

I. The Equation

For slow deformations where momentum is unimportant,  $\rho \frac{Du_i}{Dt} = 0$ , and the Cauchy conservation of momentum equation (5-4 in notes) becomes:

$$(1) \quad \rho \underline{g} + \underline{\nabla} \cdot \underline{\underline{\tau}} = 0$$

The material we consider (the earth) lies in a self-generated gravitational field and the earth is hydrostatically pre-stressed (eg pressure increases with depth). This pre-stress causes no deformation and is thus conveniently subtracted out.

The stresses <sup>and</sup> applied to the earth's surface by redistributions / load on the surface <sup>and this load-redistribution</sup> causes the deformation. If we let

$$\underline{\underline{\tau}}_{ij} = -p_0(z) \delta_{ij} + \underline{\underline{\sigma}}_{ij}$$

← Deviatoric stress tensor —  
Stress tensor with hydrostatic pressure subtracted out

Then (1) becomes:

$$(2) \quad \rho \underline{g} - \underline{\nabla} p_0 + \underline{\nabla} \cdot \underline{\underline{\sigma}}_{ij} = 0$$

From our previous discussion we know this equation must apply differently to an elastic solid and a fluid. A load floats in a fluid because the deformed fluid moves through the equilibrium (rest state) pressure field. A deformed solid carries a zero-order pressure field with it when it deforms. There is no <sup>elastic</sup> buoyancy. Love realized this in 1911. Pressure is advected in elastic deformation.

If the pressure in the elastic body is  $p$  and a load is applied at  $t_0$ , a short time later, after the elastic deformation is completed, the pressure will be

$$(3) \quad p|_{t+\delta t} = p_0|_{t_0} - \underline{u}^e \cdot \nabla p_0$$

where the superscript  $e$  indicates elastic displacement.

Now linearize the problem by expanding  $p$  and  $\underline{u}$  into rest state (no deformation) and perturbations:

(4)

$$\rho(\underline{x}, t) = \rho_0(x_1) + \rho_1(\underline{x}, t)$$

$$\underline{g}(\underline{x}, t) = \underline{g}_0(x_1) + \underline{g}_1(\underline{x}, t).$$

Note from (1) that since  $\underline{\sigma} = 0$ , the rest state is

(5)

$$\underline{\nabla} p_0 - \rho_0 \underline{g}_0 = 0.$$

Substitution into (2) for the elastin equation here

$$p_0|_{t=sd} = p_0|_L - \underline{u}^e \cdot \underline{\nabla} p_0 \quad \text{yields}$$

$$\underline{\nabla} \cdot \underline{\sigma} = \underbrace{-\nabla p_0 + \underline{\nabla}(\underline{u}^e \cdot \underline{\nabla} p_0)}_{=0 \text{ (4.5)}} + \rho_0 \underline{g}_0 + \rho_1 \underline{g}_0 + \rho_0 \underline{g}_1 =$$

The viscous equation is:

$$\underline{\nabla} \cdot \underline{\sigma} - \underbrace{\nabla p_0 + \rho_0 \underline{g}_0}_{=0} + \rho_1 \underline{g}_0 + \rho_0 \underline{g}_1 = 0$$

Elastin Eqn  
(4)

Then

$$\underline{\nabla} \cdot \underline{\sigma} + \underline{\nabla}(\underline{u}^e \cdot \underline{\nabla} p_0) + \rho_1 \underline{g}_0 + \rho_0 \underline{g}_1 = 0$$

viscous Eqn

(7)

$$\underline{\nabla} \cdot \underline{\sigma} + \rho_1 \underline{g}_0 + \rho_0 \underline{g}_1 = 0$$

These equations can be simplified by expressing  $\rho_1$  in another form. <sup>To first order</sup> The continuity equation is

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho_0 \underline{u} = 0. \quad \text{Integrating over } \Omega \text{ we find}$$

$$\rho_1 \Big|_{t+\Delta t} = \nabla \cdot \rho_0 \underline{u}^e = \underline{u}^e \cdot \nabla \rho_0 + \rho_0 \nabla \cdot \underline{u}^e = \underline{u}_1^e \frac{\partial \rho_0}{\partial x_1} + \rho_0 \nabla \cdot \underline{u}^e.$$

The second term in the elastostatic equation can be expressed:

$$\begin{aligned} \nabla (\underline{u}^e \cdot \nabla p_0) &= \nabla (\underline{u}^e \rho_0 \underline{g}_0) = -\nabla u_1 \rho_0 g_0 \\ &= -\rho_0 \nabla u_1 g_0 - g_0 u_1 \frac{\partial \rho_0}{\partial x_1} \hat{x}_1. \end{aligned}$$

Then

$$\begin{aligned} \underline{g}_0 \rho_1 + \nabla (\underline{u}^e \cdot \nabla p_0) &= \hat{x}_1 g_0 \left( \cancel{\underline{u}_1^e \frac{\partial \rho_0}{\partial x_1}} + \rho_0 \nabla \cdot \underline{u}^e \right) - \rho_0 g_0 \nabla u_1^e - \cancel{g_0 u_1 \frac{\partial \rho_0}{\partial x_1}} \\ &= \rho_0 g_0 \nabla \cdot \underline{u}^e \hat{x}_1 - \rho_0 \nabla u_1^e g_0 \end{aligned}$$

Then (6) becomes

Eqn (6a)

$$\nabla \cdot \underline{\sigma} - \rho_0 \nabla u_1^e g_0 + \rho_0 g_0 (\nabla \cdot \underline{u}^e) \hat{x}_1 + \rho_0 g_1 = 0$$

And by similar methods to uscom eqn (7) is

uscom (7a)

$$\nabla \cdot \underline{\sigma} + \left( \rho_0 g_0 \nabla \cdot \underline{u}^e + g_0 u_1^e \frac{\partial \rho_0}{\partial x_1} \right) \hat{x}_1 + \rho_0 g_1 = 0$$

Notice that we assume change in material density is due to elastic deformation, while buoyancy arises entirely from viscous movements through the zero-order pressure field. Remember  $x_i = \hat{r}$  or  $\hat{z}$ .

In fact  $\frac{\partial \rho_0}{\partial x_i}$  is the non-adiabatic density gradient.

If the fluid changes density adiabatically so it is exactly similar to its surroundings, no buoyant forces arise. Finally, rather than pressure does

not occur in these equations. We apply stresses to

the surface of the earth by re-distributing loads and these stresses cause elastic and viscous deformation.

Avoiding the complication of pressure, a factor separate from the stress tensor, is a conceptual advantage.