

Lecture 14:

Frequency Response of Rational LTI Systems,
Digital Filter Structures

School of Electrical and Computer Engineering
Georgia Institute of Technology
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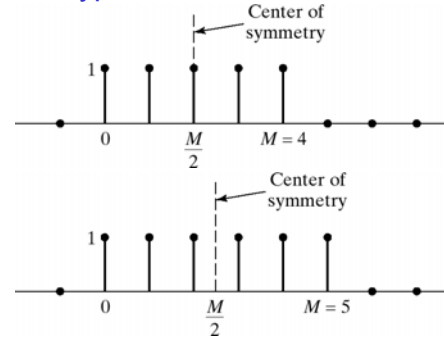
Generalized Linear Phase FIR Systems

$$h[M-n] = h[n] \quad 0 \leq n \leq M$$

$$H(e^{j\omega}) = A_e(e^{j\omega})e^{-j\omega M/2}, \quad A_e(e^{j\omega}) = A_e(e^{-j\omega})$$

- Types I & II:

$$H(z^{-1}) = z^M H(z)$$



Type I:
M even
integer delay

Type II:
M odd
half sample delay

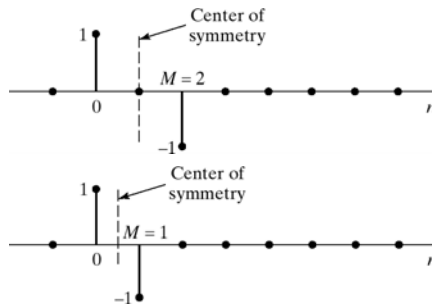
Generalized Linear Phase FIR Systems

$$h[M-n] = -h[n] \quad 0 \leq n \leq M$$

$$H(e^{j\omega}) = jA_o(e^{j\omega})e^{-j\omega M/2}, \quad A_o(e^{j\omega}) = -A_o(e^{-j\omega})$$

- Types III & IV:

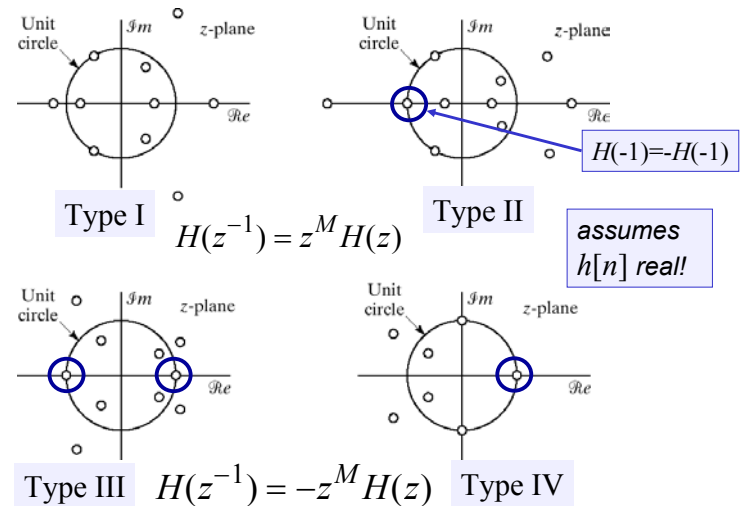
$$H(z^{-1}) = -z^M H(z)$$



Type III:
M even
integer delay

Type IV:
M odd
half sample delay

Zero Locations for FIR Linear Phase



assumes
 $h[n]$ real!

Minimum Phase, Non-Minimum Phase, And Maximum Phase Sequences

Minimum Phase

- A Linear Time-Invariant (LTI) filter $H(z) = B(z)/A(z)$ is said to be *minimum phase* if all its poles and zeros are inside the unit circle $|z|=1$.
- A minimum phase filter has to be *causal*; noncausal terms in the impulse response correspond to poles at infinity (e.g., $H(z)=z$ has zero at 0 and pole at ∞).
- A filter is minimum phase if both the numerator and denominator of its transfer function are *minimum phase polynomials* in z^{-1} .
- A polynomial of the form

$$B(z) = b_0 + b_1z^{-1} + b_2z^{-2} + \dots + b_Mz^{-M}$$

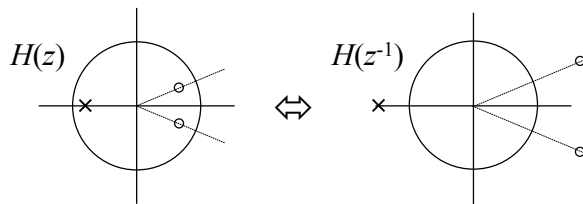
$$= b_0(1 - c_1z^{-1})(1 - c_2z^{-1}) \dots (1 - c_Mz^{-1})$$

is said to be *minimum phase* if all of its roots c_i are inside the unit circle, i.e., $|c_i| < 1$.

- A signal is *minimum phase* if its z -transform is minimum phase. Otherwise, it is non-minimum phase.

Maximum Phase & Mixed Phase

- A polynomial is said to be *maximum phase* if all roots of the polynomial are outside the unit circle.
- A polynomial is said to be *mixed phase* if some of its roots are inside the unit circle and some are outside; when its roots are ON the unit circle, it's called *marginally minimum/maximum phase* correspondingly.
- If $H(z)$ is minimum phase, then $H(z^{-1})$ is maximum phase and vice versa, because substituting z with z^{-1} would "flip" the poles and zeros in and out of the unit circle.



Minimum Phase & Maximum Decaying Sequence

- A sequence $1, c, 0, 0, \dots$ has a z -transform $H(z) = 1 + cz^{-1}$
- It is minimum phase if $|c| < 1$, meaning, it's a decaying sequence.
- Many signals have identical power spectral density

$$H(z)H^*(z)|_{z=e^{j\omega}} = \prod_{i=1}^M (1 - c_i e^{-j\omega})(1 - c_i^* e^{j\omega})$$

(e.g., any H that has the collection of either (c_i, c_i^*) or $(c_i^{-1}, (c_i^*)^{-1})$ as its root pairs)

- The minimum-phase signal $h_{m-p}(n)$ has the *fastest decay* in the sense that

$$\sum_{n=0}^K |h_{m-p}(n)|^2 \geq \sum_{n=0}^K |h_i(n)|^2 \quad K = 0, 1, 2, \dots$$

Thus, minimum-phase signals are *maximally concentrated toward time 0* among all causal signals $h_i(n)$ with a given magnitude spectrum.

All-Pass Systems

First order all-pass filter $H_{ap}(z) = \frac{z^{-1} - a^*}{1 - az^{-1}}$

$$H_{ap}(e^{j\omega}) = \frac{e^{-j\omega} - a^*}{1 - ae^{-j\omega}} = e^{-j\omega} \frac{1 - a^* e^{j\omega}}{1 - ae^{-j\omega}} \quad |H_{ap}(e^{j\omega})| = 1$$

$$20 \log_{10} |H_{ap}(e^{j\omega})| = 0 \quad a = re^{j\theta}$$

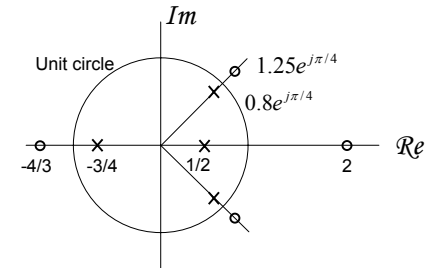
$$\angle H(e^{j\omega}) = \angle \frac{e^{-j\omega} - re^{-j\theta}}{1 - re^{j\theta} e^{-j\omega}} = -\omega - 2 \arctan \left[\frac{r \sin(\omega - \theta)}{1 - r \cos(\omega - \theta)} \right]$$

$$\text{grd} \left[\frac{e^{-j\omega} - re^{-j\theta}}{1 - re^{j\theta} e^{-j\omega}} \right] = \frac{1 - r^2}{1 + r^2 - 2r \cos(\omega - \theta)} = \frac{1 - r^2}{|1 - re^{j\theta} e^{-j\omega}|^2}$$

Higher Order All-Pass Systems

Typical pole-zero pattern of an all-pass system

- If a is a pole, then $(a^*)^{-1}$ must be a zero
- If a is a zero, then $(a^*)^{-1}$ must be a pole



All-pass filters are used to alter the phase property of a signal or a system, for example:

- compensate for phase or group delay distortion;
- change the peak to rms ratio of a signal without changing its log magnitude spectrum
- “construct” minimum-phase systems

Stable All-Pass Systems has Positive GRD

First order all-pass filter $H_{ap}(z) = \frac{z^{-1} - a^*}{1 - az^{-1}}$

$$a = re^{j\theta} \quad |H_{ap}(e^{j\omega})| = 1$$

For a stable and causal all-pass system,

$$r < 1 \quad (\text{i.e., poles are within the unit circle})$$

$$\text{grd} \left[\frac{e^{-j\omega} - re^{-j\theta}}{1 - re^{j\theta} e^{-j\omega}} \right] = \frac{1 - r^2}{1 + r^2 - 2r \cos(\omega - \theta)} = \frac{1 - r^2}{|1 - re^{j\theta} e^{-j\omega}|^2} > 0$$

Minimum-Phase & All-Pass Decomposition

Any rational system can be expressed as

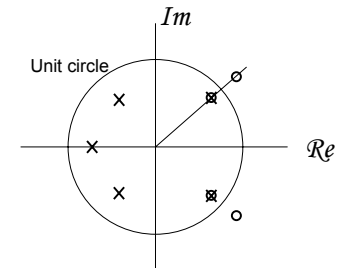
$$H(z) = H_{m-p}(z)H_{a-p}(z)$$

Assume $H(z)$ has one zero outside the unit circle at $z = 1/c^*$, $|c| < 1$

$$H(z) = H_1(z)(z^{-1} - c^*) = H_1(z)(1 - cz^{-1}) \frac{(z^{-1} - c^*)}{(1 - cz^{-1})}$$

$H_1(z)(1 - cz^{-1})$ is minimum phase because $|c| < 1$

Therefore, $H(z) = H_{m-p}(z)H_{a-p}(z)$



Minimum Phase & Minimum GRD

$$H(z) = H_{m-p}(z)H_{a-p}(z)$$

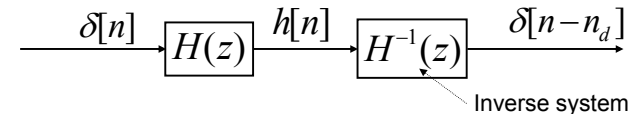
$$\angle H(z) = \angle H_{m-p}(z) + \angle H_{a-p}(z)$$

$$\text{grd}[H(z)] = \text{grd}[H_{m-p}(z)] + \text{grd}[H_{a-p}(z)]$$

$$\text{grd}[H_{a-p}(z)] \geq 0$$

Therefore, of all the $H(z)$ that have the same magnitude spectrum, the corresponding minimum phase system has the minimum group delay.

Inverse Systems



- An inverse system produces an impulse as output when driven by the impulse response of the original system.
- In practice, the output impulse may have a relative delay with respect to the original impulse.

Example:

$$H(z) = \frac{1}{1 - 2r \cos \theta z^{-1} + r^2 z^{-2}} \quad H_{inv}(z) = H^{-1}(z) = 1 - 2r \cos \theta z^{-1} + r^2 z^{-2}$$

$$h[n] = \frac{r^n \sin[\theta(n+1)]}{\sin \theta} u[n] \quad h_{inv}[n] = \delta[n] - 2r \cos \theta \delta[n-1] + r^2 \delta[n-2]$$

Digital Filters

- General N^{th} -order difference equation:

$$y[n] = \sum_{k=1}^N a_k y[n-k] + \sum_{k=0}^M b_k x[n-k]$$

- System function:

$$H(z) = \frac{\sum_{k=0}^M b_k z^{-k}}{1 - \sum_{k=1}^N a_k z^{-k}} = A \frac{\prod_{k=1}^M (1 - c_k z^{-1})}{\prod_{k=1}^N (1 - d_k z^{-1})}$$

- There is a direct correspondence between the difference equation and the system function when the numerator and denominator are written as polynomials in z^{-1} .

Direct Form I Implementation

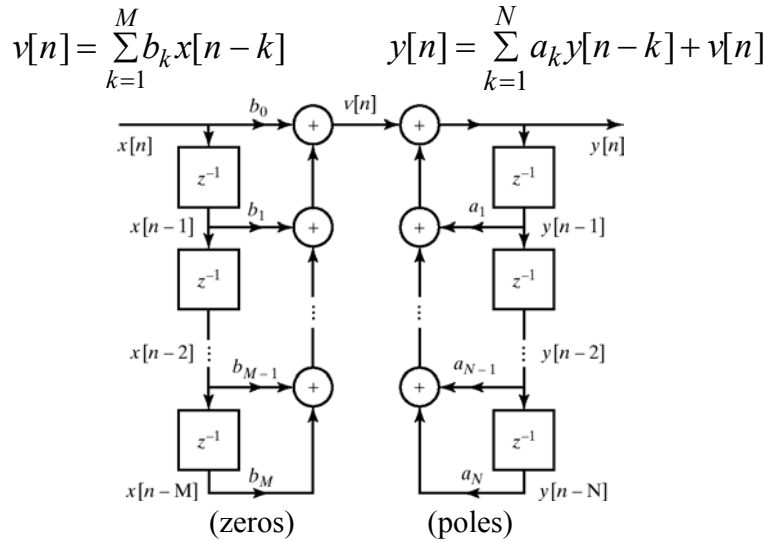
$$H(z) = \frac{\sum_{k=0}^M b_k z^{-k}}{1 - \sum_{k=1}^N a_k z^{-k}} = \underbrace{\left(\frac{1}{1 - \sum_{k=1}^N a_k z^{-k}} \right)}_{\text{poles}} \underbrace{\left(\sum_{k=0}^M b_k z^{-k} \right)}_{\text{zeros}}$$

$$Y(z) = H(z)X(z)$$

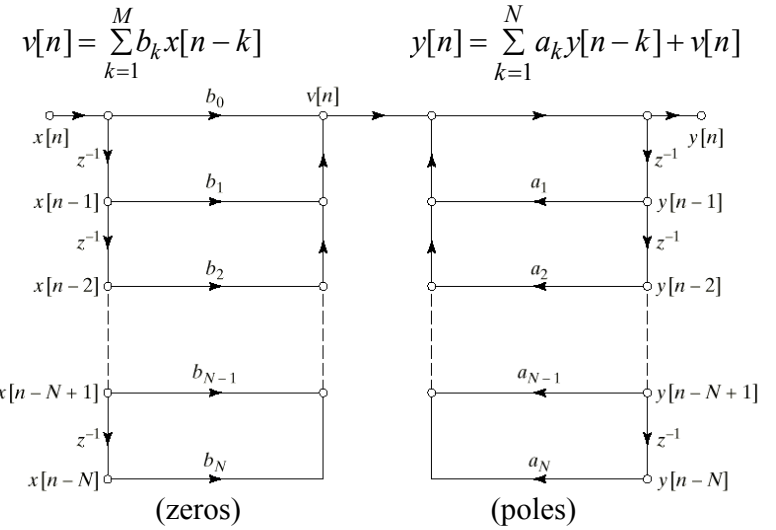
$$v[n] = \sum_{k=0}^M b_k x[n-k] \quad (\text{zeros})$$

$$y[n] = \sum_{k=1}^N a_k y[n-k] + v[n] \quad (\text{poles})$$

Block Diagram of IIR Direct Form I



Signal Flow Graph IIR Direct Form I



Direct Form II Implementation

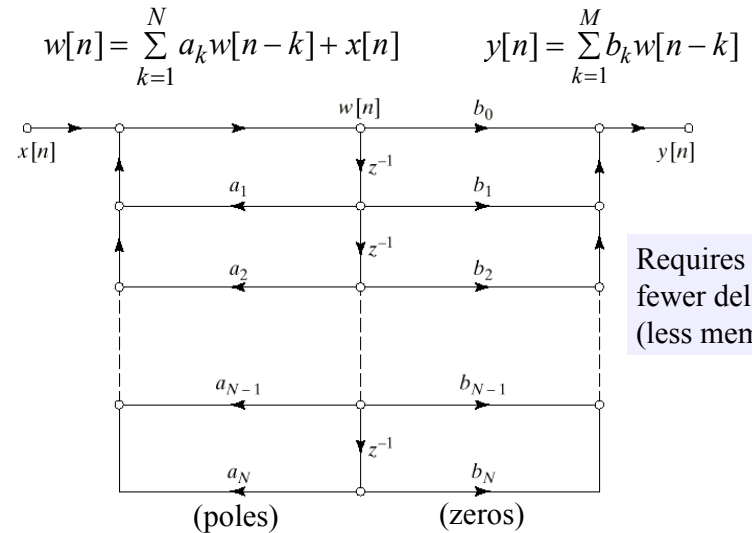
$$H(z) = \frac{\sum_{k=0}^M b_k z^{-k}}{1 - \sum_{k=1}^N a_k z^{-k}} = \underbrace{\sum_{k=0}^M b_k z^{-k}}_{\text{zeros}} \left(\underbrace{\frac{1}{1 - \sum_{k=1}^N a_k z^{-k}}}_{\text{poles}} \right)$$

$$Y(z) = H(z)X(z)$$

$$w[n] = \sum_{k=1}^N a_k w[n-k] + x[n] \quad (\text{poles})$$

$$y[n] = \sum_{k=0}^M b_k w[n-k] \quad (\text{zeros})$$

IIR Direct Form II



Requires fewer delays
(less memory)