairs and changeout on the basic device
- **Testing in Specialized Test Ports (and substantial FW coverage at later stages of operation)**
 - **Materials** Test Module
 - Material Properties Specimen matrix
 - **Blanket** Test Modules
 - Screening Tests
 - Performance Verification
 - Reliability Growth
 - **Divertor** Test Modules
 - Engineering Performance
 - Design Improvements and Advanced Divertor Testing
 - **Current Drive and Heating Launchers**
 - **Neutronics** Test Sector
 - **Safety Aspects** of the Test Program
 - **Tritium** Processing

Where to do Blanket/PFC/FNT Fusion Testing?

Options / Scenarios

1. ITER (FEAT)

- Not possible with current design

2. Modified ITER (Redesign to satisfy FNT Testing Parameters)

- Too expensive: as a minimum, think of \$5B difference between EDA and FEAT
- Issues of tritium consumption, risks

3. Defer to DEMO

- Unthinkable! (Unvalidated technology in DEMO?!)

4. Add Small Size, Small Power Device for FNT Testing (CTF)

- a – CTF parallel to ITER
- b – CTF delayed start relative to ITER

ITER-FEAT as designed can NOT perform meaningful testing of fusion nuclear components

- ITER (FEAT) has been designed as a burning plasma experiment
 - The changes in design from ITER-EDA to ITER-FEAT have made ITER not a suitable facility for FNT testing
- ITER-FEAT Parameters do not satisfy FNT testing requirements:
 - Neutron wall load: 0.55 MW/m^2 (compared to required $1\text{-}2 \text{ MW/m}^2$)
 - Neutron fluence: $0.1 \text{ MW}\cdot\text{y/m}^2$ (compared to required $>6 \text{ MW}\cdot\text{y/m}^2$)
 - Plasma duty cycle makes it impossible to adequately perform the FNT testing mission
 - FNT testing requires steady state (or at least plasma duty cycle $> 80\%$)
 - ITER-FEAT has short plasma burn (400S), long dwell time (1200S) resulting in a plasma duty cycle of 25%
 - The ITER-FEAT short burn/long dwell plasma cycle does **not** even enable **temperature equilibrium** in test modules, a fundamental requirement for many tests (most FNT tests are highly temperature dependent)

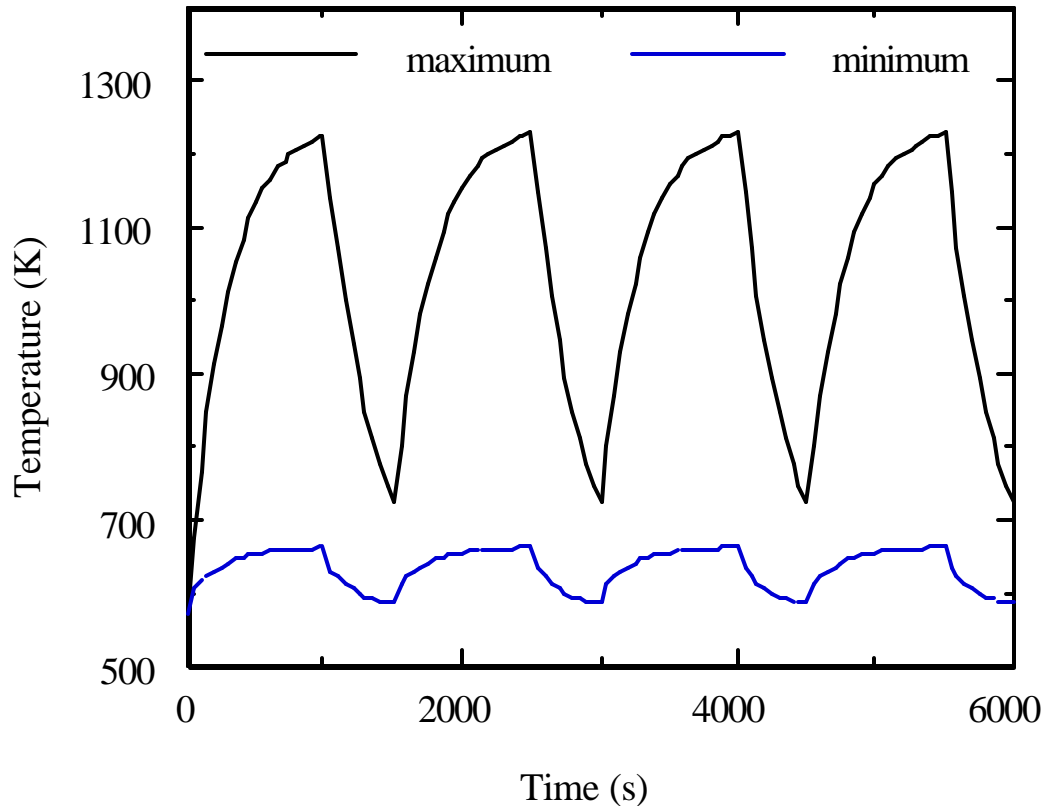
Mode of Plasma Operation in ITER-FEAT Rule Out Meaningful FNT Testing

- This issue was investigated extensively in several studies including the ITER Test Blanket Working Group in both ITER-CDA and ITER-EDA, IEA-VNS. The conclusion reached: need steady state (or if unattainable, long burn/short dwell with plasma duty cycle >80%).
- Extensive Investigation of Blanket Testing Requirements using detailed engineering scaling to preserve phenomena, etc. show that:
 - plasma burn time (t_b) > 3 τ_c
 - plasma dwell time (t_d) < 0.05 τ_c

Where τ_c is a characteristic time constant (for a given phenomena)

- Characteristic time constants for various responses/phenomena in the blanket range from a few seconds to a few hours (even days for some phenomena). See Tables in Appendix.
 - Thus the burn time needs to be hours and the dwell time needs to be a few seconds.
- Example of Difficulty: In ITER-FEAT scenario of 400 s burn and 1200 s dwell time, even temperature equilibrium can not be attained. Most critical phenomena in the blanket have strong temperature dependence. Tests for phenomena such as tritium release and recovery, failure modes, etc. can yield the wrong answer

Example of many calculations in the literature of the adverse effects of **low plasma cycle*** on the usefulness of FNT tests



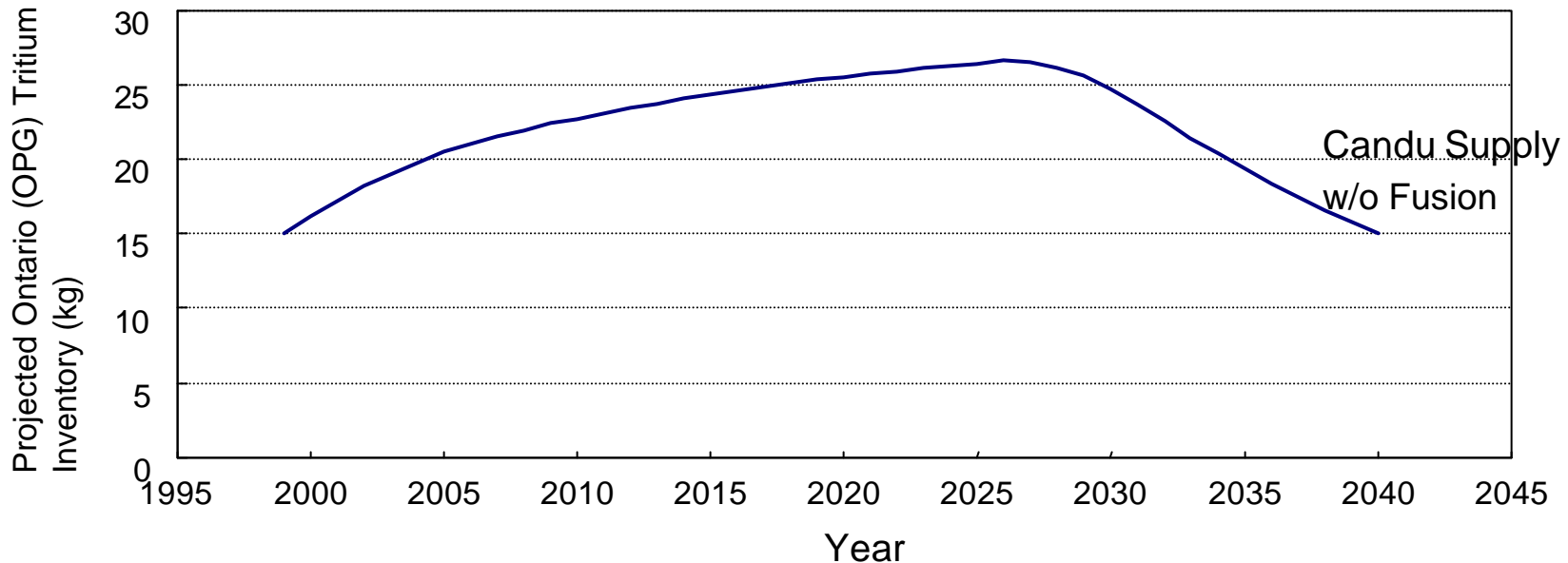
First unit cell breeder temperature response (burn time = 1000 s, dwell time = 500 s)

***Not long enough burn time and not short enough dwell time**

Tritium Consumption in Large and Small Power DT Devices
AND Tritium Supply Issue
AND Impact on the Path to FNT Development

Note: Projections of world tritium supply available to fusion for various scenarios were generated by Scott Willms, including information from Paul Rutherford's 1998 memo on "Tritium Window", and input from M. Abdou and D. Sze.

Projections for World Tritium Supply Potentially Available to Fusion



- World Maximum Tritium Supply (mainly CANDU) available for fusion is **27 kg**
- Tritium Consumption in a DT facility burns tritium at a rate of **55.8 kg/yr per 1000 MW of fusion power**
- Tritium decays at a rate of 5.47% yr
- Current Tritium cost is \$30 million/kg
- Once the Canadian Tritium is gone, **additional** tritium may be produced at a projected cost of **\$200 million/kg** (estimate by Anderson, Wittenberg, Willms, & Sze)

Conclusion

A large power DT facility must breed its own tritium

Separate Devices for Burning Plasma and FNT Development, i.e. ITER (FEAT) + CTF is more **Cost Effective** and **Faster** than a Single Combined Device

(to change ITER design to satisfy FNT testing requirements is very expensive and not practical)

	NWL	Fusion Power	Fluence (MW·y/m ²)	Tritium Consumption (TBR = 0)	Tritium Consumption (TBR = 0.6)
<u>Two Device Scenario</u>					
1) Burning Plasma (ITER)	0.55	500 MW	0.1	5 kg	2 kg
2) FNT Testing (CTF)	>1	< 100 MW	> 6	33 kg	13 kg
<u>Single Device Scenario</u> (Combined Burning Plasma + FNT Testing), i.e. ITER with major modifications (double the capital cost)					
	>1	910 MW	>6	>305 kg	>122 kg

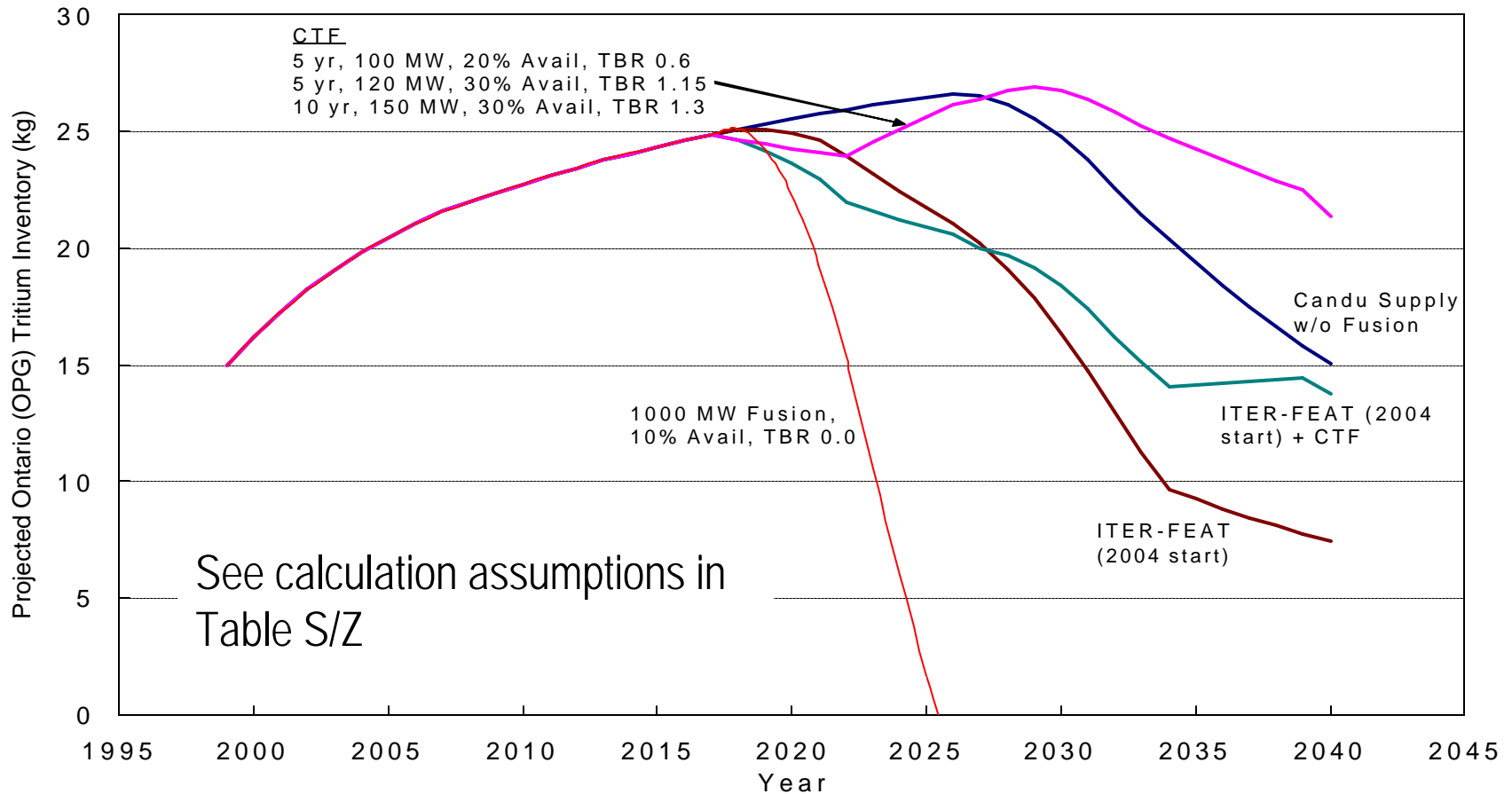
FACTS

- World Maximum Tritium Supply (mainly CANDU) available for Fusion is 27 kg
- Tritium decays at 5.47% per year
- Tritium cost now is \$30M / kg. More tritium will cost \$200M / kg.

Conclusion:

- **There is no external tritium supply to do FNT testing development in a large power DT fusion device. FNT development must be in a small fusion power device.**

Projections for World Tritium Supply Available to Fusion for Various Scenarios (Willms, et al)



- World Tritium Supply would be Exhausted by 2025 if ITER were to run at 1000 MW fusion power with 10% availability
- Large Power DT Fusion Devices are not practical for blanket/PFC development.
- We need 5-10 kg of tritium as “start-up” inventory for DEMO (can be provided from CTF operating with TBR > 1 at later stage of operation)
- Blanket/PFC must be developed prior to DEMO (and we cannot wait very long for blanket/PFC development even if we want to delay DEMO).

Table S/Z

(data used in Fig. for Tritium Supply and Consumption Calculations)

Tritium Supply Calculation Assumptions:

- Ontario Power Generation (OPG) has seven of twenty CANDU reactors idled
- Reactors licensed for 40 years
- 15 kg tritium in 1999
- 1999 tritium recovery rate was 2.1 kg/yr
- Tritium recovery rate will decrease to 1.7 kg/yr in 2005 and remain at this level until 2025
- After 2025 reactors will reach their end-of-life and the tritium recovery rate will decrease rapidly
- OPG sells 0.1 kg/yr to non-ITER/VNS users
- Tritium decays at 5.47 % / yr

It is assumed that the following will NOT happen:

- Extending CANDU lifetime to 60 years
- Restarting idle CANDU's
- Processing moderator from non-OPG CANDU's (Quebec, New Brunswick)
- Building more CANDU's
- Irradiating Li targets in commercial reactors (including CANDU's)
- Obtaining tritium from weapons programs of "nuclear superpowers"
- Premature shutdown of CANDU reactors

Table S/Z (cont'd)

(data used in Fig. for Tritium Supply and Consumption Calculations cont'd)

ITER-FEAT Assumptions:


- Construction starts in 2004 and lasts 10 years
- There are four years of non-tritium operation
- This is followed by 16 years of tritium operation. The first five years use tritium at a linearly increasing rate reaching 1.08 kg T used per year in the fifth year. Tritium usage remains at this level for the remainder of tritium operations.
- There is no tritium breeding (TBR=0)
- There is no additional tritium needed to fill materials and systems

CTF Assumptions:

- Begins burning tritium in 2017
- 5 yr, 100 MW, 20% availability, TBR 0.6
- 5 yr, 120 MW, 30% availability, TBR 1.15
- 10 yr, 150 MW, 30% availability, TBR 1.3

Reliability / Maintainability / Availability Critical Development Issues

$$Unavailability = U(total) = U(scheduled) + U(unscheduled)$$

 This you design for

 This can kill your DEMO and your future

Scheduled Outage:

Planned outage (e.g. scheduled maintenance of components, scheduled replacement of components, e.g. first wall at the end of life, etc.).

This tends to be manageable because you can plan scheduled maintenance / replacement operations to occur simultaneously in the same time period.

Unscheduled Outage: (This is a very challenging problem)

Failures do occur in any engineering system. Since they are random they tend to have the most serious impact on availability.

This is why “reliability/availability analysis,” reliability testing, and “reliability growth” programs are key elements in any engineering development.

Availability (Due to Unscheduled Events)

$$\text{Availability:} = \frac{1}{1 + \sum_i \text{Outage Risk}_i} \quad \text{i represents a component}$$

$$\text{(Outage Risk)}_i = (\text{failure rate})_i \cdot (\text{mean time to repair})_i = \frac{\text{MTTR}_i}{\text{MTBF}_i}$$

MTBF = mean time between failures = 1/failure rate

MTTR = mean time to repair

- **A Practical Engineering System must have:**

1. **Long MTBF:** have sufficient reliability

- MTBF depends on reliability of components.

One can estimate what MTBF is NEEDED from “availability allocation models” for a given availability goal and for given (assumed) MTTR.

But predicting what MTBF is ACHIEVEABLE requires real data from integrated tests in the fusion environment.

2. **Short MTTR:** be able to recover from failure in a short time

- MTTR depends on the complexity and characteristics of the system (e.g. confinement configurations, component blanket design and configuration, nature of failure). Can estimate, but **need to demonstrate MTTR in fusion test facility.**

An Example Illustration of Achieving a Demo Availability of 49%

(Table based on information from J. Sheffield's memo to the Dev Path Panel)

Component	Num ber	Failure rate in hr⁻¹	MTBF in years	MTTR for Major failure, hr	MTTR for Minor failure, hr	Fraction of failures that are Major	Outage Risk	Component Availability
Toroidal Coils	16	5×10^{-6}	23	10^4	240	0.1	0.098	0.91
Poloidal Coils	8	5×10^{-6}	23	5×10^3	240	0.1	0.025	0.97
Magnet supplies	4	1×10^{-4}	1.14	72	10	0.1	0.007	0.99
Cryogenics	2	2×10^{-4}	0.57	300	24	0.1	0.022	0.978
Blanket	100	1×10^{-5}	11.4	800	100	0.05	0.135	0.881
Divertor	32	2×10^{-5}	5.7	500	200	0.1	0.147	0.871
Htg/CD	4	2×10^{-4}	0.57	500	20	0.3	0.131	0.884
Fueling	1	3×10^{-5}	3.8	72	--	1.0	0.002	0.998
Tritium System	1	1×10^{-4}	1.14	180	24	0.1	0.005	0.995
Vacuum	3	5×10^{-5}	2.28	72	6	0.1	0.002	0.998
Conventional equipment- instrumentation, cooling, turbines, electrical plant ---							0.05	0.952
TOTAL SYSTEM							0.624	0.615

Assuming 0.2 as a fraction of year scheduled for regular maintenance.

Availability = $0.8 * [1/(1+0.624)] = 0.49$

Reliability/Availability is a challenge to fusion, particularly blanket/PFC, development

- Fusion System has **many major components** (TFC, PFC, plasma heating, vacuum vessel, blanket, divertor, tritium system, fueling, etc.)
 - Each component is required to have high availability
- All systems except the reactor core (blanket/PFC) will have reliability data from ITER and other facilities
- There is NO data for blanket/PFC (we do not even know if any present blanket concept is feasible)
- Estimates using available data from fission and aerospace for unit failure rates and using the surface area of a tokamak show:

PROBABLE MTBF for Blanket ~ 0.01 to 0.2 yr
compared to REQUIRED MTBF of many years

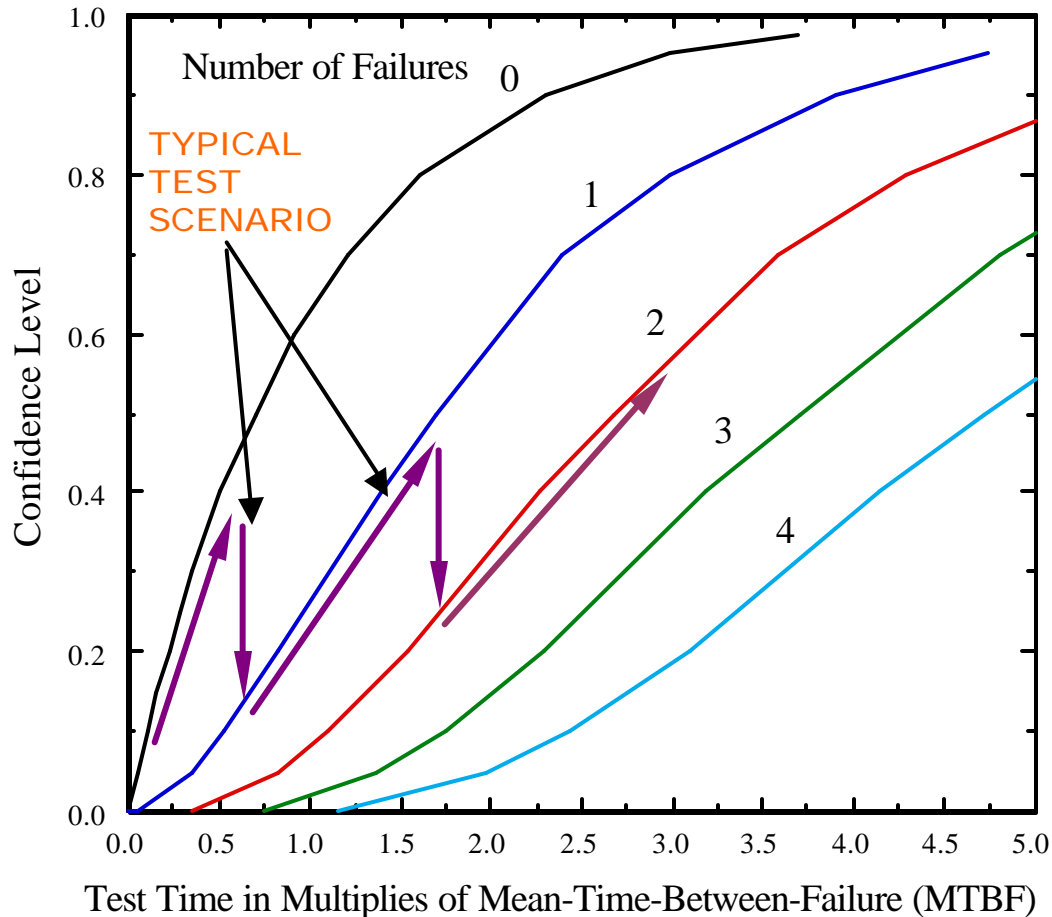
Aggressive “Reliability Growth” Program

We must have an aggressive “reliability growth” program for the blanket / PFC (beyond demonstrating engineering feasibility)

- 1) All new technologies go through a reliability growth program
- 2) Must be “aggressive” because extrapolation from other technologies (e.g. fission) strongly indicates we have a serious CHALLENGE

"Reliability Growth"

Upper statistical confidence level as a function of test time in multiples of MTBF for time terminated reliability tests (Poisson distribution). Results are given for different numbers of failures.

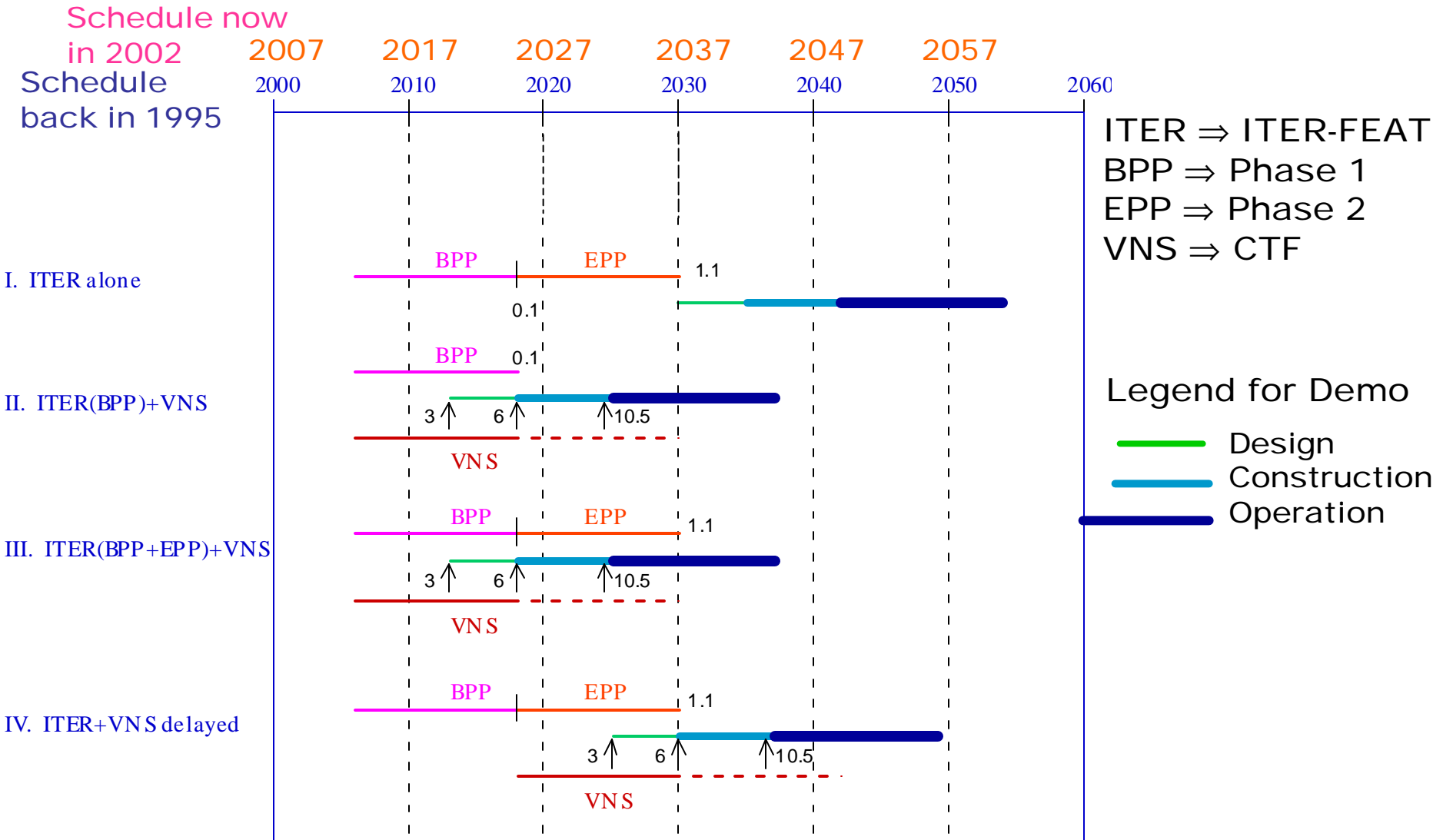


Example,

To get 80% confidence in achieving a particular value for MTBF, the total test time needed is about 3 MTBF (for case with only one failure occurring during the test).

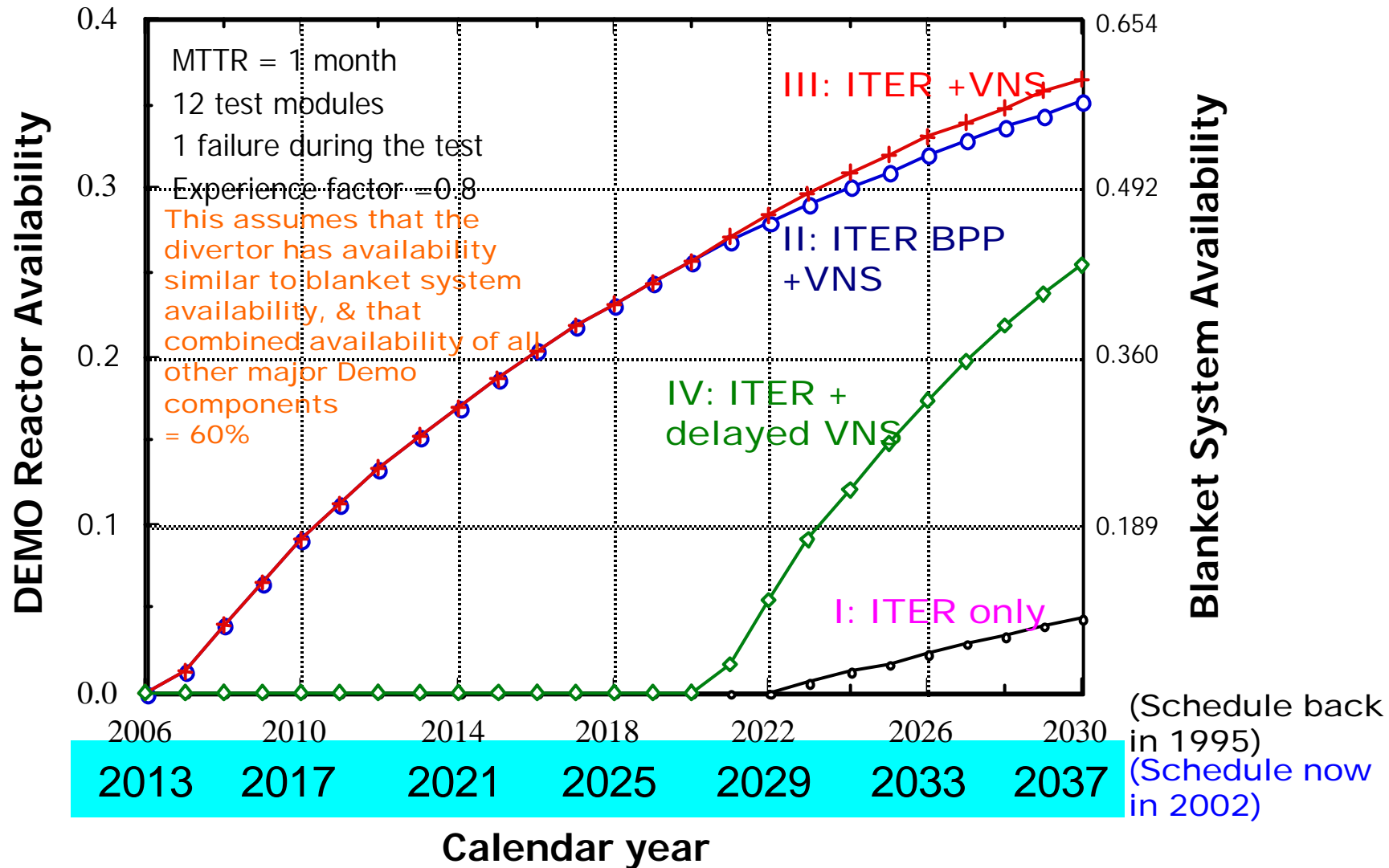
Reference: M. Abdou et. al., "FINESSE A Study of the Issues, Experiments and Facilities for Fusion Nuclear Technology Research & Development, Chapter 15 (Figure 15.2-2.) Reliability Development Testing Impact on Fusion Reactor Availability", Interim Report, Vol. IV, PPG-821, UCLA, 1984. It originated from A. Coppola, "Bayesian Reliability Tests are Practical", RADC-TR-81-106, July 1981.

Scenarios for major fusion devices leading to a DEMO



Numbers refer to Fluence values in MW·y/m²

DEMO reactor availability obtainable with 80% confidence for different testing scenarios, MTTR = 1 month



Note: ITER in Scenarios I, III and IV assumes fluence of 1.1 MW.y/m² (ITER-FEAT 1st phase has 0.1 MW.y/m²)

Conclusions on Blanket and PFC Reliability Growth

- Blanket and PFC tests in **ITER alone** cannot demonstrate DEMO availability higher than **4%**

(This also assumes ITER would be modified to a higher wall load and to operate with steady state plasma)

- Blanket and PFC testing in VNS (**CTF**) allows DEMO blanket system and PFC system availability of $> 50\%$, corresponding to DEMO availability $> 30\%$

Note that testing time required to improve reliability becomes even longer at higher availability [e.g. testing time required to increase availability from 30% to 50% is much longer than that needed to improve availability to 30%]

Recommendations on Availability/Reliability Growth Strategy and Goals

- Set availability goal for initial operation of DEMO of $\sim 30\%$ (i.e. defer some risk)
 - Operate CTF and ITER in parallel, together with other facilities, as aggressively as possible
 - Realize that there is a serious decision point with serious consequences based on results from ITER and CTF
 - If results are positive proceed with DEMO
 - If not, then we have to go back to the drawing board

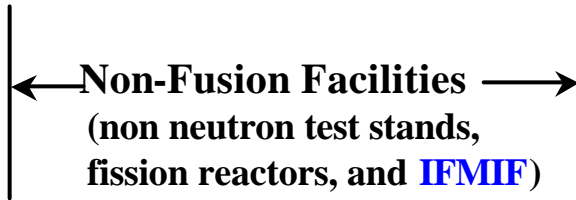
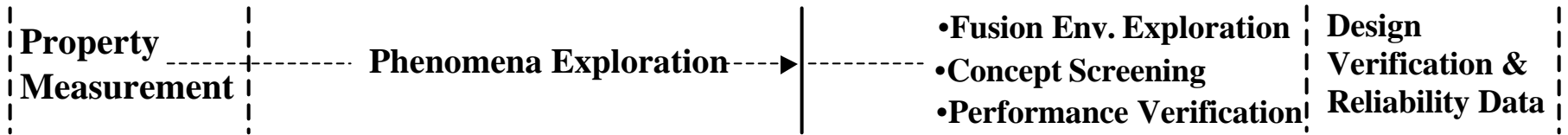
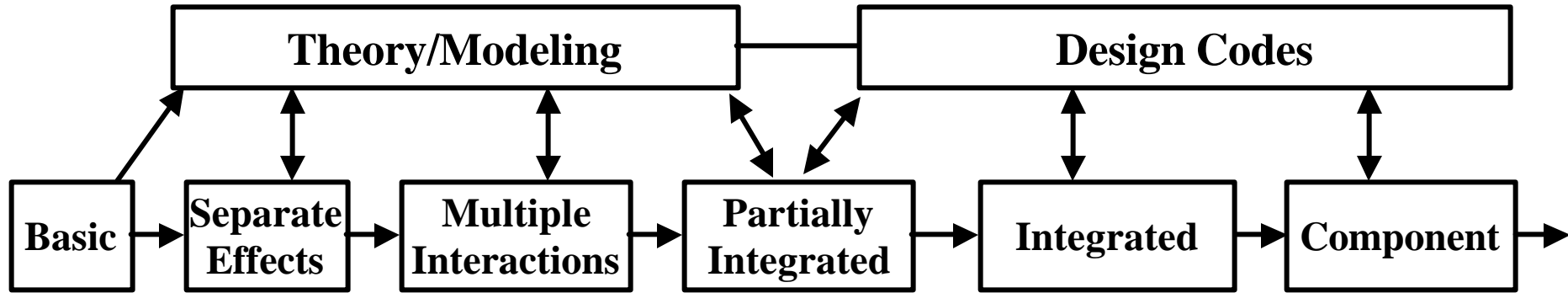
How About Reliability/Availability of CTF itself?

- CTF needs to be designed as an experimental, flexible, and maintainable facility
- Must plan an aggressive “Availability Growth” program:
 - improve maintainability
 - “reliability growth” through strategy of test/fail/analyze/fix/improve
 - for both test modules and the device itself
- Is it a Challenge?
 - **Definitely! But, if we do not succeed in CTF in obtaining 25% - 30% availability, how can we succeed in DEMO without CTF?**
 - Blanket/PFC development for DT fusion has high risks. It is more prudent, less costly, and faster to take these risks with smaller, less expensive devices than with large expensive devices
 - To put an “untested, unvalidated” breeding blanket on DEMO has unacceptably high risks, high costs (Impossible?!). Besides, how would you call that a DEMO? You should call it CTF.

Role of IFMIF

- IFMIF is a D-Li accelerator-based neutron source for “single effect” tests in a very small volume
 - It is not a fusion facility
 - Its role should not be confused with that of fusion test facilities. (It is a complementary facility)
- IFMIF will provide data on “radiation damage” effects on “basic properties” of structural materials in “miniaturized specimens” (typically mm scale)
- IFMIF cannot do materials interactions and blanket/PFC tests because of
 - Small volume (0.5 litre at about $2\text{MW}/\text{m}^2$)
 - Lack of key fusion environmental conditions (see earlier slide: surface heat flux, particle flux bulk heating, tritium production, steady and time-varying magnetic fields, neutron flux gradients, temperature gradients, stress gradients, synergistic effects, etc.)

Types and roles of experiments, facilities and modeling for FNT



- Non fusion facilities (e.g. fission reactors and IFMIF) have useful but limited roles
- Fusion testing facilities (e.g. CTF) are NECESSARY for multiple interactions, partially integrated, integrated, and component tests

Role of IFMIF (continued)

- The reason IFMIF was conceived back in the 70's (as FMIT) was the desire to obtain “accelerated” testing on radiation effects in specimens of structural materials as a key factor in projecting the “lifetime” of the first wall in DEMO and power reactors

Accelerated testing was ASSUMED because:

- 1 - Accelerators can provide high availability ~70% while fusion testing facilities will take longer to achieve high availability

Still True

- 2 - It was thought that very high fluxes ($>10 \text{ MW/m}^2$) can be realized in reasonably large volume at moderate cost ($<\$200\text{M}$)

No Longer True

- IFMIF can realize only $\sim 2 \text{ MW/m}^2$ in 500cm^3 (0.5 litre) at a cost approaching one billion dollars
- So, tests are not accelerated relative to DEMO ($3\text{-}5 \text{ MW/m}^2$), the volume is small, and the cost is high

Lesson from IFMIF experience

- IFMIF and Fusion Test Facilities should not be compared. They serve different roles. This exercise here is only for instructional purposes.
- Neutron Source Intensity in IFMIF is $\sim 1.1 \times 10^{17} \text{ n/s}$ (4π but only a fraction for tests)
(2 MW/m^2 on 100 cm^2)
at a cost of $\sim \$1\text{B}$ but availability is 70%
- Neutron Source Intensity in CTF is $\sim 7 \times 10^{19} \text{ n/s}$
(2 MW/m^2 on 75 m^2)
at a cost of $\sim \$2\text{B}$, but availability is $\sim 25\%$?
- The cost per neutron for tests in IFMIF is 7000 times higher than in a fusion test facility
 - In addition, a fusion facility has many other critical environment conditions (surface heat and particle flux, magnetic field, etc.) not available in IFMIF
- Lesson: the cost the fusion program is paying for R&D is substantially higher because the availability of near-term fusion devices is not high. (We also have to pay for accelerator technology R&D not on the path to fusion.)


The Fusion Program must have an aggressive “availability growth” program because: 1- it is needed for testing and development in the fusion environment, 2- it lowers the cost of fusion development, and 3- Necessary Goal for DEMO and beyond


Testing in a Fusion Facility is the **fastest** approach to Blanket and Fusion Development to Demo

A fusion test facility allows **SIMULTANEOUS** testing of integrated (synergistic) effects, multiple effects, and single effects

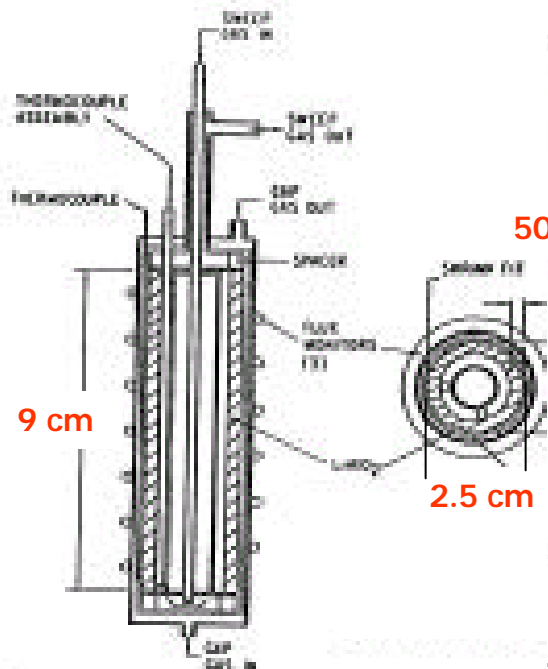
- Allows understanding through single and multiple effects tests under same conditions
- Provides "direct" answer for synergistic effects

Tension fracture toughness  Specimen (thousands)

Tension crack growth 

Charpy / dynamic fracture toughness 

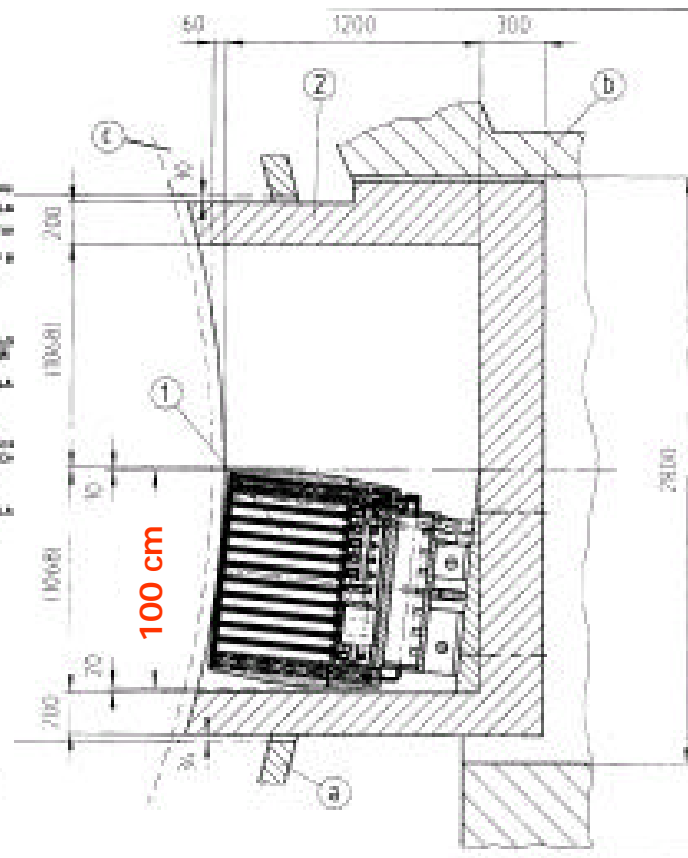
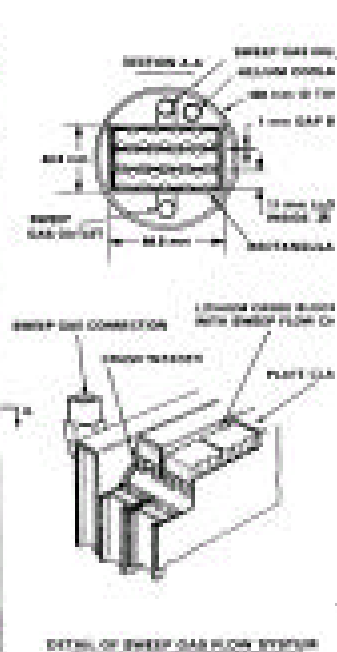
1 cm



50 cm

10.8 cm

Submodule (>100)



Blanket Test Module Frame
a. Back Plate
b. Vacuum Vessel
c. Shield Blanket

Test Module (>30)

• Also Test Sectors (several)

Capsule test (100's)
* Figures are not to scale. Note Dimensions

Issues yet to be resolved for IFMIF

- There are several issues that need to be addressed fully in the engineering R&D and design phase of IFMIF
 - 1 - Some Issues Related to Accelerator
 - 2 - Neutron Spectrum Issues
 - The neutron spectrum from the D-Li IFMIF source extends to 50 MeV (not a D-T fusion spectrum)
 - About 70% to 80% of the helium and hydrogen production rates come from neutrons above 15 MeV
 - About 30% to 40% of dpa comes from neutrons above 15 MeV
 - It is argued that the He/dpa ratio is close enough
 - However, the key problem is that nuclear data above 15 MeV is highly uncertain. There are no good measurements of cross sections and secondary particle spectra and no adequate neutron sources to do such measurements. Data generated by “nuclear models” are being used in IFMIF predictions.

However, it is known that these models fail for “weak reaction channels” such as (n,alpha)
 - These and other issues related to neutron spectrum in IFMIF need to be assessed in more detail by nuclear data and neutronics experts

Issues yet to be resolved for IFMIF (cont'd)

- 3 - Evaluation of Transmutations and their Effects
- 4 - Effect of the Steep Flux Gradients
- 5 - Ability to determine (or measure) the radiation damage indicators (flux, He production rate, etc.) in the specific specimen (to correlate observed effects with irradiation conditions) in IFMIF test cell.

Component Technology Facility (CTF)

MISSION

The mission of CTF is to test, develop, and qualify Fusion Nuclear Technology Components (fusion power and fuel cycle technologies) in prototypical fusion power conditions.

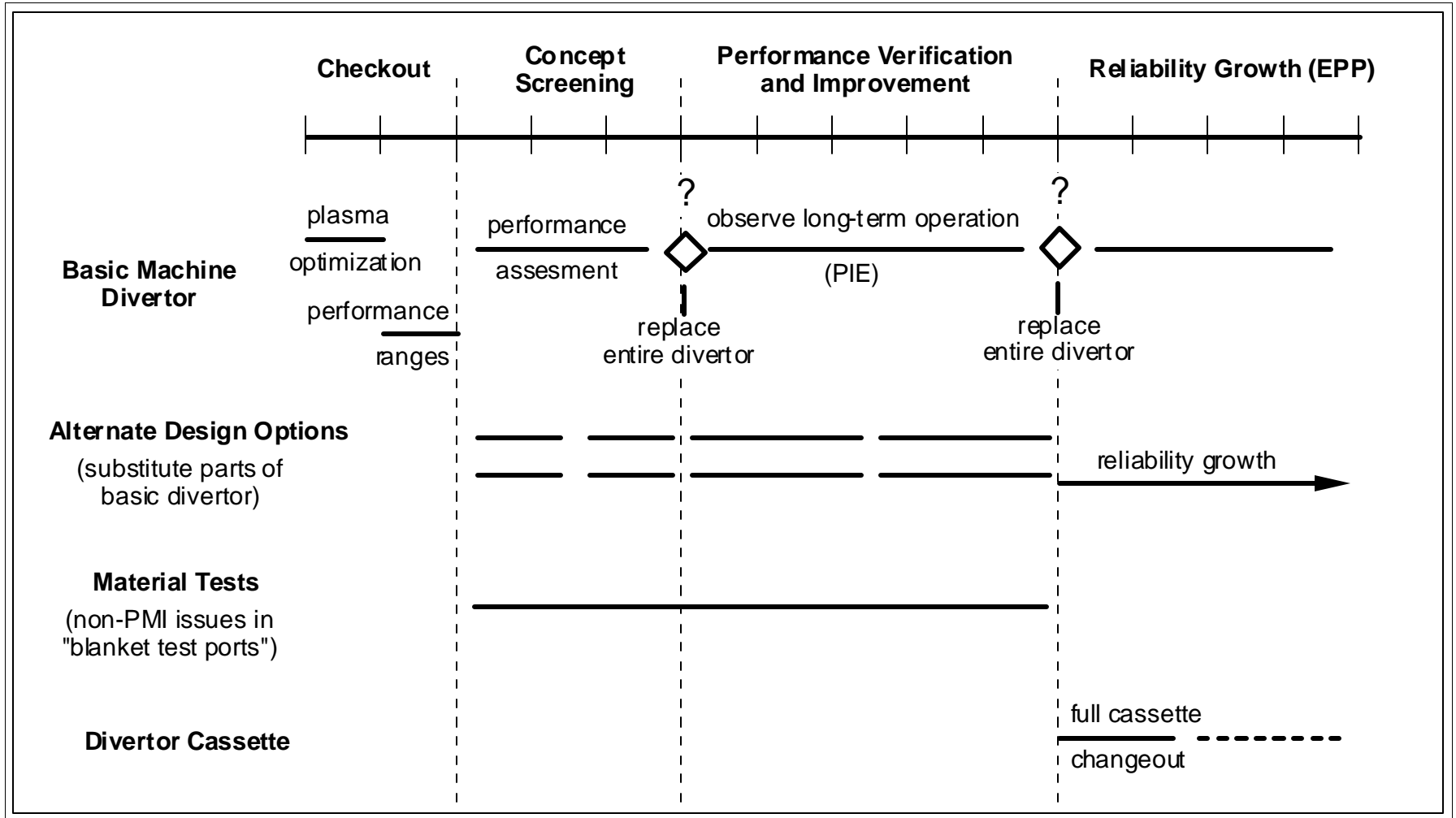
The CTF facility will provide the necessary integrated testing environment of high neutron and surface fluxes, steady state plasma (or long pulse with short dwell time), electromagnetic fields, large test area and volume, and high neutron fluence.

The testing program and CTF operation will demonstrate the engineering feasibility, provide data on reliability / maintainability / availability, and enable a “reliability growth” development program sufficient to design, construct, and operate blankets, plasma facing and other FNT components for DEMO.

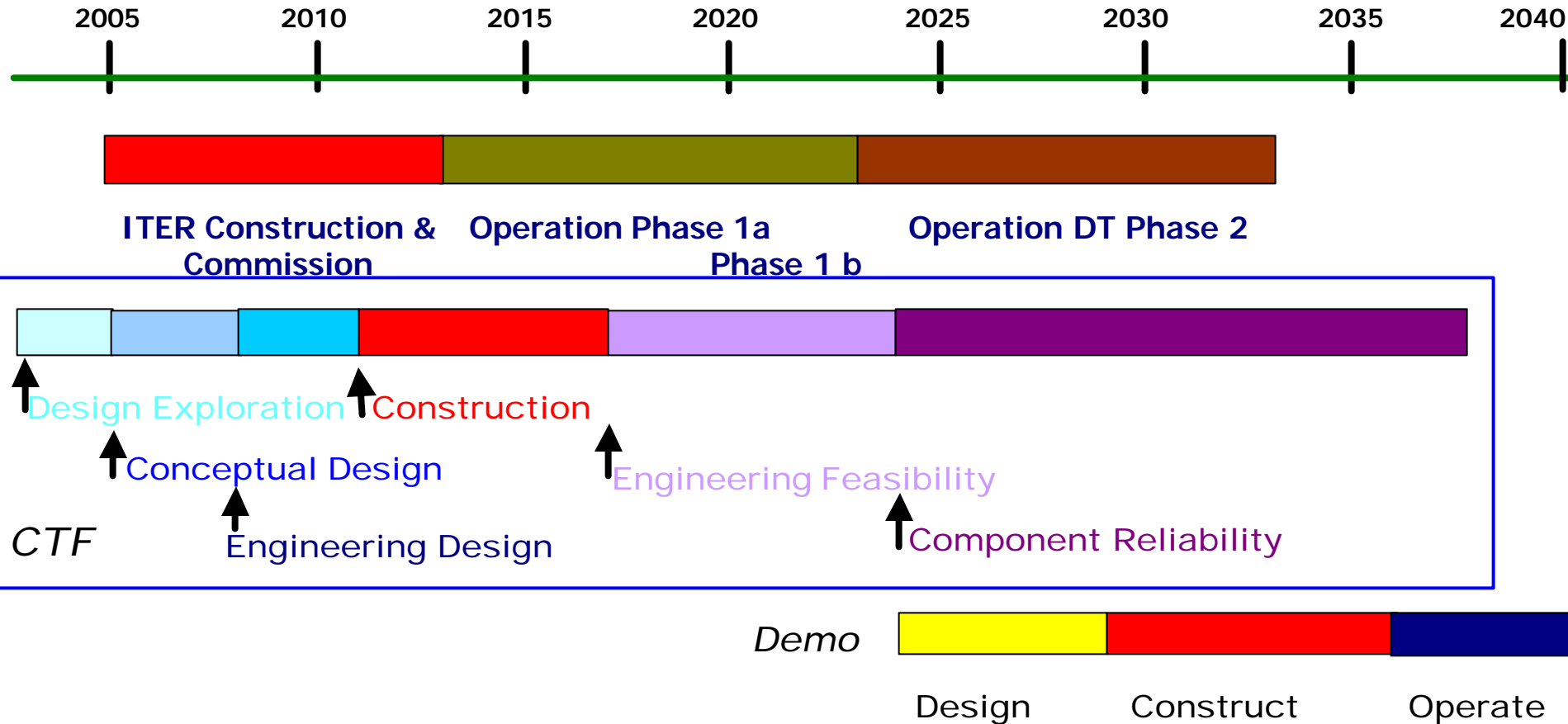
Example Blanket Test Matrix and Sequence

Test Phase/ Number of Test Articles	Scoping Phase	Performance Verification	Reliability Growth
Basic tests (Specimen/Element) <ul style="list-style-type: none"> - Irradiated Properties (2.54 cm x 1 cm x 2.54 cm) - Structural materials - Solid breeder materials - Beryllium - Insulator materials Welds/brazed joints experiments (10 cm x 10 cm x 10 cm)			
Multiple Effect Tests (Submodule) <ul style="list-style-type: none"> - Thermomechanics and tritium recovery (25 cm x 25 cm x 25 cm) - Insulator self healing and MHD pressure drop (25 cm x 25 cm x 25 cm) - Corrosion/ Welds and brazed joints with flow (25 cm x 25 cm x 25 cm) 	Material x configuration x temperature x velocity x redundancy <hr/> 4 x 2 x 2 x 1 x 3 <hr/> 2 x 2 x 2 x 2 x 3 <hr/> 2 x 2 x 2 x 2 x 3		
Integrated Tests (Module) <ul style="list-style-type: none"> - Integrated performance verification (1 m x 1 m x 0.5 m) - Qualification (1 m x 1 m x 0.5 m) - Reliability Growth (1 m x 1 m x 0.5 m) 		Concept x configuration x redundancy 4 x 2 x 3 <hr/>	<hr/> 2 x 2 x 3 <hr/> 2 x 2 x 3 <hr/>
Sector Tests Prototypical full sector test (~3m x 1m x 0.5m)			<hr/> 2 x 1 x 2 <hr/>

Figure 1. Example Test Plan for Divertors



Proposed CTF Timeline



Time line for ITER is taken from K. Lackner's presentation at SOFT, 2002

Are there Good Design Options for CTF?

- A key point in the rationale behind CTF is to design a small size, small fusion power (~ 100 MW), yet achieve a high neutron wall load and steady state plasma operation.
- This can be achieved in MFE by using highly driven plasma (low-Q plasma $\sim 1-2$).

[Similar idea in IFE is to use low target-yield to lower the fusion power but make the chamber radius small enough to get higher wall load]

- Several good options for CTF look attractive.
- The fusion physics and engineering communities need to jointly explore in more detail the options for CTF:
 - e.g. - ST, low-A, standard-A
 - physics and engineering details

Summary

A CREDIBLE Plan for DT Fusion Development MUST include a CREDIBLE Plan for Blanket/PFC Development

- The FEASIBILITY, Operability, and Reliability of Blanket/PFC systems cannot be established without testing in fusion facilities
- The fusion testing requirements for blanket/PFC are:
 - $NWL > 1 \text{ MW/m}^2$, steady state, test area $>10\text{m}^2$, test volume $>5 \text{ m}^3$
 - Fluence Requirements: $> 6 \text{ MW}\cdot\text{y/m}^2$
 - Engineering Feasibility Phase: 1 – 3 $\text{MW}\cdot\text{y/m}^2$**
(concept performance verification and selection)
 - Engineering Development & Reliability Growth Phase: $>4 \text{ MW}\cdot\text{y/m}^2$**
(not an accumulated fluence on a test article; it is “accumulated test time” on successively improved test articles)
- Tritium Supply considerations are a critical factor in developing a credible strategy for fusion testing and development of blanket/PFC
 - The world maximum tritium supply (from CANDU) over the next 40 years is **27 kg**. This tritium decays at 5.47% per year. Cost is high (\$30M-\$200M/kg)
 - Remember: A DT facility with 1000 MW fusion power burns tritium at a rate of **55.8 kg/yr**. Therefore, a large power DT facility must breed its own tritium.

(It is ironic that our major problem is “tritium fuel supply”, while the fundamental premise of Fusion is “inexhaustible” energy source)

Options for "Where" to do Blanket/PFC Developments were evaluated:

1 – ITER(FEAT): Not Suitable

- Low fluence, short plasma burn time/long dwell time, low wall load do not provide the required capability

2 – MODIFIED ITER: Too Expensive, Too Risky

- Requires complete redesign. Very Expensive (Think of ITER-EDA cost plus more)
- Tritium is not available to run the large-power ITER for high fluence
- For Modified ITER to have its own tritium breeding blanket with TBR ~1 is very risky and extremely expensive (building unvalidated blanket over 1000 m² is costly, frequent blanket failures require costly replacements)

3 – DEMO: "Unthinkable"

- Deferring Blanket/PFC development until DEMO is "unthinkable" because:

A – All the problems indicated for Modified ITER above (same mistake of doing FNT testing in large power DT device). Plus there is not much external tritium supply left.

B – This is not a DEMO: a minimum requirement for DEMO is to have at least one validated concept for each component.

So, we have a Serious Problem!

So, what to do?

- Think of What Fission Reactor Developers did as an example:

They built small-power testing reactors (10-100 MW), but with prototypical local conditions.

(They were lucky!!)

- Take advantage of the fact that our good fusion engineers have developed and utilized “**engineering scaling**” to reduce the FNT testing requirements to only 10-20 MW of fusion power with about 10 m² test area (5 m³ test volume)

Attractive Logical Solution

- Build a small size, low-fusion power DT plasma-based device in which Fusion Nuclear Technology experiments can be performed in the relevant fusion environment at the smallest possible scale and cost.
 - In MFE: small-size, low fusion power can be obtained in a **driven low-Q plasma device**.
 - Equivalent in IFE: Lower target yield and smaller chamber radius.
- This is a faster, much less expensive and less risky approach than testing in a large, ignited/high-Q plasma device for which tritium consumption, and cost of operating to high fluence are very high and the risk is too great.