

Enhanced Surface Heat Removal Using a Porous Tungsten Heat Exchanger

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COLLABORATORS

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- Brian Williams (Ultramet Inc.)
- Richard Nygren (Sandia National Labs.)



OBJECTIVE

- High Power Density Capability for Fusion Power Plants:
 - Peak Neutron Wall Load $\sim 10 \text{ MW/m}^2$
 - Peak Surface Heat Load $\sim 2 \text{ MW/m}^2$
- High Power Conversion Efficiency:
 - Greater than 40% (need high coolant exit temperature)
- High Availability:
 - MTBF is greater than 40 MTTR

**Need to Improve Heat Load Capability of
Plasma-Facing Components**



MOTIVIATION

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- The SOLID-WALL of the APEX Study is considering a W-alloy tube with W-foam inside to cool the First-Wall (FW) using Transpiration Cooling:
 - Lithium is boiled inside the FW tubes
 - Lithium pressure is low (<0.2 MPa).
 - Do exploratory research using Helium coolant to measure the improved heat load capability of W-foam inside a W-tube.



APPROACH

Use Porous Structure inside the tube to Enhance Heat transfer from the Wall to the Coolant.

A Test Section using Chemical Vapor Deposited W-foam inside a W-alloy tube was constructed for testing in the Helium-Cooled E-Beam Facility at Sandia.

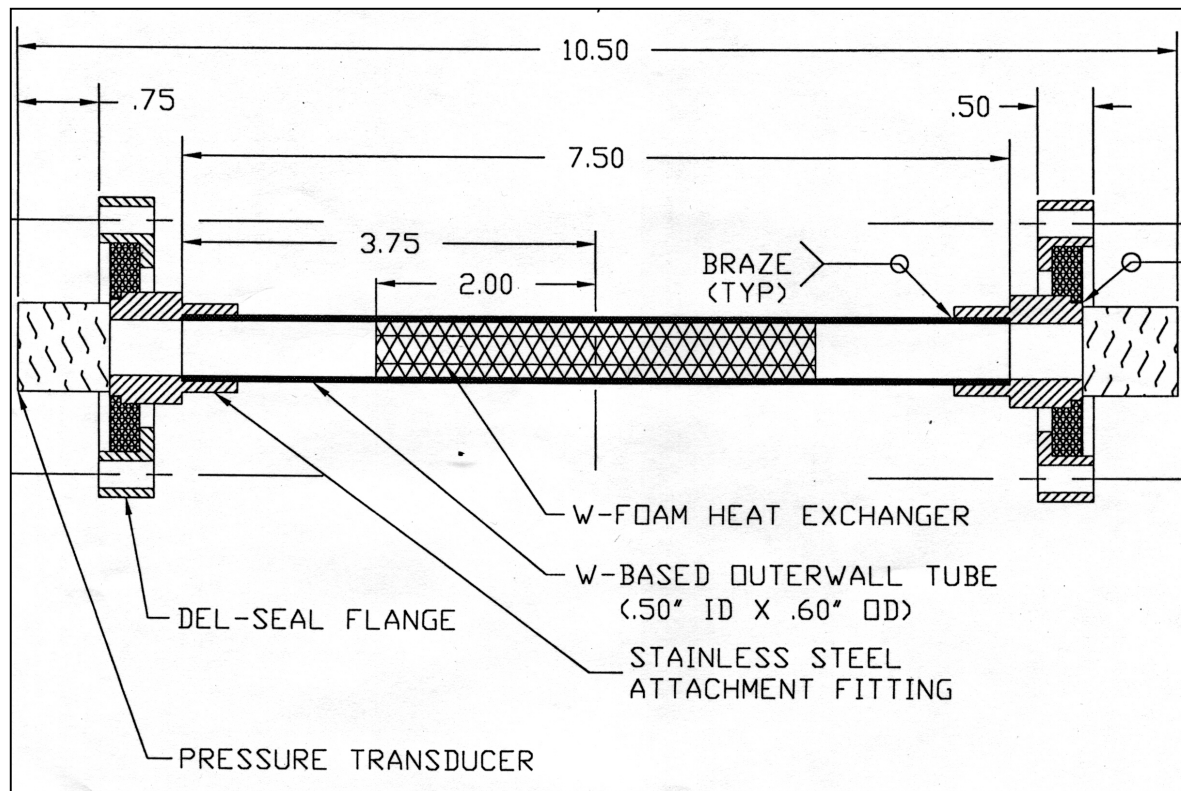
Analyze the Test Section using FEM to model potential heat load capability improvements.

ULTRAMET Inc. successfully constructed a test piece with CVD W-Foam inside a W-tube.



FABRICATED TEST SECTION

- A Test Section (19 cm long W-tube) was fabricated:



Dimensions: inches



FEM MODEL

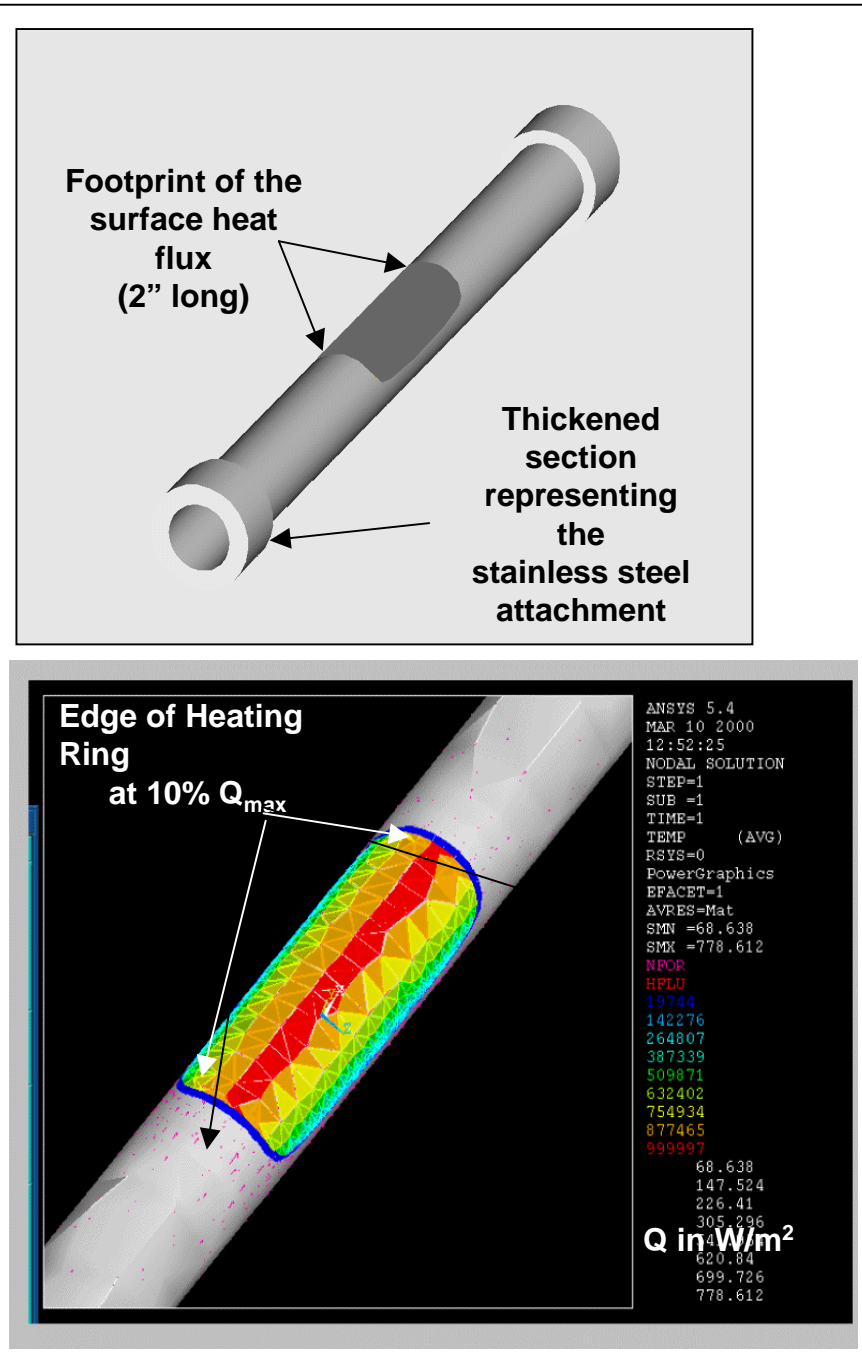
- A 3-D solid model was constructed based on the fabricated test section.
- The FEM model was built using the 3-D solid model to preserve as much detail as necessary.





FEM MODEL (cont.)

- A thin heated rim was included to model the edge of the heated section ($<10\% q''_{max}$)
- Tetragonal Solid Elements were used to mesh the 3-D Model into ~3000 elements.
- Heat transfer coefficients inside the tube are estimated in the case of the presence or absence of W-foam.





MATERIAL PROPERTIES AND FEM ANALYSIS PARAMETERS

| | | | |
|--|-------------|-----------------------------|--------------------------|
| W-Thermal Conductivity (RT/2000°C) | 130/95 | Helium flow rate | 7 g/sec |
| Foam Thermal Conductivity (W/m-K) | 4.5 | Helium pressure | 10 atm |
| Foam Porosity (%) | 90 | Helium entrance temperature | 30°C |
| Foam pores/inches (ppi) | 10 | E-Beam produced heat flux | 1 – 15 MW/m ² |
| Foam Ligament diameter (cm) | 0.0508 | Duration of Heating | 10 – 30 sec |
| Helium Thermal Conductivity (W/m-K) @ RT/600°C | 0.149/0.229 | Duration of E-beam heating | 10 – 30 sec |
| Pr Number @ RT/600°C; | 0.70/0.72 | Length of W-tube | 19.05 cm |
| μ (10 ⁶ kg/m-s) @ RT/600°C | 20.1/31.7 | Length of Foam | 10.16 cm |
| | | Inner Tube Diameter | 1.27 cm |
| | | Tube Wall Thickness | .254 cm |
| | | Length of Heated Section | 5.08 cm |



THERMAL MODEL FOR “NO-FOAM” TUBE

Hydrodynamically Fully Developed Turbulent Flow

$$\text{Re}_D = \frac{4\dot{m}}{\pi D \mu} = 34,000$$

Thermally Developing Turbulent Flow

$$\text{Nu}_D = \frac{hD}{k} = 0.023 \text{Re}_D^{4/5} \text{Pr}^{0.4} \left[1 + \frac{1.4}{L_h/D} \right]$$



TRANSPORT MODEL FOR FOAM FILLED TUBE

1. Conservation of Mass: $\dot{m} = \rho VA = \frac{P}{RT} VA = \text{const.}$

2. Darcy's Law: $-\frac{dP}{dx} = -\frac{P_{in} - P_{out}}{L} = \mu \frac{U_{\infty}}{K}$

Permeability: $K = \frac{D_f^2 \Phi^3}{180(1 - \Phi)^2}$

3. Steady-Flow Energy Equation: $\dot{m} c_p \frac{dT}{dx} = \int_0^{\pi/2} q'' \sin \theta D d\theta$



THERMAL MODEL FOR FOAM FILLED TUBE

Developing Porous Slug Flow Over a Plane Wall

$$\overline{\text{Nu}}_L = \frac{\overline{h}L_h}{k_m} = \frac{q''}{\overline{T}_w - \overline{T}_b} \frac{L}{k_m} = 1.329\text{Pe}_L^{1/2}$$

Peclet Number: $\text{Pe}_L = U_\infty L_h c_p / k_m$

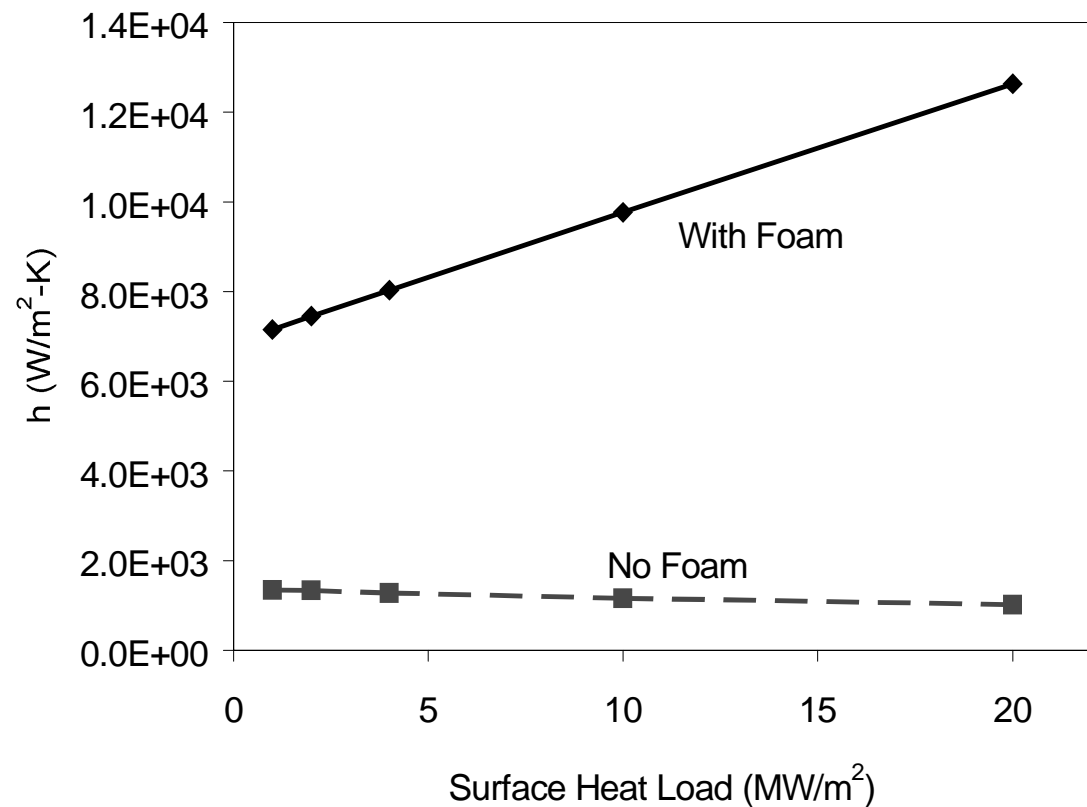
Effective Thermal Conductivity: $k_m = \Phi k_{He} + k_{foam}$



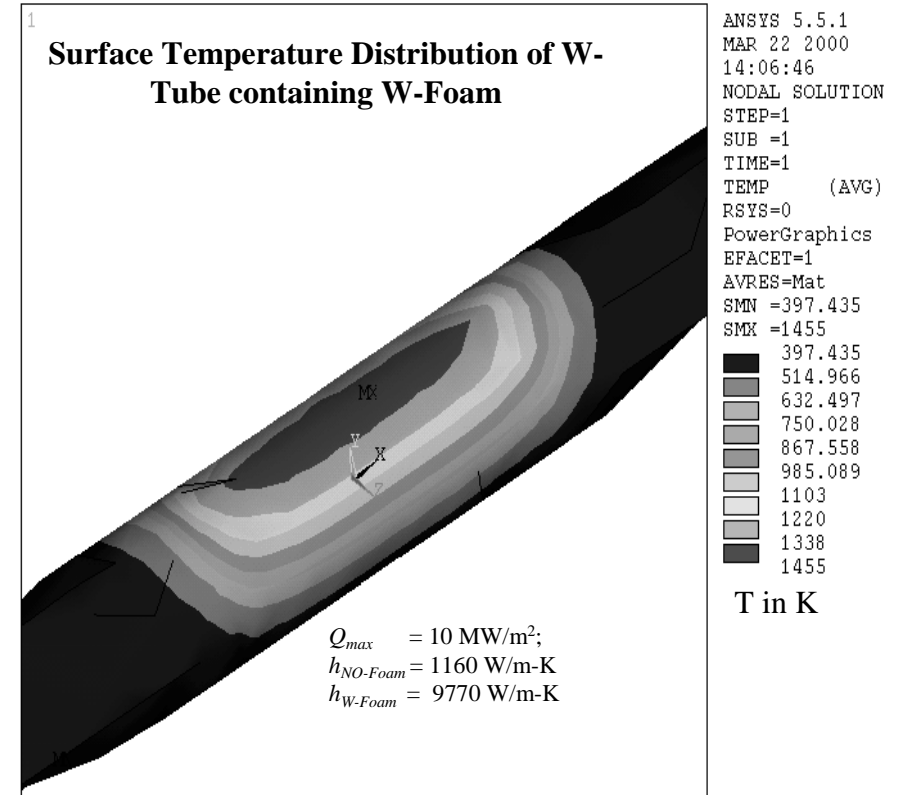
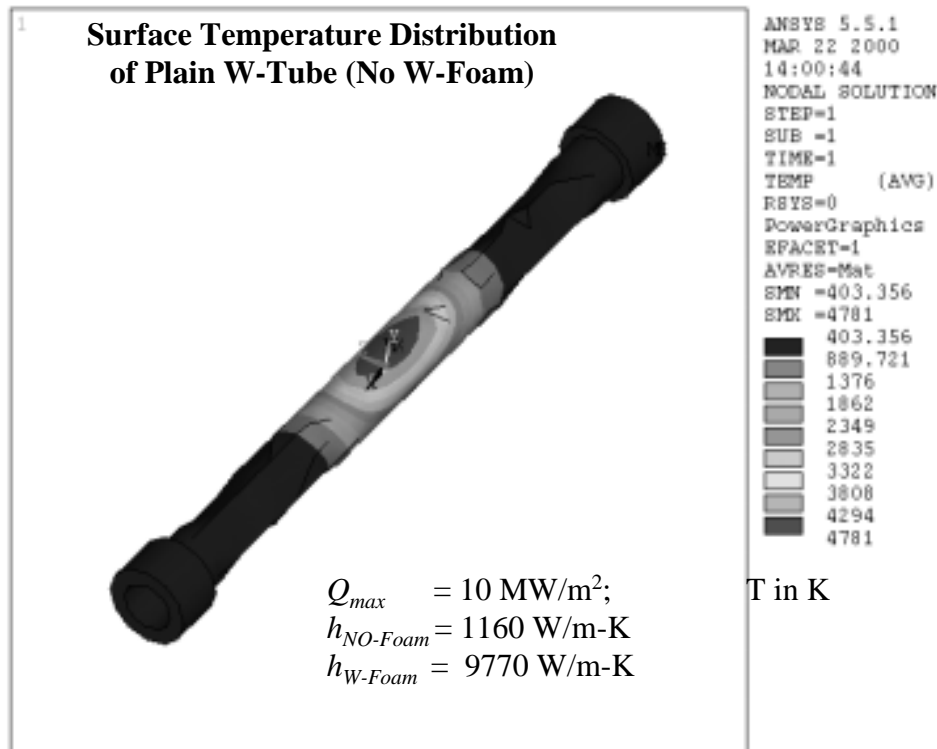
ANALYSIS RESULTS

Effect of W-foam on the overall effective heat transfer coefficient.

- The foam covered region shows an order of magnitude improved h at high heat loads.



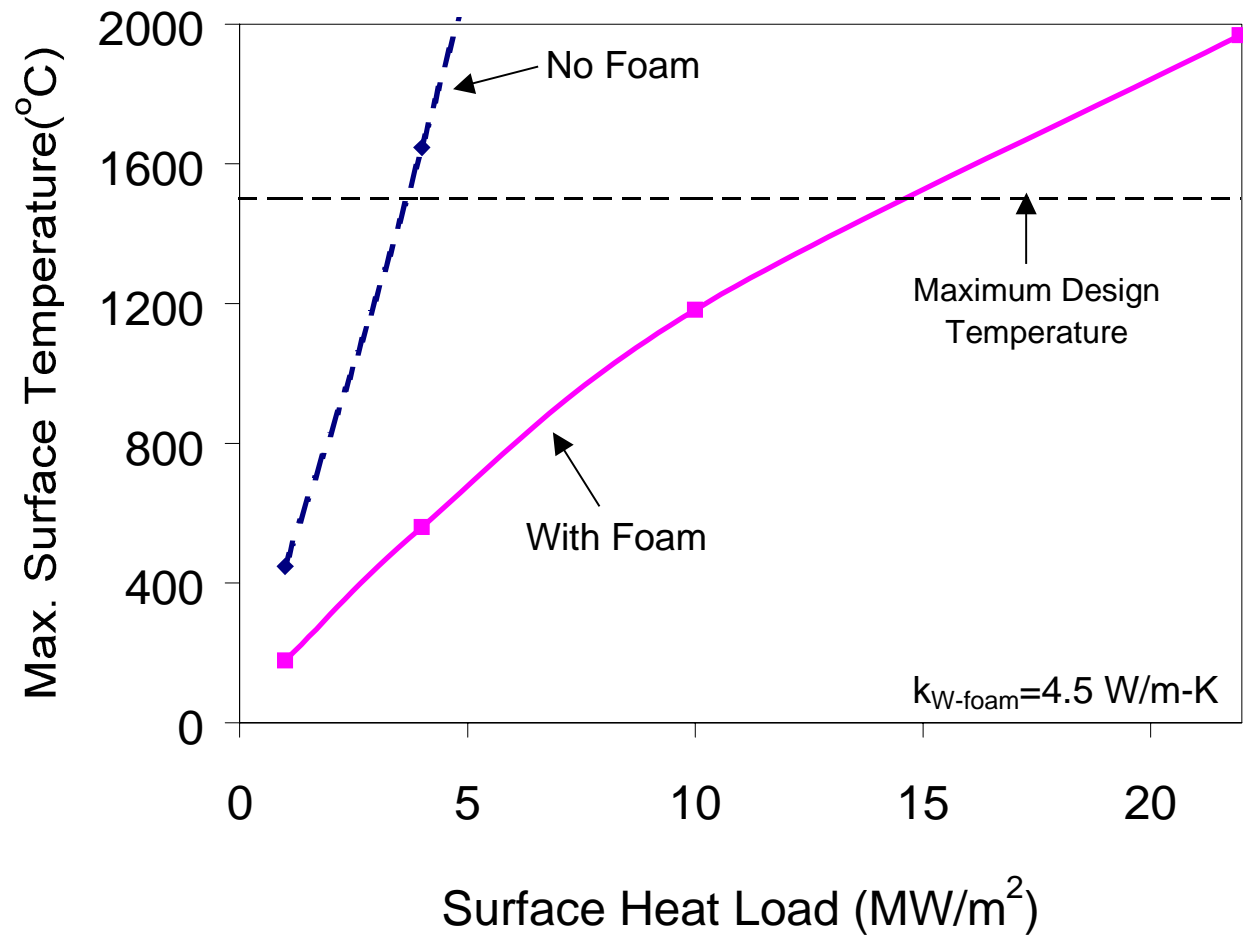
FEM RESULTS



- The foam containing W-tube shows a factor of three reduction in maximum surface temperature from 4788 K down to 1455 K.



EFFECT OF SURFACE HEAT LOAD





SUMMARY AND CONCLUSIONS

- Improvements in surface heat load capacity of plasma-facing components is essential for fusion power plant.
- The use of porous material to enhance the heat conduction from the wall to the coolant is being investigated.
- A W-tube with CVD W-Foam has been fabricated and a thermal FEM analysis has been performed.
- Enhanced heat transfer coefficient, based on fundamental fluid flow through porous material was developed and used in the FEM analysis.
- The W-foam has the potential to improve the heat load capabilities of W-alloys by a factor between 3 and 5 at operating temperatures above 1200°C.