

COMPUTER PROGRAM FOR REFRACTION OF
DIRECTIONAL RANDOM WAVES

by

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SPONSORED BY
U.S. ARMY COASTAL ENGINEERING RESEARCH CENTER

RESEARCH REPORT NO. CACR-93-04
JULY, 1993

CENTER FOR APPLIED COASTAL RESEARCH
DEPARTMENT OF CIVIL ENGINEERING
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ABSTRACT

A computer program called **RESHOAL** is presented in this report. **RESHOAL** computes the directional random wave spectrum in specified shallow water depth for given incident directional random wave spectrum in deeper water depth using linear finite-depth theory for straight shorelines with parallel bottom contours. To minimize the required input, the incident directional random wave spectrum is assumed to be given by the product of the *TMA* frequency spectrum and the Mitsuyasu-type directional spreading function. The input parameters for the *TMA* spectrum are the water depth, the spectral estimate of the significant wave height, the spectral peak period, and the peak enhancement factor for the spectral shape. The input parameters for the directional spreading function are the dominant incident wave direction and the maximum value of the spreading parameter.

The output of **RESHOAL** includes the directional random wave spectrum, the refracted frequency spectrum, and the directional energy distribution function in specified shallower water depth. The corresponding shoaled uni-directional frequency spectrum is also computed to quantify the effects of directional spreading and oblique incidence. The spectral parameters computed from the incident, refracted, and shoaled uni-directional frequency spectra include the spectral estimates of the different wave heights and periods as well as the parameters related to the spectral shape. The directional energy distribution function is used to compute the dominant wave direction and the degree of wave energy spreading about the dominant wave direction. In addition, the time series corresponding to the computed frequency spectra are generated numerically using a random phase scheme. The generated time series are analyzed using a

zero up-crossing method. The output parameters from the computed time series include various wave heights and periods as well as the parameters related to wave grouping. The individual zero up-crossing waves are compared with an empirical criterion of regular wave breaking to ensure that no wave breaking will occur in the specified shallow water depth since the linear finite-depth theory employed herein is not applicable for breaking waves.

Finally, an equivalent uni-directional frequency spectrum is computed to generate the shoaled uni-directional frequency spectrum in a two-dimensional wave flume that will be equivalent to the refracted frequency spectrum in the specified shallow water depth as long as the linear finite-depth theory is valid. An example is given to show the use of the computed equivalent uni-directional frequency spectrum in order to account for the effects of directionality and refraction in a two-dimensional experiment.

ACKNOWLEDGEMENT

The authors thank Andoyo Wurjanto and Daniel Cox for their contributions to the development of **RESHOAL**. This is the first report resulting from research sponsored by the Coastal Engineering Research Center, U.S. Army Engineer Waterways Experiment Station under contract number DACW 39-93-C-0074.

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Chapter 1

INTRODUCTION

1.1 BACKGROUND

The design of a coastal structure requires the determination of design wave conditions at the site of the structure, while available wave data is typically situated in relatively deep water (e.g., 10 m depth). Consequently, analyses of irregular wave transformation into the nearshore region will be necessary. The effects of directional spreading of incident irregular waves are generally not considered in such analyses. Relatedly, hydraulic model tests for the design of a coastal structure are typically performed in a two-dimensional wave flume since three-dimensional model tests are time consuming and expensive. The two-dimensional tests do not account for the effects of directional spreading unless wave conditions in front of the structure are reproduced approximately considering the refraction and shoaling of directional random waves.

For the restricted case of a straight shoreline with parallel bottom contours, linear finite-depth theory (Longuet-Higgins 1957; LeMéhauté and Wang 1982) may be applied to predict the refraction and shoaling of directional random waves with little computational effort. This theory has been shown to be reasonably accurate except that it does not predict the generation of higher and lower harmonics due to nonlinear wave-wave interactions (Elgar and Guza 1985; Freilich *et al.* 1990; Abreu *et al.* 1992). It is noted that nonlinear theories for directional random waves are available but require considerable computational efforts. Kobayashi and Wurjanto (1992) applied this theory to estimate the incident random waves immediately seaward of the breaker zone which

were used as input to the numerical model **RBREAK** for predicting irregular wave setup and run-up on natural beaches. The computer program **RESHOAL** presented in this report is an expanded version of the computer program used by Kobayashi and Wurjanto (1992) to allow more routine applications of linear finite-depth theory for the refraction and shoaling of directional random waves incident on straight shorelines with parallel bottom contours.

1.2 OUTLINE OF REPORT

This report is written in such a way that users should be able to run **RESHOAL** without knowing the details of the computer program **RESHOAL** listed in Appendix A. Chapter 2 concisely explains the equations and numerical procedures used in **RESHOAL**. Chapter 3 explains the computer program **RESHOAL** in detail, although the listed computer program is written in a self-explanatory manner. The additional explanations will facilitate usage of **RESHOAL** and modifications of **RESHOAL** by users if necessary.

Appendix B presents computed examples corresponding to Run 1 in the paper of Kobayashi and Wurjanto (1992) who used an earlier version of **RESHOAL** to compute the incident random waves immediately seaward of the breaker zone. **RESHOAL** based on linear finite-depth theory is not applicable inside the surf zone. The computed incident random waves were used as input to the numerical model **RBREAK** which is applicable for breaking and broken waves. **RBREAK** can not predict shoaling of nonlinear shallow-water waves over a long distance without wave breaking as explained by Kobayashi *et al.* (1989). The combined use of **RESHOAL** and **RBREAK** will hence be necessary for the design of coastal structures located inside the surf zones if design waves are specified in relatively deep water.

Appendix C presents an example of the applications of **RESHOAL** to a laboratory experiment in a two-dimensional wave flume. In this example, directional random waves specified at the location of a wave maker are shoaled and refracted using **RESHOAL**. The refracted frequency spectrum at specified shallower water depth is computed from the refracted directional random waves. The equivalent uni-directional frequency spectrum at the location of the wave maker is then computed from the refracted frequency spectrum. Linear uni-directional random waves generated using this equivalent frequency spectrum in a two-dimensional wave flume will result in the shoaled uni-directional frequency spectrum that will be the same as the refracted frequency spectrum at the specified shallower depth provided other factors such as nonlinearity and dissipation are negligible.

Appendix D explains the contents of the disk accompanying this report as well as the computation time for each of the examples included in this report.

Chapter 2

MATHEMATICAL FORMULATION

2.1 GOVERNING EQUATION

Linear finite-depth theory for computing the shoaling and refraction of directional random waves incident on straight shorelines with parallel bottom contours can be expressed as (LeMéhauté and Wang 1982)

$$S_2(f, \theta_2) = \frac{C_1(Cg)_1}{C_2(Cg)_2} S_1(f) G_1(f, \theta_1) = \frac{k_2 (Cg)_1}{k_1 (Cg)_2} S_1(f) G_1(f, \theta_1) \quad (2.1)$$

with

$$\theta_1 = \sin^{-1} \left(\frac{k_2}{k_1} \sin \theta_2 \right) \quad (2.2)$$

where

$S(f, \theta)$ = directional wave spectrum ($s \cdot m^2$)

$S(f)$ = frequency spectrum ($s \cdot m^2$)

$G(f, \theta)$ = directional spreading function defined as $G(f, \theta) = S(f, \theta)/S(f)$

C = phase velocity = $\frac{2\pi f}{k}$ (m/s)

Cg = group velocity = $\frac{C}{2} \left[1 + \frac{2kh}{\sinh(2kh)} \right]$ (m/s)

f = frequency (Hz)

θ = wave direction (rad) with $\theta = 0$ for normal incidence

h = water depth (m)

k = wave number (1/m)

computed from the linear dispersion relationship

$$kh \tanh(kh) = h(2\pi f)^2/g \quad (2.3)$$

In this report, the subscript 1 denotes the deeper water depth where the incident directional waves are specified, while the subscript 2 indicates the shallower water depth where the refracted directional waves are predicted.

2.2 COMPUTATIONAL DOMAINS

The frequency, time and angle are discretized in the following manners to reduce the number of input parameters. The maximum frequency, f_{max} , and the number of data points, NP, are selected from the following criterion:

$$f_{max} = 1/(2\Delta t) = 10/T_p \text{ with } \Delta t = T_p/20$$

$$NP = t_{max}/\Delta t = 4000 \text{ with } t_{max} = 200T_p$$

where

$$T_p = \text{incident wave spectral peak period (s)}$$

$$\Delta t = \text{time step or sampling interval (s)}$$

$$t_{max} = \text{duration of generated time series (s).}$$

The corresponding number of discrete frequencies within the frequency domain is

$$NF = \frac{NP + 2}{2} = 2001. \quad (2.4)$$

Setting the minimum frequency $f_{min} = 0$, the frequency band width Δf and the discrete frequency f_j are computed

$$\Delta f = \frac{f_{max} - f_{min}}{NF - 1} \quad (2.5)$$

$$f_j = f_{min} + (j - 1)\Delta f \quad (2.6)$$

where the subscript $j = 1, 2, 3, \dots, NF$ and $f_{min} = 0$. Similarly, the time level t_n is given by

$$t_n = t_{min} + (n - 1)\Delta t \quad (2.7)$$

with

$$\Delta t = \frac{1}{2f_{max}} \quad (2.8)$$

where the subscript $n = 1, 2, 3, \dots, NP$ and $t_{min} = 0$. It is noted that the time series are assumed to be periodic with the period t_{max} . The directional domain ranges from $\theta_{min} = -90^\circ$ to $\theta_{max} = 90^\circ$. Specifying the number of discrete angles as $ND = 181$, the directional bandwidth $\Delta\theta$ and discretized wave direction θ_i are given by

$$\Delta\theta = \frac{\theta_{max} - \theta_{min}}{ND - 1} = 1^\circ \quad (2.9)$$

$$\theta_i = \theta_{min} + (i - 1)\Delta\theta \quad (2.10)$$

where the subscript $i = 1, 2, 3, \dots, ND$.

2.3 INCIDENT FREQUENCY SPECTRUM

The incident frequency spectrum in the deeper water depth is assumed to be given by the *TMA* spectrum (Bouws *et al.* 1985)

$$S_1(f) = S_{TMA}(f) = S_J \Phi_K. \quad (2.11)$$

The transformation factor Φ_K extending the JONSWAP spectrum to the finite depth h_1 is expressed as

$$\Phi_K = \tanh^2(k_1 h_1) \left[1 + \frac{2k_1 h_1}{\sinh(2k_1 h_1)} \right]^{-1}. \quad (2.12)$$

The JONSWAP spectrum S_J for wind waves in deep water is given by

$$S_J = S_P(f) \Phi_{PM}(f/f_p) \Phi_J(f, f_p, \gamma, \sigma) \quad (2.13)$$

with

$$S_P(f) = \alpha g^2 (2\pi)^{-4} f^{-5} \quad (2.14)$$

$$\Phi_{PM}(f/f_p) = \exp [(-5/4)(f/f_p)^{-4}] \quad (2.15)$$

$$\Phi_J(f, f_p, \gamma, \sigma) = \exp \left\{ \ln(\gamma) \exp \left[-(f - f_p)^2 / (2\sigma^2 f_p^2) \right] \right\} \quad (2.16)$$

$$\sigma = \begin{cases} \sigma_a = 0.07 & f_p \geq f \\ \sigma_b = 0.09 & f_p < f \end{cases} \quad (2.17)$$

where

α = variable coefficient related to the spectral estimate of the significant wave height H_{m0} at the deeper water depth h_1

g = gravitational acceleration

f_p = spectral peak frequency at the deeper water depth h_1

σ = variable coefficient assumed to be given by the standard values in (2.17)

The peak enhancement factor γ may range from 1 to 7 with a mean of 3.3. The value of γ will need to be determined using site-specific wave data. It is noted that the *TMA* spectrum is limited to wind waves and does not include infragravity waves (*e.g.*, Elgar *et al.* 1992).

The Bretschneider-Mitsuyasu spectrum in deep water (Goda 1985) is expressed as

$$S_1(f) = 0.257 H_s^2 T_s (T_s f)^{-5} \exp[-1.03(T_s f)^{-4}] \quad (2.18)$$

where H_s and T_s are the significant wave height and period. Goda assumed in (2.18) that $H_s = H_{m0}$ and $T_s = T_p/1.05$ and (2.18) is rewritten as

$$S_1(f) = 0.312 H_{m0}^2 T_p (T_p f)^{-5} \exp[-1.25(T_p f)^{-4}] \quad (2.19)$$

The *TMA* spectrum given by (2.11) reduces to (2.19) for $\gamma = 1$ and $\Phi_K = 1$. The computer program **RESHOAL** allows for the specification of the incident frequency spectrum $S_1(f)$ using (2.11) for any value of γ including $\gamma = 1$. To include the case of deep water in (2.11), an option is provided to specify $\Phi_K = 1$ by specifying **IDEEP** = 1 as input.

2.4 DIRECTIONAL SPREADING FUNCTION

The Mitsuyasu-type spreading function $G_1(f, \theta_1)$ at the deeper water depth h_1 as given by Goda (1985), is assumed in this report

$$G_1(f, \theta_1) = \frac{S_1(f, \theta_1)}{S_1(f)} = G_o(f) \cos^{2s(f)} \left(\frac{\theta_1 - \alpha_p}{2} \right) \quad (2.20)$$

where α_p is the predominant incident wave direction relative to the axis of $\theta = 0$ normal to the straight shoreline and ranges from $-\pi/2$ to $\pi/2$. The spreading parameter $s(f)$ and the normalization parameter $G_o(f)$ are expressed as

$$s(f) = \begin{cases} s_{max}(f/f_p)^5 & f \leq f_p \\ s_{max}(f/f_p)^{-2.5} & f > f_p \end{cases} \quad (2.21)$$

$$G_o(f) = \frac{1}{\pi} 2^{2s-1} \frac{\Gamma^2(s+1)}{\Gamma(2s+1)} \quad (2.22)$$

where s_{max} denotes the maximum value of s at $f = f_p$. Field observations indicate that $s_{max} \simeq 10$ for wind waves and $s_{max} \simeq 25 - 75$ for swells (Goda 1985). Γ denotes the gamma function (Press *et al.* 1986). It is noted that (2.20) was defined in the range $-\pi \leq (\theta_1 - \alpha_p) \leq \pi$ which included waves propagating seaward. In this report, all the waves are assumed to propagate landward with the corresponding range $-\pi/2 \leq \theta_1 \leq \pi/2$ in relation to (2.9) and (2.10). This will not cause any problems provided G_1 is negligible in the ranges $(-\pi + \alpha_p) \leq \theta_1 < -\pi/2$ and $\pi/2 < \theta_1 \leq (\pi + \alpha_p)$. Combining the incident frequency spectrum $S_1(f)$ and the directional spreading function $G_1(f, \theta)$, the incident directional spectrum is given by

$$S_1(f, \theta_1) = S_1(f)G_1(f, \theta_1) \quad (2.23)$$

which has been used in (2.1).

2.5 ENERGY DISTRIBUTION FUNCTION

The directional energy distribution function may be defined as

$$D(\theta) = \int_{f_{min}}^{f_{max}} S(f, \theta) df \quad (2.24)$$

where $f_{min} = 0$ and f_{max} has been given in Section 2.2. The directional spectrum $S(f, \theta)$ is $S_1(f, \theta_1)$ given by (2.23) or $S_2(f, \theta_2)$ computed by (2.1). The functions $D_1(\theta_1)$ and $D_2(\theta_2)$ at the corresponding water depths h_1 and h_2 are used to examine the energy distributions with respect to the wave direction.

2.6 SHOALING OF UNI-DIRECTIONAL RANDOM WAVES

Uni-directional waves propagating at normal incidence to the shoreline, such as irregular waves generated in a two-dimensional wave flume, undergo shoaling only. The frequency spectrum at the shallower water depth h_2 for uni-directional, normally-incident waves is given by (*e.g.* Goda 1985)

$$S_2^u(f) = \frac{(Cg)_1}{(Cg)_2} S_1(f) \quad (2.25)$$

where Cg = group velocity and $S_1(f)$ is assumed to be given by (2.11).

2.7 REFRACTION OF DIRECTIONAL RANDOM WAVES

The refracted directional wave spectrum at the shallower water depth h_2 is computed by (2.1) which is rewritten as

$$S_2(f, \theta_2) = \frac{k_2 (Cg)_1}{k_1 (Cg)_2} S_1(f, \theta_1). \quad (2.26)$$

For the computation of $S_2(f, \theta_2)$, θ_2 is discretized uniformly and the corresponding value of θ_1 is calculated from (2.2). Since $|\sin \theta_1| \leq 1$, $S_2(f, \theta_2)$ is set equal to zero when $(k_2 \sin \theta_2 / k_1) > 1$.

The refracted frequency spectrum at the shallower water depth h_2 is computed from the refracted directional spectrum

$$S_2(f) = \int_{\theta_{min}}^{\theta_{max}} S_2(f, \theta_2) d\theta_2. \quad (2.27)$$

The refracted energy distribution function $D_2(\theta_2)$ is calculated using (2.24) with $S(f, \theta) = S_2(f, \theta_2)$. The predominant wave direction at the shallower water depth h_2 is assumed to be the direction where $D_2(\theta_2)$ is the maximum.

2.8 SPECTRAL PARAMETERS

The spectral parameters associated with the frequency spectra, $S_1(f)$, $S_2^u(f)$, and $S_2(f)$, represented by $S(f)$ in the following are computed using the subroutine **SPCPAR** written by Cox *et al.* (1991) and modified herein. These parameters are also explained in Goda (1985) except for the spectral correlated parameter κ (Battjes and van Vledder, 1984; Liu *et al.*, 1993) and summarized in the following for convenience.

The n -th spectral moment of $S(f)$ with $n = 0, 1, 2$ and 4 is computed from

$$m_n = \int_{f_{min}}^{f_{max}} f^n S(f) df. \quad (2.28)$$

The following spectral parameters are computed:

- Spectral width parameter based on m_2 and m_4 :

$$\epsilon = \left[1 - \frac{m_2^2}{m_0 m_4} \right]^{1/2} \quad (2.29)$$

- Spectral width parameter based on m_1 and m_2 :

$$\nu = \left[\frac{m_0 m_2}{m_1^2} - 1 \right]^{1/2} \quad (2.30)$$

- Spectral peakedness parameter:

$$Q_p = \frac{2}{m_0^2} \int_{f_{min}}^{f_{max}} f \left[S(f) \right]^2 df \quad (2.31)$$

- Standard deviation of free surface displacement:

$$\eta_{rms} = \sqrt{m_0} \quad (2.32)$$

- Root-mean-square wave height:

$$H_{\text{rms}} = \sqrt{8m_0} \quad (2.33)$$

- Significant wave height:

$$H_{\text{mo}} = 4.004\sqrt{m_0} \quad (2.34)$$

- Mean period based on m_1 :

$$T_{01} = \frac{m_0}{m_1} \quad (2.35)$$

- Mean period based on m_2 :

$$T_{02} = \sqrt{\frac{m_0}{m_2}} \quad (2.36)$$

- Spectral Correlated Parameter:

$$\kappa = \frac{1}{m_0} \left\{ \left[\int_{f_{\min}}^{f_{\max}} S(f) \cos(2\pi f T_{02}) df \right]^2 + \left[\int_{f_{\min}}^{f_{\max}} S(f) \sin(2\pi f T_{02}) df \right]^2 \right\}^{1/2} \quad (2.37)$$

In addition, the spectral peak period T_p and the spectral peak frequency $f_p = 1/T_p$, where $S(f)$ is the maximum at $f = f_p$, are given as output. The predominant wave direction corresponding to the maximum value of $D(\theta)$ given by (2.24) is also given as output along with the aforementioned spectral parameters.

2.9 TIME SERIES GENERATION AND PARAMETERS

For the specified or computed frequency spectrum $S(f)$ the corresponding free surface displacement $\eta(t)$, as a function of time t for the duration $0 \leq t \leq t_{\max}$, is generated using the random phase scheme as explained by Cox *et al.* (1991). The generated time series $\eta_n = \eta(t_n)$, where t_n with $n = 1, 2, 3, \dots, NP$ given by (2.7), is analyzed using the zero-upcrossing method as described by Cox *et al.* (1991). The zero-upcrossing wave height and period, denoted by H_i and T_i with $i = 1, 2, 3, \dots, N_o$, are obtained for N_o individual waves. The individual waves are also ranked in descending order of H_i . The wave height and period of the r -th ranked wave are denoted by H_r and T_r , respectively.

The following time series parameters are given as output using the subroutine **TIMPAR** given by Cox *et al.* (1991) and modified herein:

- Mean water level:

$$\bar{\eta} = \frac{1}{NP} \sum_{i=1}^{NP} \eta_i \quad (2.38)$$

- Standard deviation of free surface displacement:

$$\eta_{\text{rms}} = \left[\frac{1}{NP} \sum_{i=1}^{NP} (\eta_i - \bar{\eta})^2 \right]^{1/2} \quad (2.39)$$

- Number of zero-upcrossing waves:

$$N_o = \frac{t_{max}}{\bar{T}} \quad (2.40)$$

- Average wave height:

$$\bar{H} = \frac{1}{N_o} \sum_{i=1}^{N_o} H_i \quad (2.41)$$

- Average wave period:

$$\bar{T} = \frac{1}{N_o} \sum_{i=1}^{N_o} T_i \quad (2.42)$$

- Root-mean-square wave height:

$$H_{\text{rms}} = \left[\frac{1}{N_o} \sum_{i=1}^{N_o} H_i^2 \right]^{1/2} \quad (2.43)$$

- Significant wave height:

$$H_s = \frac{3}{N_o} \sum_{r=1}^{N_o/3} H_r \quad (2.44)$$

- Significant wave period:

$$T_s = \frac{3}{N_o} \sum_{r=1}^{N_o/3} T_r \quad (2.45)$$

- Average height of the one-tenth highest waves:

$$H_{10} = \frac{10}{N_o} \sum_{r=1}^{N_o/10} H_r \quad (2.46)$$

- Average period of the one-tenth highest waves:

$$T_{10} = \frac{10}{N_0} \sum_{r=1}^{N_0/10} T_r. \quad (2.47)$$

In addition, the run length of wave groups is computed. The run length is equal to the number of individual waves in a sequence for which the wave heights are greater than a specified wave height (Goda 1985). This wave height is taken to be the significant wave height H_s herein. The mean run length \bar{j} is defined as

$$\bar{j} = \frac{1}{NK} \sum_{j=1}^{NK} LRN(j) \quad (2.48)$$

where NK = number of runs obtained from N_o wave heights; and $LRN(j)$ = run length of wave heights exceeding H_s . A large mean run length implies that wave heights exceeding H_s appear in groups rather than individually.

2.10 WAVE BREAKING

The linear finite-depth theory used in (2.1) will not be appropriate inside the surf zone since the linear theory does not include wave energy dissipation due to wave breaking. Kobayashi and Wurjanto (1992) used an approximate method based on the empirical criterion of regular wave breaking to ensure that individual waves in the irregular wave train would not break at the shallower water depth h_2 . For the r -th ranked wave whose wave period is T_r , the corresponding breaker height H_b may be estimated using the empirical criterion proposed by Goda (1985), although other criteria may also be applied

$$H_b = 0.17L_o \left\{ 1 - \exp \left[-1.5 \frac{\pi h_2}{L_o} (1 + 15m^{4/3}) \right] \right\} \quad (2.49)$$

with

$$L_o = \frac{gT_r^2}{2\pi} \quad (2.50)$$

where m = the bottom slope at the shallower water depth h_2 . The r -th ranked wave may be assumed to be breaking or broken if its wave height $H_r \geq H_b$. It should be

emphasized that the proposed procedure may not be very accurate since the individual waves in the irregular wave train are not regular waves and the empirical criterion expressed by (2.49) is applicable for regular waves only.

2.11 EQUIVALENT UNI-DIRECTIONAL FREQUENCY SPECTRUM

One way to account for the effects of refraction of directional random waves in a two-dimensional wave flume is to generate an equivalent uni-directional frequency spectrum in the wave flume which will result in the refracted frequency spectrum $S_2(f)$ at the shallower depth h_2 instead of the shoaled uni-directional frequency spectrum $S_2^u(f)$. The equivalent uni-directional frequency spectrum may be generated in any depth greater than h_2 . For simplicity, the equivalent uni-directional frequency spectrum is assumed to correspond to the deeper water depth h_1 and is expressed as

$$S_1^e(f) = \frac{(Cg)_2}{(Cg)_1} S_2(f). \quad (2.51)$$

Linear uni-directional random waves generated using $S_1^e(f)$ at the water depth h_1 will result in the shoaled uni-directional frequency spectrum that should be the same as $S_2(f)$ provided other factors such as nonlinearity and dissipation are negligible.

It should be noted that two-dimensional hydraulic model tests using (2.51) may be justified if the directional energy distribution function $D_2(\theta_2)$ at the shallower depth h_2 is essentially zero except for the very narrow range around $\theta_2 = 0$, corresponding to normal incidence.

Chapter 3

COMPUTER PROGRAM RESHOAL

3.1 INTRODUCTION

The computer program **RESHOAL**, attached in Appendix A, consists of the main program and 21 primary subroutines. The program has been tested on the IBM 3090 running under VM/XA. The program is written in FORTRAN-77 and should run on other systems. Also, **RESHOAL** is written using the SI units for which the gravitational acceleration $g = 9.81m/s^2$. Replacing $g = 9.81m/s^2$ by $g = 32.2ft/s^2$ in the program allows the user to use English units.

RESHOAL is described in detail in the following sections. To minimize the number of input parameters associated with various options, **RESHOAL** computes the entire scope of the program including the shoaling of uni-directional random waves, the refraction of directional random waves, spectral and time series parameters and wave breaking statistics. The typical computation time for each run made in this report was several minutes and the minimization of the computation time is regarded to be secondary. **RESHOAL** is written in a self-explanatory manner to allow modifications without difficulties if necessary.

3.2 INPUT DATA FILE

The execution of **RESHOAL** requires the user to supply one input data file. The program offers the user the freedom to specify the file name, however, the length of

the name is limited to 13 characters. The preparation of the input data file is described in Section 3.6.

3.3 MAIN PROGRAM

The main program lists the parameters and variables contained in the **COMMON** blocks, which are detailed in Section 3.5., and coordinates the computational procedures executed by the subroutines. The procedures can be separated into the following tasks and are explained below:

1. Groundwork.
2. Spectral Calculations.
3. Time Series Calculations.
4. Wave Breaking Calculations.
5. Output and Graphing.

3.3.1 GROUNDWORK

The preliminary tasks performed include

- Reading the input data file.
- Discretization of frequency, direction and time domains as explained in Section 2.2.
- Calculating the wave numbers and their ratios in (2.1), (2.2) and (2.26).
- Calculating the ratios of the group velocities in (2.1), (2.25) and (2.26).

3.3.2 SPECTRAL CALCULATIONS

The following spectral calculations are performed:

1. Incident Frequency Spectrum $S_1(f)$ at deeper depth h_1 given by (2.11).
2. Incident Directional Spectrum $S_1(f, \theta_1)$ at deeper depth h_1 given by (2.23).
3. Directional Energy Distribution Function $D_1(\theta)$ at deeper depth h_1 given by (2.24) using $S_1(f, \theta_1)$.
4. Shoaled Uni-Directional Frequency Spectrum $S_2^u(f)$ at shallower depth h_2 given by (2.25).
5. Frequency Spectrum $S_2(f)$ at shallower depth h_2 given by (2.27).
6. Refracted Directional Spectrum $S_2(f, \theta_2)$ at shallower depth h_2 given by (2.1) and (2.26).
7. Directional Energy Distribution Function $D_2(\theta)$ at shallower depth h_2 given by (2.24) using $S_2(f, \theta_2)$.
8. Equivalent Uni-Directional Frequency Spectrum $S_1^e(f)$ at deeper depth h_1 given by (2.51).
9. Spectral parameters explained in Section 2.8 for the frequency spectra $S_1(f)$, $S_2^u(f)$ and $S_2(f)$.

3.3.3 TIME SERIES CALCULATIONS

The following time series calculations are performed:

1. Three time series corresponding to the three frequency spectra $S_1(f)$, $S_2^u(f)$, and $S_2(f)$ using the random phase scheme.

2. The time series parameters explained in Section 2.9 for the three time series generated numerically.

3.3.4 WAVE BREAKING CALCULATIONS

For the ranked wave heights and periods computed from the three time series, the breaking criterion for the ranked individual waves is evaluated as explained in Section 2.10.

3.3.5 OUTPUT AND GRAPHING

Six output data files are created and used for storing and tabulating the following information:

1. Input Parameters.
2. Spectral Parameters.
3. Time Series Parameters.
4. Ranked Waves and Breaker Heights for Shoaled Uni-Directional Frequency Spectrum.
5. Ranked Waves and Breaker Heights for Frequency Spectrum of Refracted Directional Waves.
6. Run Length Statistics.

Fourteen output data files are created and used for the purposes of plotting the following figures:

1. Incident, Shoaled and Refracted Frequency Spectra versus Frequency.

2. Energy Distribution Functions at depths h_1 and h_2 versus Direction.
3. Time Series of Free Surface Displacement for Incident, Shoaled and Refracted Frequency Spectra.
4. Incident Directional Spectrum versus Frequency and Direction.
5. Refracted Directional Spectrum versus Frequency and Direction.
6. Equivalent Uni-Directional Frequency Spectrum versus Frequency.

These data files are to be utilized by the user to plot the figures as shown in the example in Appendix B. **RESHOAL** *does not* contain plotting routines.

3.4 SUBROUTINES

The 21 primary subroutines arranged in numerical order within the program are listed in Table 1. The page numbers for the subroutines listed in Table 1 correspond to the page numbers for the listing of **RESHOAL** in Appendix A. The subroutines are explained concisely with the following format

Number	Name	Description
--------	------	-------------

, where the

Number

 refers to the numerical order in the program.

01 INPUT1 reads information from the input data file, as explained in Section 3.6.

02 DISCRE computes the frequency, time and directional domains.

03 WAVNUM calculates the wave numbers at depths h_1 and h_2 , k_1 and k_2 , and their ratio k_2/k_1 used in (2.1), (2.2) and (2.26).

04 GRPVEL determines the ratio of the group velocities at depths h_1 and h_2 , $(Cg)_1/(Cg)_2$, used in (2.1), (2.25) and (2.26).

05 TMASPC computes the incident *TMA* frequency spectrum $S_1(f)$ at depth h_1 given by (2.11) where the peak enhancement factor γ is treated as an input

parameter and the specification of the integer **IDEEP** = 1 as input results in $\Phi_K = 1$, corresponding to the JONSWAP spectrum in deep water.

FUNCTION: EJ computes the JONSWAP Spectrum given by (2.13).

06 INTGRL performs integration using Simpson's rule. It is used in **05 TMASPC**, **07 DIRSPC**, **09 REFDIR**, and **11 SPCPAR**.

07 DIRSPC determines the directional variables $G_o(f)$ and $s(f)$ given by (2.22) and (2.21), the directional spectrum $S_1(f, \theta_1)$ given by (2.23) and the energy distribution function $D_1(\theta_1)$ at depth h_1 defined by (2.24) with $S(f, \theta) = S_1(f, \theta_1)$.

FUNCTION: GAMMLN computes the natural log of the gamma function in (2.22) using Press *et al.* (1986).

08 SHOUNI calculates the shoaled, uni-directional frequency spectrum $S_2^u(f)$ at depth h_2 given by (2.25).

09 REFDIR calculates the refracted directional spectrum $S_2(f, \theta_2)$ given by (2.1) and (2.26), the refracted frequency spectrum $S_2(f)$ given by (2.27), and the energy distribution function $D_2(\theta_2)$ at depth h_2 defined as (2.24) with $S(f, \theta) = S_2(f, \theta_2)$. In addition, the equivalent uni-directional frequency spectrum $S_1^c(f)$ at depth h_1 given by (2.51) is computed.

10 FINDMA finds the maximum value for a given function and its location within the function's domain and is used in **08 SHOUNI** and **09 REFDIR**.

11 SPCPAR computes the spectral parameters summarized in Section 2.8 for the incident, shoaled and refracted frequency spectra denoted by $S_1(f)$, $S_2^u(f)$ and $S_2(f)$.

12 TSRIES generates the three time series $\eta(t)$ of the free surface displacements corresponding to the frequency spectra $S_1(f)$, $S_2^u(f)$ and $S_2(f)$ using the

random phase scheme and the inverse Fast Fourier Transform where the same seed value for a random number generator is used for the three time series.

External IMSL Subroutine: **RNSET** sets the random number generator.

External IMSL Subroutine: **RNUN** returns a random number array.

External IMSL Subroutine: **FFT2B** performs an inverse Fast Fourier Transform.

The *IMSL* subroutines **RNSET**, **RNUN**, and **FFT2B** are computationally efficient and are widely available throughout the U.S.A.

- 13 **TIMPAR** calculates the time series parameters summarized in Section 2.9 by the zero-upcrossing method for each time series generated in 12 **TSRIES**.
- 14 **WBREAK** computes the breaker height given by (2.49) for the ranked individual waves for the three time series generated in 12 **TSRIES** and analyzed in 13 **TIMPAR**.
- 15 **OFILES** opens the output files described in Section 3.3.5.
- 16 **TABINP** tabulates the input and discretization parameters and lists the respective output file names.
- 17 **TABSPC** outputs the spectral parameters computed in 11 **SPCPAR**.
- 18 **TABTIM** outputs the time series parameters computed in 13 **TIMPAR**.
- 19 **TABIWS** tabulates the ranked individual waves and the corresponding breaker heights.
- 20 **TABRUN** tabulates the run length statistics for the zero-upcrossing waves.
- 21 **FLFIGS** stores all quantities for plotting purposes.

Table 3.1: LIST OF 21 PRIMARY SUBROUTINES IN COMPUTER PROGRAM RESHOAL.

NO.	SUBROUTINE	PAGE NO.
01	INPUT1	46 - 48
02	DISCRE	48 - 49
03	WAVNUM	49 - 51
04	GRPVEL	51 - 52
05	TMASPC	52 - 55
06	INTGRL	55
07	DIRSPC	55 - 58
08	SHOUNI	58 - 59
09	REFDIR	59 - 61
10	FINDMA	61 - 62
11	SPCPAR	62 - 65
12	TSRIES	65 - 67
13	TIMPAR	67 - 72
14	WBREAK	72 - 73
15	OFILES	73 - 74
16	TABINP	74 - 77
17	TABSPC	77 - 79
18	TABTIM	79 - 80
19	TABIWS	80 - 82
20	TABRUN	82 - 84
21	FLFIGS	84 - 85

3.5 PARAMETERS AND VARIABLES

The **COMMON** blocks in the main program **RESHOAL** are explained in detail in this section providing the user with the necessary information to comprehend the specifics of the program and revise it as desired.

PARAMETER(NF = 2001) **NF** is the odd number of discrete frequencies within the frequency domain $f_{min} \leq f \leq f_{max}$ with $f_{min} = 0$. The user may increase or decrease this parameter to adjust the frequency resolution.

PARAMETER(ND = 181) **ND** is the odd number of discrete directions within the directional domain $-\pi/2 \leq \theta \leq \pi/2$. The user may adjust this parameter

and hence the direction resolution.

PARAMETER(N = 4000) N is the integer used to dimension the number of data points in the time domain $0 \leq t < t_{max}$ and should be equal to or greater than the even number $NP = (2 * NF - 2)$ based on (2.4). If NF is adjusted, N must be adjusted accordingly.

PARAMETER(NDS = 8000) NDS is the integer used to dimension the number of Fourier coefficients.

PARAMETER(NDZ = 500) NDZ is the parameter used to specify the upper limit for the number of zero upcrossing waves, NZ.

/CONST/ contains the following constants.

PI = $\pi=3.141592\dots$

G = gravitational acceleration, $g = 9.81m/s^2$ in the SI units.

/INPUT/ contains the input parameters read from the input data file and one calculated parameter.

H(2) = 1D array containing the deeper water depth h_1 and the shallower water depth h_2 .

HMO1 = spectral estimate of the significant wave height H_{mo} at the depth h_1 .

TP1 = spectral peak period T_p at the depth h_1 .

FP1 = spectral peak frequency at the depth h_1 .

GAM = peak enhancement factor γ of the JONSWAP shape function defined by (2.16).

SMAX = maximum value s_{max} of the directional spreading parameter s at the depth h_1 given by (2.21).

ALPHA1 = predominant incident wave direction at the depth h_1 used in (2.20).

SLOPE = bottom slope m at the depth h_2 used in (2.49).

IS = seed value for the random number generator used to generate the time series of the free surface displacement as discussed in Section 2.9.

IDEEP = water depth identifier for which $\text{IDEEP} = 1$ specifies $\Phi_K = 1$ in (2.11), corresponding to the JONSWAP spectrum in deep water.

For the *TMA* spectrum in finite depth water, set $\text{IDEEP} = 0$.

/OUTPUT/ contains the header information for the output files.

COMMEN1-COMMEN5 are character strings used to contain the input data file's five line header which is used to title the output files.

/DISFRQ/ contains the frequency bandwidth and domain.

DF = frequency bandwidth Δf given by (2.5).

FQ(NF) = 1D array containing the discrete frequency f_j with $j = 1, 2, 3, \dots, NF$ given by (2.6).

/DISTIM/ contains the time domain and related parameters.

NP = even number of data points in the time series used in (2.4).

DT = time step Δt given by (2.8).

TIME(N) = 1D array containing the discrete time level t_n with $n = 1, 2, 3, \dots, NP$ given by (2.7).

/DISDIR/ contains the directional bandwidth and domain.

DD = directional bandwidth $\Delta\theta$ specified by (2.9).

THETA(ND) = 1D array containing the discrete direction θ_i with $i = 1, 2, 3, \dots, ND$ given by (2.10).

/MINMAX/ contains the minimum and maximum frequencies and periods.

FMIN = minimum frequency f_{min} which is set as $f_{min} = 0$.

FMAX = maximum frequency f_{max} specified in Section 2.2.

TMIN = minimum time level t_{min} which is set as $t_{min} = 0$.

TMAX = maximum time level t_{max} which is selected as $t_{max} = 200T_p$.

/WNUMBR/ contains the wave number and group velocity parameters.

WN(2,NF) = 2D array containing the wave numbers k_1 and k_2 computed using (2.3) for each discrete frequency f_j .

WN21(NF) = 1D array containing the ratio k_2/k_1 for each discrete frequency f_j .

CG12(NF) = 1D array containing the ratio $(Cg)_1/(Cg)_2$ of the group velocities at the depths h_1 and h_2 for each discrete frequency f_j .

/FQSPEC/ contains the incident, shoaled, refracted, and equivalent uni-directional frequency spectra.

STMA(NF) = 1D array containing the incident frequency spectrum $S_1(f_j)$ given by (2.11).

SUNI(NF) = 1D array containing the shoaled frequency spectrum $S_2^u(f_j)$ given by (2.25).

SDIR(NF) = 1D array containing the refracted frequency spectrum $S_2(f_j)$ given by (2.27).

SEQU(NF) = 1D array containing the equivalent uni-directional frequency spectrum $S_1^e(f)$ given by (2.51).

/MITSU/ contains the parameters of the directional spreading function $G_1(f, \theta)$ given by (2.20).

S(NF) = 1D array containing the directional spreading parameter $s(f_j)$ given by (2.21).

G0(NF) = 1D array containing the directional spreading parameter $G_o(f_j)$ given by (2.22).

/DIREC1/ contains the directional spectrum and energy distribution function at the deeper depth h_1 .

S1(NF,ND) = 2D array containing the incident directional spectrum $S_1(f_j, \theta_i)$ computed by (2.23).

D1(ND) = 1D array containing the incident directional energy distribution function $D_1(\theta_i)$ defined as (2.24) using $S_1(f, \theta_1)$.

/DIREC2/ contains the directional spectrum and energy distribution function at the shallower depth h_2 .

S2(NF,ND) = 2D array containing the refracted directional spectrum $S_2(f_j, \theta_i)$ given by (2.1) and (2.26).

D2(ND) = 1D array containing the refracted directional energy distribution function $D_2(\theta_i)$ defined as (2.24) using $S_2(f, \theta_2)$.

/PEAKS/ contains the peak frequency, period and predominant wave direction at the shallower depth h_2 .

FPUNI = peak frequency f_p of the shoaled frequency spectrum where $S_2^u(f_j)$ is the maximum.

TPUNI = peak period T_p of the shoaled frequency spectrum which is equal to $1/\text{FPUNI}$.

FPDIR = peak frequency f_p of the refracted frequency spectrum where $S_2(f_j)$ is the maximum.

TPDIR = peak period T_p of the refracted frequency spectrum which is equal to $1/\text{FPDIR}$.

ALPHA2 = predominant wave direction of the refracted directional spectrum where $D_2(\theta_i)$ is the maximum.

/SPCTRM/ contains the three frequency spectra for convenience of programming.

$SP(3,NF)$ = 2D array containing the three frequency spectra such that
 $SP(1,NF) = STMA(NF)$, $SP(2,NF) = SUNI(NF)$ and $SP(3,NF) =$
 $SDIR(NF)$.

/SPECF/ contains the frequency spectral parameters.

$SPECF(3,12)$ = 2D array containing the spectral parameters for the three
frequency spectra as follows:

$EP = SPECF(*,1)$ = spectral width parameter ϵ given by (2.29).

$VU = SPECF(*,2)$ = spectral width parameter ν given by (2.30).

$QP = SPECF(*,3)$ = spectral peakedness parameter Q_p given by (2.31).

$ER = SPECF(*,4)$ = standard deviation of the free surface oscillation, η_{rms}
given by (2.32).

$HR = SPECF(*,5)$ = spectral estimate of the root-mean-square wave height
 H_{rms} given by (2.33).

$HM = SPECF(*,6)$ = spectral estimate of the significant wave height H_{mo}
given by (2.34).

$T1 = SPECF(*,7)$ = spectral estimate of the mean period T_{01} given by (2.35).

$T2 = SPECF(*,8)$ = spectral estimate of the mean period T_{02} given by (2.36).

TP^* = spectral peak period for the three spectra denoted by the following:

$TP1 = SPECF(1,9)$ = peak period at depth h_1 .

$TPUNI = SPECF(2,9)$ = peak period of normally-incident frequency
spectrum at depth h_2 .

$TPDIR = SPECF(3,9)$ = peak period of refracted frequency spectrum
at depth h_2 .

FP^* = spectral peak frequency for the three spectra denoted by the following:

$FP1 = SPECF(1,10)$ = peak frequency at depth h_1 .

$FPUNI = SPECF(2,10)$ = peak frequency of normally-incident frequency
spectrum at depth h_2 .

$FPDIR = SPECF(3,10)$ = peak frequency of refracted frequency spectrum

at depth h_2 .

ALPHA* = predominant incident wave direction denoted by the following:

ALPHA1 = **SPECP(1,11)** = predominant incident wave direction at depth h_1 .

ALPHA2 = **SPECP(2,11)** = predominant incident wave direction for normally incident frequency spectrum at depth h_2 which is equal to zero.

ALPHA2 = **SPECP(3,11)** = predominant incident wave direction at depth h_2 .

KP = **SPECP(*,12)** = spectral correlated parameter given by (2.37).

/SERIES/ contains the three time series generated numerically for the three frequency spectra.

TS(3,N) = 2D array containing the three time series of the free surface displacement $\eta(t_n)$ such that **TS(1,N)** = $\eta_1(t_n)$ for $S_1(f_j)$, **TS(2,N)** = $\eta_2^u(t_n)$ for $S_2^u(f_j)$, and **TS(3,N)** = $\eta_2(t_n)$ for $S_2(f_j)$.

/UPCROS/ contains the ranked time series parameters.

NZ(3) = 1D array containing the number N_o of zero upcrossing waves for the three time series in sequence of $\eta_1(t_n)$, $\eta_2^u(t_n)$ and $\eta_2(t_n)$.

HRK(3,NDZ) = 2D array containing the ranked wave heights H_r with $r = 1, 2, 3, \dots, N_o$ for the three time series.

TRK(3,NDZ) = 2D array containing the wave periods T_r associated with the ranked wave heights for the three time series.

NK(3) = 1D array containing the number NK of runs for the three time series.

LRN(3,NDZ) = 2D array containing the run length $LRN(j)$ with $j = 1, 2, 3, \dots, NK$ of wave heights exceeding the significant wave height H_s for the three time series.

/TIMEPR/ contains the time series parameters.

TIMEP(3,12) = 2D array containing the time series parameters for the three time series as follows:

SD = **TIMEP(*,1)** = mean water level $\bar{\eta}$ given by (2.38).

ER = **TIMEP(*,2)** = standard deviation of the free surface displacement η_{rms} given by (2.39).

NZ = **TIMEP(*,3)** = number of zero upcrossings N_0 given by (2.40).

HB = **TIMEP(*,4)** = average wave height \bar{H} given by (2.41).

TB = **TIMEP(*,5)** = average wave period \bar{T} given by (2.42).

HV = **TIMEP(*,6)** = root-mean-square wave height H_{rms} given by (2.43).

HS = **TIMEP(*,7)** = significant wave height, *i.e.*, the average of the one-third highest waves, H_s , given by (2.44).

T3 = **TIMEP(*,8)** = significant wave period, *i.e.*, the average period of the one-third highest waves, T_s , given by (2.45).

HT = **TIMEP(*,9)** = average height of the one-tenth highest waves, H_{10} , given by (2.46).

TT = **TIMEP(*,10)** = average period of the one-tenth highest waves, T_{10} , given by (2.47).

NK = **TIMEP(*,11)** = number of runs exceeding the significant wave height, H_s .

\bar{J} = **TIMEP(*,12)** = mean run length given by (2.48).

/WAVEBK/ contains the individual wave breaking statistics.

HBREAK(3,NDZ) = 2D array containing the breaker heights H_b given by (2.49) for each ranked wave for the shoaled time series $\eta_2^u(t_n)$ and the refracted time series $\eta_2(t_n)$.

IBREAK(3,NDZ) = 2D array containing the breaker indicator of each ranked wave for the shoaled and refracted time series. **IBREAK** = 1 for $H_r \geq H_b$,

that is, breaking of the r -th ranked wave. $\text{IBREAK} = 0$ for $H_r < H_b$,
that is, no breaking of the r -th ranked wave.

3.6 FORMATTING AND READING THE INPUT DATA FILE

The input data file is read by Subroutine **01 INPUT1**. This section describes the input format so the user will be able to prepare the input data file easily.

3.6.1 FILE NAME

RESHOAL allows the user to name the input data file **FILENM**, **UNIT = 10**. The file name is limited to thirteen characters and is read in as follows:

```
CHARACTER*13 FILENM
```

```
•  
•  
•
```

```
C REQUEST INPUT FILE NAME
```

```
WRITE(*,*) 'ENTER INPUT FILE NAME AND EXTENSION'
```

```
READ(*,10) FILENM
```

```
•  
•  
•
```

```
10  FORMAT(A13)
```

3.6.2 HEADER

The first five lines of the input file shall contain header information **COMMEN1**, **COMMEN2**, **COMMEN3**, **COMMEN4** and **COMMEN5**. This header is then written to the output files for titling purposes. The header lines are limited to

thirty characters each and are read in as follows:

```

      CHARACTER*30 COMMEN1,COMMEN2,COMMEN3,
      COMMEN4,COMMEN5
      •
      •
      •
C      READ HEADER
      READ(10,20) COMMEN1
      READ(10,20) COMMEN2
      READ(10,20) COMMEN3
      READ(10,20) COMMEN4
      READ(10,20) COMMEN5
      •
      •
      •
20    FORMAT(A30)

```

3.6.3 INPUT DATA

Following the header in the data file, the input parameters shall be specified in the following order:

- $H(M)$ = water depths denoted by $H(1) = h_1$ and $H(2) = h_2$
- $HMO1$ = spectral estimate of the significant wave height H_{m0} at the depth h_1
- $TP1$ = spectral peak period T_p at the depth h_1
- GAM = peak enhancement factor γ of the JONSWAP shape function
- $IDEEP$ = water depth identifier

- **SMAX** = maximum value s_{max} of the directional spreading parameter s at the depth h_1
- **ALPHA1** = predominant incident wave direction at the depth h_1
- **SLOPE** = bottom slope m at the depth h_2
- **IS** = seed value for the random number generator.

RESHOAL reads in these parameters as follows:

```
READ(10,*) (H(M), M=1,2)
```

```
READ(10,*) HMO1,TP1
```

```
READ(10,*) GAM,IDEEP
```

```
READ(10,*) SMAX,ALPHA1
```

```
READ(10,*) SLOPE
```

```
READ(10,*) IS
```

3.7 OUTPUT DATA FILES

Subroutine **15 OFILES** opens all the output files for storing and tabulating data and are listed below. Note, each output data file contains the header described in Section 3.6.2.

INPUT is an output data file listing the input parameters and preset variables described in Sections 2.2 and 3.6.3 and placed in the following order:

- **H(1)** = the deeper depth h_1 (m)
- **H(2)** = the shallower depth h_2 (m)

- **HMO1** = spectral estimate of the significant wave height H_{mo} at the depth h_1 (m)
- **TP1** = spectral peak period T_p at the depth h_1 (s)
- **GAM** = peak enhancement factor γ of the JONSWAP shape function
- **IDEEP** = water depth identifier
- **SMAX** = maximum value s_{max} of the directional spreading parameter s at the depth h_1
- **ALPHA1** = predominant incident wave direction at the depth h_1 (deg)
- **SLOPE** = bottom slope m at the depth h_2
- **IS** = seed value for the random number generator
- **NF** = number of discrete frequencies
- **ND** = number of discrete directions
- **FMIN** = lower bound of the frequency domain set equal to zero (Hz)
- **FMAX** = upper bound of the frequency domain (Hz)
- **TMIN** = lower bound of the directional domain set equal to -90°
- **TMAX** = upper bound of the directional domain set equal to 90° .

FQ is an output file containing the frequency domain **FQ(J)** where $J = 1, 2, 3, \dots, NF$ calculated in Section 2.2 for plotting purposes.

ANG is an output file containing the directional domain **THETA(I)** where $I = 1, 2, 3, \dots, ND$ calculated in Section 2.2 for plotting purposes.

TIME is an output file containing the time domain **TIME(K)** where $K = 1, 2, 3, \dots, NP$ calculated in Section 2.2 for plotting purposes.

SPECP is an output data file listing the spectral parameters described in Section 2.8 for the three frequency spectra and specified below:

- SPECP(*,1) = spectral width parameter ϵ
- SPECP(*,2) = spectral width parameter ν
- SPECP(*,3) = spectral peakedness parameter Q_p
- SPECP(*,4) = standard deviation of the free surface oscillation, η_{rms}
- SPECP(*,5) = spectral estimate of the root-mean-square wave height H_{rms}
- SPECP(*,6) = spectral estimate of the significant wave height H_{mo}
- SPECP(*,7) = spectral estimate of the mean period T_{01}
- SPECP(*,8) = spectral estimate of the mean period T_{02}
- SPECP(*,9) = peak period of the frequency spectrum
- SPECP(*,10) = peak frequency of the frequency spectrum
- SPECP(*,11) = predominant incident wave direction of the frequency spectrum
- SPECP(*,12) = spectral correlated parameter κ

TIMEP is an output data file listing the time series parameters described in Section 2.9 for the three time series and specified below:

- TIMEP(*,1) = mean water level $\bar{\eta}$
- TIMEP(*,2) = standard deviation of the free surface displacement, η_{rms}
- TIMEP(*,3) = number of zero upcrossings, N_0
- TIMEP(*,4) = average wave height \bar{H}

- TIMEP(*,5) = average wave period \bar{T}
- TIMEP(*,6) = root-mean-square wave height H_{rms}
- TIMEP(*,7) = significant wave height, *i.e.*, average of one-third highest waves, H_s
- TIMEP(*,8) = significant wave period, *i.e.*, average period of one-third highest waves, T_s
- TIMEP(*,9) = average height of the one-tenth highest waves, H_{10}
- TIMEP(*,10) = average period of the one-tenth highest waves, T_{10}
- TIMEP(*,11) = number of runs exceeding the significant wave height H_s
- TIMEP(*,12) = mean run length

UNIBRK is an output data file listing the ranked waves and breaker heights for the incident versus shoaled uni-directional frequency spectra described in Sections 2.9 and 2.10 and specified below:

- TRK(1,NZ) = wave periods T_r associated with the ranked wave heights for the incident frequency spectrum
- HRK(1,NZ) = ranked wave heights H_r for the incident frequency spectrum
- TRK(2,NZ) = wave periods T_r associated with the ranked wave heights for the shoaled uni-directional frequency spectrum
- HRK(2,NZ) = ranked wave heights H_r for the shoaled uni-directional frequency spectrum
- HBREAK(2,NZ) = breaker heights for the shoaled uni-directional frequency spectrum

- **IBREAK(2,NZ)** = breaker indicator for the shoaled uni-directional frequency spectrum

DIRBRK is an output data file listing the ranked waves and breaker heights for the incident versus refracted directional frequency spectra described in Sections 2.9 and 2.10. The format for **DIRBRK** is the same as for **UNIBRK** except that the shoaled uni-directional frequency spectrum is replaced by the refracted directional frequency spectrum.

RUNLTH is an output data file listing the run length statistics described in Section 2.9 for the three time series and specified below:

- **LRN(*,NK)** = run length of wave heights exceeding H_s
- **TIMEP(*,12)** = mean run length

STMA is an output file containing the *TMA* frequency spectrum **STMA(J)** where $J = 1,2,3,\dots,NF$ at depth h_1 described in Section 2.3 for plotting purposes.

SUNI is an output file containing the shoaled uni-directional frequency spectrum **SUNI(J)** where $J = 1,2,3,\dots,NF$ at depth h_2 described in Section 2.6 for plotting purposes.

SDIR is an output file containing the refracted frequency spectrum **SDIR(J)** where $J = 1,2,3,\dots,NF$ at depth h_2 described in Section 2.7 for plotting purposes.

SEQU is an output file containing the equivalent uni-directional frequency spectrum **SEQU(J)** where $J = 1,2,3,\dots,NF$ at depth h_1 described in Section 2.11 for plotting purposes.

D1 is an output file containing the directional energy distribution function **D1(I)** where $I = 1,2,3,\dots,ND$ at depth h_1 described in Section 2.5 for plotting purposes.

D2 is an output file containing the directional energy distribution function **D2(I)** where **I = 1,2,3,...,ND** at depth h_2 described in Section 2.5 for plotting purposes.

DIRSP1 is an output file containing the directional spectrum **S1(J,I)** where **J = 1,2,3,...,NF** and **I = 1,2,3,...,ND** at depth h_1 described in Section 2.4 for plotting purposes.

DIRSP2 is an output file containing the directional spectrum **S2(J,I)** where **J = 1,2,3,...,NF** and **I = 1,2,3,...,ND** at depth h_2 described in Sections 2.1 and 2.7 for plotting purposes.

TS1 is an output file containing the time series for the incident frequency spectrum, **TS(1,K)**, where **K = 1,2,3,...,NP** at depth h_1 described in Section 2.9 for plotting purposes.

TS2 is an output file containing the time series for the shoaled uni-directional frequency spectrum, **TS(2,K)**, where **K = 1,2,3,...,NP** at depth h_2 described in Section 2.9 for plotting purposes.

TS3 is an output file containing the time series for the refracted frequency spectrum, **TS(3,K)**, where **K = 1,2,3,...,NP** at depth h_2 described in Section 2.9 for plotting purposes.

3.8 USER MODIFICATONS

Subroutine **15 OFILES** may be revised by the user to rename any or all of the output file names. The extension **OUT** for data files and **DATA** for plotting files was chosen specifically for the authors' computer system and should be revised as necessary. Also, Subroutines 16 through 21 may be amended to reformat the output files.

The number of frequencies used throughout **RESHOAL** is specified in the main program using the **PARAMETER** statement, **PARAMETER(NF= 2001)**. To

increase or decrease the number of frequencies, the user must modify this **PARAMETER** statement appearing in the main program and Subroutines 02 through 05, 07 through 09, 11, 12, 16 and 21. Accordingly, the number of data points, **NP**, equal to $(2*NF-2)$, will change and the user must adjust the **PARAMETER** statement, **PARAMETER(N = 4000)**, appearing in the main program and Subroutines 02, 12, 13, 16 and 21 in suit. Also, the parameter **NDS** equal to $(2*NP)$ used in the FFT routines will have to increase or decrease as necessary in the main program and subroutines 12 and 13.

Similarly, the user may increase or decrease the directional resolution, **NDRESHOAL** contains a 1° angular step corresponding to **ND** equal to 181. The **PARAMETER** statement, **PARAMETER(ND = 181)**, appearing in the main program and Subroutines 02, 07, 09, 11, 16 and 21, should be revised as necessary.

The dimensioning for the arrays containing the number of zero upcrossing waves may have to be adjusted depending upon the length of the time domain set to be **200TP1**. A dimension size of 500 should be sufficient. The **PARAMETER** statement, **PARAMETER(NDZ = 500)** appears in the main program and in subroutines 13, 14, 19 and 20.

Subroutine **02 DISCRE** may be modified to alter the upper and lower bounds of the discretized domains. The minimum and maximum frequencies are preset to 0 and $10/TP1$, respectively. The directions $-\pi/2$ and $\pi/2$ parallel to the straight shoreline establish the physical lower and upper bounds on the directional domain. The user may revise these limits if necessary.

Chapter 4

CONCLUSIONS AND RECOMMENDATIONS

The computer program **RESHOAL** computes the directional random wave spectrum in specified shallower water depth for given incident directional random wave spectrum in deeper water depth using linear finite-depth theory for straight shorelines with parallel bottom contours. The incident directional random wave spectrum is simply assumed to be given by the product of the *TMA* frequency spectrum and the Mitsuyasu-type directional spreading function since incident directional random wave data may not be available for practical applications. Although the linear finite-depth theory is well established, the user-friendly computer program **RESHOAL** with the minimum input and various output will allow more routine applications of this theory.

RESHOAL is limited to straight shorelines with parallel bottom contours and can not be applied to complex bathymetry. The linear finite-depth theory is limited to the region outside the surf zone in which cumulative effects of wind and bottom friction are negligible. The linear theory has been shown to be reasonably accurate in predicting the gross wave characteristics such as the spectral estimate of the significant wave height. The linear theory may not predict the details of the wave spectra since it does not account for the generation of higher and lower harmonics due to nonlinear wave-wave interactions.

RESHOAL may be sufficient for determining the representative wave height and period used for the current design procedures of coastal structures, although other

wave characteristics such as the spectral shape and wave grouping are being investigated to improve the specification of design waves.

The applications of **RESHOAL** are given in Appendices B and C in relation to field data and generation of equivalent uni-directional frequency spectra in a two-dimensional wave flume. **RESHOAL** may be used to estimate the incident random waves required as input to other numerical models developed for the design of coastal structures. The use of the equivalent uni-directional frequency spectra in the two-dimensional model tests has been examined by Poff and Kobayashi (1993).

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Appendix A

LISTING OF COMPUTER PROGRAM RESHOAL

```
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
C                                                                 C
C      RESHOAL:  PROGRAM RESHOAL COMPUTES THE SHOALING AND      C
C      REFRACTION OF DIRECTIONAL RANDOM WAVES PROPAGATING ONTO  C
C      A STRAIGHT SHORELINE WITH PARALLEL BOTTOM CONTOURS      C
C                                                                 C
C      WRITTEN BY MICHAEL POFF AND NOBUHISA KOBAYASHI          C
C      CENTER FOR APPLIED COASTAL RESEARCH, UNIVERSITY OF DELAWARE  C
C      JULY, 1993                                             C
C                                                                 C
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC

C      PARAMETERS
C      -----
C      NAME              DESCRIPTION
C      -----
C      PARAMETER(NF=2001) NF is the number of frequencies within the fre-
C      quency domain.
C      PARAMETER(ND=181) ND is the number of directions within the direc-
C      tional domain.
C      PARAMETER(N=4000) N is the integer used to dimension the time
C      domain.
C      PARAMETER(NDS=8000) NDS is the integer used to dimension the
C      number of Fourier Coefficients.
C      PARAMETER(NDZ=500) NDZ is the upper limit of the number of zero-
C      upcrossing waves in the time domain.
C
C      COMMONs
C      -----
C      NAME      CONTENTS
C      -----
C      /CONST/  contains constants.
```

C /INPUT/ contains input parameters read from the input data file
 C and one calculated parameter.
 C /OUTPUT/ contains header information for output files.
 C /DISFRQ/ contains the frequency domain and related variables.
 C /DISTIM/ contains the time domain and related variables.
 C /DISDIR/ contains the directional domain and related variables.
 C /MINMAX/ contains the minimum and maximum frequencies and time
 C levels.
 C /WNUMBR/ contains the wave number and group velocity variables.
 C /FQSPEC/ contains the incident, shoaled, refracted, and equivalent
 C uni-directional frequency spectra.
 C /MITSU/ contains the directional spreading parameters.
 C /DIREC1/ contains the directional spectrum and energy distribution
 C function at deeper depth one.
 C /DIREC2/ contains the directional spectrum and energy distribution
 C function at shallower depth two.
 C /PEAKS/ contains the peak frequencies, periods and predominant
 C wave direction at shallower depth two.
 C /SPCTRM/ contains all three frequency spectra for use in Sub-
 C routines 11 SPCPAR and 12 TSRIES.
 C /SPECP/ contains the frequency spectral parameters.
 C /SERIES/ contains the three time series generated for the three
 C frequency spectra.
 C /UPCROS/ contains the ranked wave parameters and wave group
 C statistics.
 C /TIMEPR/ contains the time series parameters for the three time
 C series.
 C /WAVEBK/ contains the breaker height for the ranked waves.

C INITIALIZE & DIMENSION VARIABLES/COMMON STATEMENTS

PARAMETER (NF=2001)
 PARAMETER (ND=181)
 PARAMETER (N=4000)
 PARAMETER (NDS=8000)
 PARAMETER (NDZ=500)
 CHARACTER*30 COMMEN1,COMMEN2,COMMEN3,COMMEN4,COMMEN5

C PROVIDE IMSL WORKSPACE

REAL RWKSP(32056)
 COMMON/WORKSP/RWKSP

COMMON/CONST/PI,G
 COMMON/INPUT/H(2),HMO1,TP1,FP1,GAM,SMAX,ALPHA1,SLOPE,IS,IDEEP
 COMMON/OUTPUT/COMMEN1,COMMEN2,COMMEN3,COMMEN4,COMMEN5

```

COMMON/DISFRQ/DF , FQ(NF)
COMMON/DISTIM/NP , DT , TIME(N)
COMMON/DISDIR/DD , THETA (ND)
COMMON/MINMAX/FMIN , FMAX , TMIN , TMAX
COMMON/WNUMBR/WN(2 , NF) , WN21(NF) , CG12(NF)
COMMON/FQSPEC/STMA(NF) , SUNI(NF) , SDIR(NF) , SEQU(NF)
COMMON/MITSU/S(NF) , GO(NF)
COMMON/DIREC1/S1(NF , ND) , D1(ND)
COMMON/DIREC2/S2(NF , ND) , D2(ND)
COMMON/PEAKS/FPUNI , TPUNI , FPDIR , TPDIR , ALPHA2
COMMON/SPCTRM/SP(3 , NF)
COMMON/SPECP/SPECP(3 , 12)
COMMON/SERIES/TS(3 , N)
COMMON/UPCROS/NZ(3) , HRK(3 , NDZ) , TRK(3 , NDZ) , NK(3) , LRN(3 , NDZ)
COMMON/TIMEPR/TIMEP(3 , 12)
COMMON/WAVEBK/HBREAK(3 , NDZ) , IBREAK(3 , NDZ)

```

```

C   CALL TO IMSL WORKSPACE
C   CALL IWKIN(32056)

```

```

C   CONSTANTS

```

```

C           PI=3.14159...
C   PI=4.*ATAN(1.)
C           G=9.81 (m/s^2)=GRAVITATIONAL ACCELERATION
C   G=9.81

```

```

C   SPECIFY INPUT VALUES USING 01 INPUT1
C   CALL INPUT1

```

```

C   CALCULATE FREQUENCY, TIME AND DIRECTIONAL DOMAINS USING 02 DISCRE
C   CALL DISCRE

```

```

C   CALCULATE RATIO OF WAVE NUMBERS AT DEPTHS 1 & 2 USING 03 WAVNUM
C   CALL WAVNUM

```

```

C   CALCULATE RATIO OF GROUP VELOCITIES USING 04 GRPVEL
C   CALL GRPVEL

```

```

C   CALCULATE FREQUENCY SPECTRUM AT DEPTH 1 USING 05 TMASPC
C   CALL TMASPC

```

```

C   CALCULATE DIRECTIONAL SPREADING PARAMETERS, SPECTRUM AND
C   ENERGY DISTRIBUTION FUNCTION AT DEPTH 1 USING 07 DIRSPC
C   CALL DIRSPC

```

```

C CALCULATE SHOALED UNIDIRECTIONAL FREQUENCY SPECTRUM AT DEPTH 2
C USING 08 SHOUNI
  CALL SHOUNI

C CALCULATE DIRECTIONAL SPECTRUM AT DEPTH 2 USING 09 REFDIR
  CALL REFDIR

C CALCULATE SPECTRAL PARAMETERS USING 11 SPCPAR
  CALL SPCPAR

C CALCULATE TIME SERIES USING 12 TSRIES
  CALL TSRIES

C CALCULATE TIME SERIES PARAMETERS USING 13 TIMPAR
  CALL TIMPAR

C CALCULATE BREAKING HEIGHTS AND INDICATORS USING 14 WBREAK
  CALL WBREAK

C OUTPUT USING SUBROUTINES 15-21
  CALL OFILES
  CALL TABINP
  CALL TABSPC
  CALL TABTIM
  CALL TABIWS
  CALL TABRUN
  CALL FLFIGS

  END

```

```

CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
C          SUBROUTINES & FUNCTIONS          C
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC

```

```

CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
C          SUBROUTINE 01 CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
C          C
C INPUT1 C
C C
C READS INPUT PARAMETERS FOR PROGRAM RESHOAL FROM USER SPECIFIED C
C INPUT DATA FILE (UNIT=10) C
C C
C IN/OUT: C
C H(M).....WATER DEPTHS 1 & 2 (M=1,2) (M) C

```

```

C   HMO1.....SPECTRAL ESTIMATE OF SIGNIFICANT WAVE HEIGHT AT      C
C           DEPTH 1 (M)                                           C
C   TP1.....PEAK PERIOD AT DEPTH 1 (S)                             C
C   GAM.....PEAK ENHANCEMENT FACTOR OF JONSWAP SPECTRUM          C
C   IDEEP.....WATER DEPTH IDENTIFIER: SET IDEEP=1 FOR DEEP WATER  C
C           SPECTRUM                                              C
C   SMAX.....MAX. VALUE OF DIRECTIONAL SPREADING PARAMETER, S,    C
C           AT DEPTH 1                                           C
C   ALPHA1.....PREDOMINANT INCIDENT WAVE DIRECTION AT DEPTH 1 (RAD)C
C   SLOPE.....BOTTOM SLOPE AT DEPTH 2                             C
C   IS.....SEED VALUE FOR RANDOM NO. GENERATOR                   C
C                                                                 C
C           OUT:                                                 C
C   FP1.....PEAK FREQUENCY AT DEPTH 1 (HZ)                         C
C                                                                 C
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC

```

SUBROUTINE INPUT1

```

C INITIALIZE & DIMENSION VARIABLES/COMMON STATEMENTS:
  CHARACTER*13 FILENM
  CHARACTER*30 COMMEN1,COMMEN2,COMMEN3,COMMEN4,COMMEN5
  COMMON/INPUT/H(2),HMO1,TP1,FP1,GAM,SMAX,ALPHA1,SLOPE,IS,IDEEP
  COMMON/OUTPUT/COMMEN1,COMMEN2,COMMEN3,COMMEN4,COMMEN5

C REQUEST INPUT FILE NAME (UNIT=10)
  WRITE(*,*) 'ENTER INPUT FILE NAME AND EXTENSION'
  READ(*,10) FILENM

C OPEN INPUT DATA FILE
  OPEN(UNIT=10,FILE=FILENM)

C           READ HEADER
  READ(10,20) COMMEN1
  READ(10,20) COMMEN2
  READ(10,20) COMMEN3
  READ(10,20) COMMEN4
  READ(10,20) COMMEN5

C           READ INPUT PARAMETERS
C           WATER DEPTHS 1 & 2
  READ(10,*) (H(M),M=1,2)

C           SIGN WAVE HT & PEAK PERIOD AT DEPTH 1
  READ(10,*) HMO1,TP1

C           SPECTRAL PARAMETER GAMMA & WATER DEPTH

```



```

C NOTE:  PARAMETERS MUST BE ADJUSTED ACCORDINGLY
PARAMETER (NF=2001)
PARAMETER (ND=181)
PARAMETER (N=4000)
COMMON/CONST/PI,G
COMMON/INPUT/H(2),HMO1,TP1,FP1,GAM,SMAX,ALPHA1,SLOPE,IS,IDEEP
COMMON/DISFRQ/DF,FQ(NF)
COMMON/DISTIM/NP,DT,TIME(N)
COMMON/DISDIR/DD,THETA(ND)
COMMON/MINMAX/FMIN,FMAX,TMIN,TMAX

C DISCRETIZE FREQUENCY DOMAIN
FMIN= 0.0
FMAX= 10./TP1
DF=(FMAX-FMIN)/(FLOAT(NF)-1.)

DO 100 J=1,NF
  FQ(J)=FMIN+(FLOAT(J)-1.)*DF
100 CONTINUE

C CALCULATE TIME DOMAIN FOR SUBSEQUENT TIME SERIES COMPUTATIONS
NP=2*NF-2
DT=1./(2.*FMAX)
TIMEMIN=0.

DO 200 K=1,NP
  TIME(K)=TIMEMIN+(FLOAT(K)-1.)*DT
200 CONTINUE

C DISCRETIZE DIRECTIONAL DOMAIN AT DEPTH 2
C                                     THETA RANGES FROM -PI/2 TO PI/2
TMAX=PI/2.
TMIN=-PI/2.

C                                     FOR 1 DEGREE INCREMENT
DD=(TMAX-TMIN)/(FLOAT(ND)-1.)

DO 300 I=1,ND
  THETA(I)=TMIN+(FLOAT(I)-1.)*DD
300 CONTINUE

RETURN
END

```

```

CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC SUBROUTINE 03 CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC

```

```

C
C WAVNUM
C
C COMPUTES WAVE NUMBERS AT DEPTHS 1 & 2 AND THEIR RATIO
C THIS SUBROUTINE IS AN IMPROVED VERSION OF THE SUBROUTINE WAVNUM IN
C COX ET AL. (1991) TO COMPUTE A WAVE NUMBER
C
C      IN:
C      FQ(NF).....FREQUENCY (HZ)
C      H(M).....WATER DEPTHS 1 & 2 (M)
C
C      OUT:
C      WN(M,NF)....WAVE NUMBER FOR SPECIFIED FQ(NF) AT DEPTHS
C                1 & 2 (1/M)
C      WN21(NF)....RATIO OF WAVE NUMBERS AT DEPTHS 2 & 1
C
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC

```

SUBROUTINE WAVNUM

```

C INITIALIZE & DIMENSION VARIABLES/COMMON STATEMENTS:
  PARAMETER (NF=2001)
  COMMON/CONST/PI,G
  COMMON/INPUT/H(2),HM01,TP1,FP1,GAM,SMAX,ALPHA1,SLOPE,IS,IDEEP
  COMMON/DISFRQ/DF,FQ(NF)
  COMMON/WNUMBR/WN(2,NF),WN21(NF),CG12(NF)

  DO 100 M=1,2
    DO 200 J=1,NF
      SIG=2.*PI*FQ(J)
      R=SIG**2*H(M)/G
      IF(R.GE.10.)THEN
        WN(M,J)=R/H(M)
        GO TO 200
      ENDIF
      IF(R.LE.1.E-8)THEN
        WN(M,J)=SQRT(R)/H(M)
        GO TO 200
      ENDIF
      IF(R.GE.1.)THEN
        X=R
      ELSE
        X=SQRT(R)
      ENDIF
    
```



```

C   STMA(NF).....FREQUENCY SPECTRUM AT DEPTH 1 (M*M*S)           C
C                                                                 C
C   INTERNAL FUNCTION SUBROUTINE:  EJ(FQ,FP)                       C
C                                                                 C
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC

```

SUBROUTINE TMASPC

```

C INITIALIZE & DIMENSION VARIABLES/COMMON STATEMENTS:
  PARAMETER (NF=2001)
  COMMON/INPUT/H(2),HMO1,TP1,FP1,GAM,SMAX,ALPHA1,SLOPE,IS,IDEEP
  COMMON/CONST/PI,G
  COMMON/DISFRQ/DF,FQ(NF)
  COMMON/WNUMBR/WN(2,NF),WN21(NF),CG12(NF)
  COMMON/FQSPEC/STMA(NF),SUNI(NF),SDIR(NF),SEQU(NF)

C SET AP=1 AND COMPUTE ITS VALUE LATER FOR GIVEN HMO1
  AP=1.

C SET FREQUENCY SPECTRUM=0 FOR J=1, THAT IS, ZERO FREQUENCY
  STMA(1)=0.

C SET PHIK = 1.0 IN DEEP WATER (IDEEP=1) AND COMPUTE JONSWAP SPECTRUM
  IF(IDEEP.EQ.1)THEN
    PHIK=1.
    DO 50 J=2,NF
      STMA(J)=AP*EJ(FQ(J),FP1)*PHIK
50    CONTINUE
  ELSE
C OTHERWISE COMPUTE PHIK AND TMA SPECTRUM FOR FINITE DEPTH
    DO 100 J=2,NF
      AKH=WN(1,J)*H(1)
      AKH2=AKH*2.
C LIMIT FOR SINH(ARG), ARG<150
      IF(AKH2.GT.150.)THEN
        PHIK=1.
      ELSE
        PHIK=(TANH(AKH)**2/(1.+AKH2/SINH(AKH2)))
      ENDIF
      STMA(J)=AP*EJ(FQ(J),FP1)*PHIK
100   CONTINUE
    ENDIF

C COMPUTE ALPHA AND RECOMPUTE STMA(NF)

```

```

CALL INTGRL(STMA,NF,DF,ZM)
AP=HMO1**2/(4.004**2*ZM)
DO 200 J=1,NF
  STMA(J)=AP*STMA(J)
200 CONTINUE

RETURN
END

C  INTERNAL FUNCTION SUBROUTINE EJ:  COMPUTES JONSWAP SPECTRUM
C
C      IN:
C      FQ.....FREQUENCY (HZ)
C      FP.....PEAK FREQUENCY (HZ)
C
C      OUT:
C      EJ.....JONSWAP SPECTRUM

REAL FUNCTION EJ(FQ,FP)

C  INITIALIZE & DIMENSION VARIABLES/COMMON STATEMENTS:
COMMON/CONST/PI,G
COMMON/INPUT/H(2),HMO1,TP1,FP1,GAM,SMAX,ALPHA1,SLOPE,IS,IDEEP
TWOPI=2.*PI
SIGA=0.07
SIGB=0.09

C  CALCULATE EP
C1=G**2*TWOPI**(-4)
EP=C1*FQ**(-5)
C  CALCULATE PHIPM
C=1.25*(FQ/FP)**(-4)
IF(C.GT.150.)THEN
  C=150.
ENDIF
PHIPM=EXP(-C)
C  JONSWAP SHAPE FUNCTION
IF(FQ.LE.FP)THEN
  SIG=SIGA
ELSE
  SIG=SIGB
ENDIF
C2=(1./(2.*SIG**2))*(FQ/FP-1.)**2
IF(C2.GT.150.)THEN

```



```

C
C COMPUTES DIRECTIONAL SPREADING PARAMETERS, SPECTRUM AND ENERGY
C DISTRIBUTION FUNCTION AT DEEPER WATER DEPTH 1
C
C      IN:
C      NF.....NO. OF DISCRETE FREQUENCIES
C      FQ(NF).....FREQUENCY DOMAIN (HZ)
C      FP1.....PEAK FREQUENCY AT DEPTH 1 (HZ)
C      SMAX.....MAXIMUM DIRECTIONAL SPREADING PARAMETER
C      ND.....NO. OF DISCRETE DIRECTIONS
C      THETA(ND)....DIRECTIONAL DOMAIN AT DEPTH 1 (RADS)
C      ALPHA1.....PREDOMINANT INCIDENT WAVE DIRECTION AT DEPTH 1 (RAD)
C      STMA(NF)....FREQUENCY SPECTRUM AT DEPTH 1 (M**M*S)
C      DF.....FREQUENCY BANDWIDTH (DELTA F) (HZ)
C
C      OUT:
C      S(NF).....DIRECTIONAL SPREADING PARAMETER
C      GO(NF).....PARAMETER FOR DIRECTIONAL SPREADING FUNCTION
C      S1(NF,ND)....DIRECTIONAL SPECTRUM AT DEPTH 1 (M**M*S/RAD)
C      D1(ND).....DIRECTIONAL ENERGY DISTRIBUTION FUNCTION
C                   AT DEPTH 1 (M**2/RAD)
C
C      INTERNAL FUNCTION SUBROUTINE:  GAMMLN(XX)
C
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC

```

SUBROUTINE DIRSPC

```

C INITIALIZE & DIMENSION VARIABLES/COMMON STATEMENTS:
  PARAMETER(NF=2001)
  PARAMETER(ND=181)
  DIMENSION SINTER(NF)
  COMMON/INPUT/H(2),HMO1,TP1,FP1,GAM,SMAX,ALPHA1,SLOPE,IS,IDEEP
  COMMON/CONST/PI,G
  COMMON/DISFRQ/DF,FQ(NF)
  COMMON/DISDIR/DD,THETA(ND)
  COMMON/MITSU/S(NF),GO(NF)
  COMMON/FQSPEC/STMA(NF),SUNI(NF),SDIR(NF),SEQU(NF)
  COMMON/DIREC1/S1(NF,ND),D1(ND)

C CALCULATE DIRECTIONAL SPREADING PARAMETER S(NF)
  DO 100 J=1,NF
    IF(FQ(J).LE.FP1)THEN
      S(J)=SMAX*(FQ(J)/FP1)**5
    
```

```

        ELSE
          S(J)=SMAX*(FQ(J)/FP1)**(-2.5)
        ENDIF
100  CONTINUE

C CALCULATE PARAMETER GO(NF) FOR DIRECTIONAL SPREADING FUNCTION
  DO 200 J=1,NF
    X=S(J)+1.
    Y=2*S(J)+1.
    W=2*S(J)-1.
    EXPON=2.*GAMMLN(X)-GAMMLN(Y)
    GO(J)=2.**W*EXP(EXPON)/PI
  200  CONTINUE

C CALCULATE DIRECTIONAL SPECTRUM AT DEPTH 1
  DO 300 J=1,NF
    DO 400 I=1,ND
      S1(J,I)=STMA(J)*GO(J)*COS((THETA(I)-ALPHA1)/2)**(2*S(J))
    400  CONTINUE
  300  CONTINUE

C CALCULATE DIRECTIONAL ENERGY DISTRIBUTION FUNCTION AT DEPTH 1
  DO 500 I=1,ND
    DO 600 J=1,NF
      SINTER(J)=S1(J,I)
    600  CONTINUE
    CALL INTGRL(SINTER,NF,DF,D1(I))
  500  CONTINUE

  RETURN
  END

C INTERNAL FUNCTION SUBROUTINE TO GET NATURAL LOG OF GAMMA FUNCTION
C
C BORROWED FROM NUMERICAL RECIPES (PRESS ET AL. 1986, P.157)
C
C   IN:
C   XX.....ARGUMENT OF FUNCTION
C
C   OUT:
C   GAMMLN.....NATURAL LOG OF GAMMA FUNCTION

FUNCTION GAMMLN(XX)

```



```

C          AT DEPTH 2 (M**2/RAD)                                C
C  FPDIR.....PEAK FREQUENCY OF DIRECTIONAL SPECTRUM          C
C          AT DEPTH 2 (HZ)                                    C
C  TPDIR.....PEAK PERIOD OF DIRECTIONAL SPECTRUM             C
C          AT DEPTH 2 (SEC)                                  C
C  ALPHA2.....PREDOMINANT INCIDENT WAVE DIRECTION AT DEPTH 2 (RAD)C
C                                                                 C
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC

```

SUBROUTINE REFDIR

```

C INITIALIZE & DIMENSION VARIABLES/COMMON STATEMENTS:
  PARAMETER (NF=2001)
  PARAMETER (ND=181)
  DIMENSION S2MAX(NF),SINTER1(ND),SINTER2(NF)
  COMMON/INPUT/H(2),HMO1,TP1,FP1,GAM,SMAX,ALPHA1,SLOPE,IS,IDEEP
  COMMON/DISFRQ/DF,FQ(NF)
  COMMON/DISDIR/DD,THETA(ND)
  COMMON/WNUMBR/WN(2,NF),WN21(NF),CG12(NF)
  COMMON/FQSPEC/STMA(NF),SUNI(NF),SDIR(NF),SEQU(NF)
  COMMON/MITSU/S(NF),GO(NF)
  COMMON/DIREC2/S2(NF,ND),D2(ND)
  COMMON/PEAKS/FPUNI,TPUNI,FPDIR,TPDIR,ALPHA2

  DO 100 J=1,NF
    S2MAX(J)=WN21(J)*SUNI(J)*GO(J)
100  CONTINUE

  DO 200 J=1,NF
    DO 300 I=1,ND
      C=WN21(J)*SIN(THETA(I))
      IF(ABS(C).GT.1.)THEN
        S2(J,I)=0.
      ELSE
        S2(J,I)=S2MAX(J)*COS((ASIN(C)-ALPHA1)/2)**(2.*S(J))
      ENDIF
300  CONTINUE
200  CONTINUE

C CALCULATE FREQUENCY SPECTRUM AND ENERGY DISTRI. FCT AT DEPTH 2
  DO 400 J=1,NF
    DO 500 I=1,ND
      SINTER1(I)=S2(J,I)
500  CONTINUE

```

```

        CALL INTGRL(SINTER1,ND,DD,SDIR(J))
400  CONTINUE
        DO 600 I=1,ND
            DO 700 J=1,NF
                SINTER2(J)=S2(J,I)
700  CONTINUE
            CALL INTGRL(SINTER2,NF,DF,D2(I))
600  CONTINUE

```

C CALCULATE PEAKS

```

        CALL FINDMA(SDIR,NF,SDIRPK,LOC1)
        FPDIR=FQ(LOC1)
        TPDIR=1./FPDIR
        CALL FINDMA(D2,ND,D2PK,LOC2)
        ALPHA2=THETA(LOC2)

```

C CALCULATE EQUIVALENT UNI-DIRECTIONAL FREQUENCY SPECTRUM AT DEPTH 1

```

        DO 800 J=1,NF
            SEQU(J)=SDIR(J)/CG12(J)
800  CONTINUE

```

```

        RETURN
        END

```

```

CCCCCCCCCCCCCCCCCCCCCCCCCCCCCC SUBROUTINE 10 CCCCCCCCCCCCCCCCCCCCCCCCCCC
C                                                                 C
C  FINDMA                                                                 C
C                                                                 C
C  FINDS MAXIMUM VALUE OF GIVEN FUNCTION AND ITS LOCATION          C
C                                                                 C
C      IN:                                                                 C
C      F(NL).....FUNCTION                                           C
C      NL.....NO. OF VALUES                                         C
C                                                                 C
C      OUT:                                                                 C
C      PEAK.....PEAK VALUE                                           C
C      LOC.....LOCATION OF PEAK VALUE                                  C
C                                                                 C
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCC

```

```

SUBROUTINE FINDMA(F,NL,PEAK,LOC)

```

```

REAL F(NL)
PEAK=-.000001

```



```

C   ALPHA1:SPECP(1,11)..PREDOMINANT INCIDENT WAVE DIRECTION      C
C   AT DEPTH 1 (RAD)                                             C
C   TPUNI:SPECP(2,9)...PEAK PERIOD OF NORMALLY-INCIDENT FREQUENCY C
C   SPECTRUM AT DEPTH 2 (S)                                     C
C   FPUNI:SPECP(2,10)...PEAK FREQUENCY OF NORMALLY-INCIDENT FREQUENCYC
C   SPECTRUM AT DEPTH 2 (S)                                     C
C   ALPHA2:SPECP(2,11)..ZERO FOR NORMALLY INCIDENT FREQUENCY SPECTRUMC
C   AT DEPTH 2                                                 C
C   TPDIR:SPECP(3,9)...PEAK PERIOD OF DIRECTIONAL SPECTRUM      C
C   AT DEPTH 2 (S)                                             C
C   FPDIR:SPECP(3,10)...PEAK FREQUENCY OF DIRECTIONAL SPECTRUM C
C   AT DEPTH 2 (HZ)                                           C
C   ALPHA2:SPECP(3,11)..PREDOMINANT INCIDENT WAVE DIRECTION      C
C   AT DEPTH 2 (RAD)                                           C
C   M=1: INCIDENT   M=2: SHOALED UNI-DIR   M=3: REFRACTED DIR    C
C   CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC

```

SUBROUTINE SPCPAR

```

C INITIALIZE & DIMENSION VARIABLES/COMMON STATEMENTS:
PARAMETER (NF=2001)
PARAMETER (ND=181)
DIMENSION SM(5),SINTER1(NF),SINTER2(NF)
COMMON/CONST/PI,G
COMMON/DISFRQ/DF,FQ(NF)
COMMON/FQSPEC/STMA(NF),SUNI(NF),SDIR(NF),SEQU(NF)
COMMON/INPUT/H(2),HMO1,TP1,FP1,GAM,SMAX,ALPHA1,SLOPE,IS,IDEEP
COMMON/PEAKS/FPUNI,TPUNI,FPDIR,TPDIR,ALPHA2
COMMON/SPCTRM/SP(3,NF)
COMMON/SPECP/SPECP(3,12)

DO 100 M=1,3
DO 200 J=1,NF
IF(M.EQ.1)THEN
SP(M,J)=STMA(J)
ELSEIF(M.EQ.2)THEN
SP(M,J)=SUNI(J)
ELSE
SP(M,J)=SDIR(J)
ENDIF
200 CONTINUE
100 CONTINUE

```

C SPECTRAL MOMENTS AND PEAKEDNESS PARAMETER INTEGRATION
 C USING SUBROUTINE 06 INTGRL

```

    SINTER1(1)=0.
    DO 300 M=1,3
      DO 400 K=1,5
        IF(K.NE.4)THEN
          K1=K-1
          DO 500 J=2,NF
            SINTER1(J)=SP(M,J)*FQ(J)**(K1)
500      CONTINUE
          ELSE
            DO 600 J=2,NF
              SINTER1(J)=FQ(J)*SP(M,J)**2
600      CONTINUE
          ENDIF
          CALL INTGRL(SINTER1,NF,DF,SM(K))
400    CONTINUE
  
```

C SPECTRAL STATISTICS

```

    SPECPC(M,1)=SQRT(1-SM(3)**2/(SM(1)*SM(5)))
    SPECPC(M,2)=SQRT((SM(1)*SM(3)/SM(2)**2)-1)
    SPECPC(M,3)=(2./SM(1)**2)*SM(4)
    SPECPC(M,4)=SQRT(SM(1))
    SPECPC(M,5)=SQRT(8.*SM(1))
    SPECPC(M,6)=4.004*SQRT(SM(1))
    SPECPC(M,7)=SM(1)/SM(2)
    SPECPC(M,8)=SQRT(SM(1)/SM(3))
    IF(M.EQ.1)THEN
      SPECPC(M,9)=TP1
      SPECPC(M,10)=FP1
      SPECPC(M,11)=ALPHA1
    ELSEIF(M.EQ.2)THEN
      SPECPC(M,9)=TPUNI
      SPECPC(M,10)=FPUNI
      SPECPC(M,11)=0.0
    ELSE
      SPECPC(M,9)=TPDIR
      SPECPC(M,10)=FPDIR
      SPECPC(M,11)=ALPHA2
    ENDIF
  
```

C CORRELATED PARAMETER INTEGRATION AND CALCULATION

```

    SINTER1(1)=0.
  
```



```

REAL PHI(NF)
COMPLEX CN(N), COEF(NDS,1), AFFT(NDS,1)
COMMON/CONST/PI,G
COMMON/INPUT/H(2),HMO1,TP1,FP1,GAM,SMAX,ALPHA1,SLOPE,IS,IDEEP
COMMON/DISFRQ/DF,FQ(NF)
COMMON/DISTIM/NP,DT,TIME(N)
COMMON/SPCTRM/SP(3,NF)
COMMON/SERIES/TS(3,N)

TWOPI=2.*PI

C GENERATE RANDOM NUMBERS FROM 0 TO 1
  CALL RNSET(IS)
  CALL RNUN(NF-1,PHI)

C FILL UP COMPLEX COEFFICIENTS
C                                     AVERAGE VALUE
  DO 200 M=1,3
    CN(1)=CMPLX(0.0,0.0)
C                                     FIRST HALF OF ARRAY
  DO 300 K=2,NF-1
    PHX=TWOPI*PHI(K-1)
    CX=SQRT(2.*SP(M,K)*DF)
    CN(K)=.5*CX*CMPLX(COS(PHX),SIN(PHX))
300  CONTINUE
C                                     AT NYQUIST FREQUENCY
  PHX=TWOPI*PHI(NF-1)
  CX=SQRT(2.*SP(M,NF)*DF)
  CN(NF)=CX*CMPLX(COS(PHX),0.0)
C                                     SECOND HALF OF ARRAY
  DO 400 K=NF+1,NP
    NN=NP-K+2
    PHX=TWOPI*PHI(NN-1)
    CX=SQRT(2.*SP(M,NN)*DF)
    CN(K)=.5*CX*CMPLX(COS(PHX),-SIN(PHX))
400  CONTINUE
C                                     INVERSE FOURIER TRANSFORM
  DO 500 K=1,NP
    COEF(K,1)=CN(K)
500  CONTINUE
  NRcoef=NP
  NCCOEF=1
  LDCOEF=NDS
  LDA=NDS

```


SUBROUTINE TIMPAR

```

C INITIALIZE & DIMENSION VARIABLES/COMMON STATEMENTS:
  PARAMETER (NDS=8000)
  PARAMETER (NDZ=500)
  PARAMETER (N=4000)
  REAL ATS(NDS),HGT(NDZ)
  REAL TMZERO(NDZ),T(NDZ),TSMAX(NDZ),TSMIN(NDZ)
  INTEGER IZERO(NDZ),JMAX(NDZ),JMIN(NDZ),IRK(NDZ)
  LOGICAL SORTED
  COMMON/DISTIM/NP,DT,TIME(N)
  COMMON/SERIES/TS(3,N)
  COMMON/UPCROS/NZ(3),HRK(3,NDZ),TRK(3,NDZ),NK(3),LRN(3,NDZ)
  COMMON/TIMEPR/TIMEP(3,12)

  TM=NP*DT
C ADJUST TIME SERIES TO MAKE PERIODIC OVER TIME FOR M=1,2 AND 3
  DO 50 M=1,3
    DO 100 I=1,NP
      ATS(I)=TS(M,I)
100  CONTINUE
      ATS(NP+1)=TS(M,1)
C CORRECT FOR MEAN WATER LEVEL
      SUM=0.0
      DO 150 I=1,NP
        SUM=SUM+ATS(I)
150  CONTINUE
      SD=SUM/FLOAT(NP)
      DO 200 I=1,NP+1
        ATS(I)=ATS(I)-SD
200  CONTINUE
      TIMEP(M,1)=SD
C COMPUTE STANDARD DEVIATION OF ETA(T)
      SUM=0.0
      DO 250 I=1,NP
        SUM=SUM+(ATS(I)*ATS(I))
250  CONTINUE
      ER=SQRT(SUM/FLOAT(NP))
      TIMEP(M,2)=ER
C ZERO-UPCROSSING POINTS
      NZ(M)=0
      DO 300 J=1,NP
        IF(ATS(J).EQ.0.0)THEN
          NZ(M)=NZ(M)+1

```

```

        IZERO(NZ(M))=J+1
        TMZERO(NZ(M))=(J-1)*DT
    ELSEIF(ATS(J).LT.0.0.AND.ATS(J+1).GT.0.0)THEN
        NZ(M)=NZ(M)+1
        IZERO(NZ(M))=J+1
        TMZERO(NZ(M))=(J-1)*DT+(-ATS(J)/(ATS(J+1)-ATS(J)))*DT
    ENDIF
300    CONTINUE
        TIMEP(M,3)=FLOAT(NZ(M))
C CALCULATE WAVE PERIOD, T, OF EACH WAVE
    DO 350 I=1,NZ(M)-1
        T(I)=TMZERO(I+1)-TMZERO(I)
350    CONTINUE
        T(NZ(M))=(TM-TMZERO(NZ(M)))+TMZERO(1)
C NEED TO FIND TSMAX, TSMIN
    DO 400 I=1,NZ(M)
        TSMAX(I)=0.0
        TSMIN(I)=0.0
        J1=IZERO(I)
        IF(I.EQ.NZ(M))THEN
            J2=NP+IZERO(1)-1
        ELSE
            J2=IZERO(I+1)-1
        ENDIF
        DO 450 J=J1,J2
            IF(J.GT.NP)THEN
                JT=J-NP
            ELSE
                JT=J
            ENDIF
            IF(ATS(JT).GT.TSMAX(I))THEN
                TSMAX(I)=ATS(JT)
                JMAX(I)=JT
            ENDIF
            IF(ATS(JT).LT.TSMIN(I))THEN
                TSMIN(I)=ATS(JT)
                JMIN(I)=JT
            ENDIF
450    CONTINUE
400    CONTINUE
C IMPROVE ESTIMATES W/ PARABOLIC CURVE
    DO 500 I=1,NZ(M)
        J=JMAX(I)
        J1=J-1

```

```

      IF(J1.LT.1)THEN
        J1=NP
      ENDIF
      TS1=ATS(J1)
      TS2=ATS(J)
      TS3=ATS(J+1)
      TSMAX(I)=TS2-(TS3-TS1)**2/(8.*(TS1-2*TS2+TS3))
      J=JMIN(I)
      J1=J-1
      IF(J1.LT.1)THEN
        J1=NP
      ENDIF
      TS1=ATS(J1)
      TS2=ATS(J)
      TS3=ATS(J+1)
      TSMIN(I)=TS2-(TS3-TS1)**2/(8.*(TS1-2*TS2+TS3))
C WAVE HEIGHT, HGT, OF EACH WAVE
      HGT(I)=TSMAX(I)-TSMIN(I)
500  CONTINUE
C STATISTICS OF INDIVIDUAL WAVE HEIGHTS
      SUM=0.0
      SUMHB=0.0
      SUMHV=0.0
      DO 550 I=1,NZ(M)
        SUM=SUM+T(I)
        SUMHB=SUMHB+HGT(I)
        SUMHV=SUMHV+HGT(I)*HGT(I)
550  CONTINUE
      TB=SUM/FLOAT(NZ(M))
      HB=SUMHB/FLOAT(NZ(M))
      HV=SQRT(SUMHV/FLOAT(NZ(M)))
      TIMEP(M,5)=TB
      TIMEP(M,4)=HB
      TIMEP(M,6)=HV
C SORTING ROUTINE FOR WAVE HEIGHT RANKING
C                               SET UP HRANK, TRANK, IRANK ARRAYS
      DO 600 I=1,NZ(M)
        IRK(I)=I
        HRK(M,I)=HGT(I)
        TRK(M,I)=T(I)
600  CONTINUE
      SORTED=.FALSE.
      IPASS=0
650  IF(.NOT.SORTED)THEN

```

```

IPASS=IPASS+1
SORTED=.TRUE.
DO 700 I=1,NZ(M)-IPASS
  IF(HGT(IRK(I)).LT.HGT(IRK(I+1)))THEN
    ITEMP=IRK(I)
    IRK(I)=IRK(I+1)
    IRK(I+1)=ITEMP
    HTEMP=HRK(M,I)
    HRK(M,I)=HRK(M,I+1)
    HRK(M,I+1)=HTEMP
    TTEMP=TRK(M,I)
    TRK(M,I)=TRK(M,I+1)
    TRK(M,I+1)=TTEMP
    SORTED=.FALSE.
  ENDIF
700  CONTINUE
    GOTO 650
  ENDIF
C REPRESENTATIVE WAVE HEIGHT AND PERIOD
  ITHIRD=NZ(M)/3
  ITENTH=NZ(M)/10
  HS=0.0
  T3=0.0
  DO 750 I=1,ITHIRD
    HS=HS+HRK(M,I)
    T3=T3+TRK(M,I)
750  CONTINUE
  HS=HS/FLOAT(ITHIRD)
  T3=T3/FLOAT(ITHIRD)
  TIMEP(M,7)=HS
  TIMEP(M,8)=T3
  HT=0.0
  TT=0.0
  DO 800 I=1,ITENTH
    HT=HT+HRK(M,I)
    TT=TT+TRK(M,I)
800  CONTINUE
  HT=HT/FLOAT(ITENTH)
  TT=TT/FLOAT(ITENTH)
  TIMEP(M,9)=HT
  TIMEP(M,10)=TT
C RUN LENGTH OF WAVE HEIGHTS EXCEEDING HS
  NK(M)=0
  NCOUNT=0

```

```

      I=1
850   IF(I.LE.NZ(M))THEN
      IF(HGT(I).GT.HS)THEN
      NK(M)=NK(M)+1
      NCOUNT=NCOUNT+1
900   IF(HGT(I+NCOUNT).GT.HS)THEN
      NCOUNT=NCOUNT+1
      GO TO 900
      ENDIF
      LRN(M,NK(M))=NCOUNT
      I=I+NCOUNT
      NCOUNT=0
      ENDIF
      I=I+1
      GOTO 850
      ENDIF
      TIMEP(M,11)=FLOAT(NK(M))
C CALCULATE MEAN RUN LENGTH
      SUMLRN=0.0
      DO 950 J=1,NK(M)
      SUMLRN=SUMLRN+LRN(M,J)
950   CONTINUE
      TIMEP(M,12)=SUMLRN/FLOAT(NK(M))

50   CONTINUE

      RETURN
      END

CCCCCCCCCCCCCCCCCCCCCCCCCCCCCC SUBROUTINE 14 CCCCCCCCCCCCCCCCCCCCCCCCCC
C                                                                 C
C  WBREAK                                                                 C
C                                                                 C
C  COMPUTES BREAKING OF INDIVIDUAL WAVES AT SHALLOWER DEPTH 2      C
C                                                                 C
C      IN:                                                                 C
C      H(2).....SHALLOWER WATER DEPTH 2 (M)                        C
C      SLOPE.....BOTTOM SLOPE AT DEPTH 2                            C
C      NZ:TIMEP(M,3)...NUMBER OF ZERO-UPCROSSING WAVES              C
C      HRK(M,NZ).....RANKED WAVE HEIGHTS WITH HRK(1) THE HIGHEST (M) C
C      TRK(M,NZ).....WAVE PERIODS FOR RANKED WAVE HEIGHTS (S)       C
C                                                                 C
C      OUT:                                                                 C
C      HBREAK(M,NZ)...BREAKER HEIGHT (M)                            C

```



```

C   TP1.....PEAK PERIOD AT DEPTH 1 (S)                                C
C   GAM.....PEAK ENHANCEMENT FACTOR FOR JONSWAP SPECTRUM           C
C   IDEEP.....WATER DEPTH IDENTIFIER: SET IDEEP=1 FOR DEEP WATER   C
C   SPECTRUM                                                                    C
C   SMAX.....MAX. VALUE OF DIRECTIONAL SPREADING PARAMETER, S,     C
C   AT DEPTH 1                                                                    C
C   ALPHA1.....PREDOMINANT INCIDENT WAVE DIRECTION AT DEPTH 1 (RAD)C
C   SLOPE.....BOTTOM SLOPE AT DEPTH 2                                     C
C   IS.....SEED VALUE FOR RANDOM NO. GENERATOR                       C
C   NF.....NO. OF DISCRETE FREQUENCIES                                 C
C   DF.....FREQUENCY BANDWIDTH (DELTA F) (HZ)                        C
C   NP.....EVEN NO. OF DATA POINTS IN TIME SERIES                  C
C   DT.....TIME STEP (DELTA T)                                         C
C   ND.....NO. OF DISCRETE DIRECTIONS                                 C
C   DD.....DIRECTIONAL BANDWIDTH (RADS)                               C
C
C   OUT:                                                                    C
C   INPUT OUT....OUTPUT (DATA) FILE NAME FOR INPUT AND              C
C   DISCRETIZATION PARAMETERS (UNIT=11)                                C
C   FQ DATA.....OUTPUT (PLOT) FILE NAME FOR FREQUENCY DOMAIN       C
C   (UNIT=12)                                                            C
C   ANG DATA....OUTPUT (PLOT) FILE NAME FOR DIRECTIONAL DOMAIN     C
C   (UNIT=13)                                                            C
C   TIME DATA....OUTPUT (PLOT) FILE NAME FOR TIME DOMAIN (UNIT=14) C
C
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC

```

SUBROUTINE TABINP

```

C INITIALIZE & DIMENSION VARIABLES/COMMON STATEMENTS
  PARAMETER (NF=2001)
  PARAMETER (ND=181)
  PARAMETER (N=4000)
  CHARACTER*30 COMMEN1,COMMEN2,COMMEN3,COMMEN4,COMMEN5
  COMMON/CONST/PI,G
  COMMON/INPUT/H(2),HMO1,TP1,FP1,GAM,SMAX,ALPHA1,SLOPE,IS,IDEEP
  COMMON/OUTPUT/COMMEN1,COMMEN2,COMMEN3,COMMEN4,COMMEN5
  COMMON/DISFRQ/DF,FQ(NF)
  COMMON/DISTIM/NP,DT,TIME(N)
  COMMON/DISDIR/DD,THETA(ND)
  COMMON/MINMAX/FMIN,FMAX,TMIN,TMAX

C OPEN (DATA) FILE INPUT OUT FOR PARAMETERS (UNIT=11)
  WRITE(11,*) COMMEN1

```

```

WRITE(11,*) COMMEN2
WRITE(11,*) COMMEN3
WRITE(11,*) COMMEN4
WRITE(11,*) COMMEN5
WRITE(11,*) ' '
WRITE(11,*) 'INPUT PARAMETERS'
WRITE(11,*) ' '
WRITE(11,10) H(1)
WRITE(11,11) H(2)
WRITE(11,12) HMO1,TP1
WRITE(11,13) GAM
WRITE(11,14) IDEEP
WRITE(11,15) SMAX
WRITE(11,16) ALPHA1*180./PI
WRITE(11,17) SLOPE
WRITE(11,18) IS
WRITE(11,19) NF
WRITE(11,20) ND
WRITE(11,21) FMIN,FMAX
WRITE(11,22) TMIN*180./PI,TMAX*180./PI
WRITE(11,*) ' '
WRITE(11,*) 'FILE NAME          OUTPUT'
WRITE(11,*) '-----          -----'
WRITE(11,*) 'FQ DATA          FRQ. DOMAIN'
WRITE(11,*) 'ANG DATA          DIR. DOMAIN'
WRITE(11,*) 'TIME DATA          TIME DOMAIN'
10  FORMAT(F12.8,22X,'--> H1 (M)')
11  FORMAT(F12.8,22X,'--> H2 (M)')
12  FORMAT(F12.8,5X,F12.8,5X,'--> HMO1 (M), TP1 (S)')
13  FORMAT(F12.8,22X,'--> GAMMA')
14  FORMAT(I5,29X,'--> IDEEP')
15  FORMAT(F12.8,22X,'--> SMAX')
16  FORMAT(F12.8,22X,'--> ALPHA1 (DEG)')
17  FORMAT(F12.8,22X,'--> SLOPE')
18  FORMAT(I5,29X,'--> IS')
19  FORMAT(I5,29X,'--> NO. OF FRQ.')
20  FORMAT(I5,29X,'--> NO. OF DIR.')
21  FORMAT(F12.8,5X,F12.8,5X,'--> FMIN (HZ), FMAX (HZ)')
22  FORMAT(F12.8,5X,F12.8,5X,'--> THETAMIN (DEG), THETAMAX (DEG)')

```

```

C OPEN (PLOT) FILE FQ DATA, ANG DATA AND TIME DATA FOR DOMAINS
C (UNITS 12-14)

```

```

WRITE(12,23) (FQ(J),J=1,NF)
WRITE(13,23) (THETA(I)*180./PI,I=1,ND)

```



```

C      M=1: INCIDENT      M=2: SHOALED UNI-DIR      M=3: REFRACTED DIR      C
C
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SUBROUTINE TABSPC

```

```

C INITIALIZE & DIMENSION VARIABLES/COMMON STATEMENTS

```

```

CHARACTER*30 COMMEN1,COMMEN2,COMMEN3,COMMEN4,COMMEN5
COMMON/INPUT/H(2),HMO1,TP1,FP1,GAM,SMAX,ALPHA1,SLOPE,IS,IDEEP
COMMON/OUTPUT/COMMEN1,COMMEN2,COMMEN3,COMMEN4,COMMEN5
COMMON/SPECP/SPECP(3,12)

```

```

C WRITE SPECTRAL PARAMETERS TO (DATA) FILE SPECP OUT (UNIT=15)

```

```

WRITE(15,*) COMMEN1
WRITE(15,*) COMMEN2
WRITE(15,*) COMMEN3
WRITE(15,*) COMMEN4
WRITE(15,*) COMMEN5
WRITE(15,*) ' '
WRITE(15,*) 'SPECTRAL PARAMETERS'
WRITE(15,*) ' '
WRITE(15,*) ' SPECTRAL      INCIDENT      SHOALED      REFRACTED'
WRITE(15,*) 'PARAMETERS    SPECTRUM      SPECTRUM      SPECTRUM'
WRITE(15,*) '-----'
WRITE(15,10) H(1),H(2),H(2)
WRITE(15,*) '-----'
WRITE(15,11) SPECP(1,1),SPECP(2,1),SPECP(3,1)
WRITE(15,12) SPECP(1,2),SPECP(2,2),SPECP(3,2)
WRITE(15,13) SPECP(1,3),SPECP(2,3),SPECP(3,3)
WRITE(15,14) SPECP(1,4),SPECP(2,4),SPECP(3,4)
WRITE(15,15) SPECP(1,5),SPECP(2,5),SPECP(3,5)
WRITE(15,16) SPECP(1,6),SPECP(2,6),SPECP(3,6)
WRITE(15,17) SPECP(1,7),SPECP(2,7),SPECP(3,7)
WRITE(15,18) SPECP(1,8),SPECP(2,8),SPECP(3,8)
WRITE(15,19) SPECP(1,9),SPECP(2,9),SPECP(3,9)
WRITE(15,20) SPECP(1,10),SPECP(2,10),SPECP(3,10)
WRITE(15,21) SPECP(1,11),SPECP(2,11),SPECP(3,11)
WRITE(15,22) SPECP(1,12),SPECP(2,12),SPECP(3,12)
10  FORMAT(' DEPTH (M)      ',F8.5,3X,F8.5,3X,F8.5)
11  FORMAT('      EP',7X,F8.5,3X,F8.5,3X,F8.5)
12  FORMAT('      VU',7X,F8.5,3X,F8.5,3X,F8.5)
13  FORMAT('      Qp',7X,F8.5,3X,F8.5,3X,F8.5)
14  FORMAT('      ER',7X,F8.5,3X,F8.5,3X,F8.5)
15  FORMAT('      HR',7X,F8.5,3X,F8.5,3X,F8.5)

```

```

16  FORMAT('      HMO',6X,F8.5,3X,F8.5,3X,F8.5)
17  FORMAT('      T1',7X,F8.5,3X,F8.5,3X,F8.5)
18  FORMAT('      T2',7X,F8.5,3X,F8.5,3X,F8.5)
19  FORMAT('      TP',7X,F8.5,3X,F8.5,3X,F8.5)
20  FORMAT('      FP',7X,F8.5,3X,F8.5,3X,F8.5)
21  FORMAT('      ALPHA',4X,F8.5,3X,F8.5,3X,F8.5)
22  FORMAT('      KAPPA',4X,F8.5,3X,F8.5,3X,F8.5)
      RETURN
      END

CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC SUBROUTINE 18 CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
C                                                                 C
C  TABTIM                                                                 C
C                                                                 C
C  OUPUTS TIME SERIES PARAMETERS                                                                 C
C                                                                 C
C      IN/OUT:                                                                 C
C  H(M).....WATER DEPTHS 1 & 2 (M=1,2) (M)                                                                 C
C  SD:TIMEP(M,1)...AVERAGE OF TS (SETUP OR SETDOWN) (M)                                                                 C
C  ER:TIMEP(M,2)...STANDARD DEVIATION OF TIME SERIES (M)                                                                 C
C  NZ:TIMEP(M,3)...NUMBER OF ZERO-UPCROSSING WAVES                                                                 C
C  HB:TIMEP(M,4)...MEAN WAVE HEIGHT (M)                                                                 C
C  TB:TIMEP(M,5)...MEAN WAVE PERIOD (S)                                                                 C
C  HV:TIMEP(M,6)...ROOT-MEAN-SQUARE WAVE HEIGHT (M)                                                                 C
C  HS:TIMEP(M,7)...SIGNIFICANT WAVE HEIGHT OF 1/3 HIGHEST WAVES (M) C
C  T3:TIMEP(M,8)...SIGNIFICANT WAVE PERIOD OF 1/3 HIGHEST WAVES (S) C
C  HT:TIMEP(M,9)...MEAN HEIGHT OF ONE-TENTH HIGHEST WAVES (M)                                                                 C
C  TT:TIMEP(M,10)...MEAN PERIOD OF ONE-TENTH HIGHEST WAVES (S)                                                                 C
C  NK:TIMEP(M,11)...NUMBER OF RUNS EXCEEDING HS                                                                 C
C  TIMEP(M,12)....MEAN RUN LENGTH                                                                 C
C                                                                 C
C  M=1: INCIDENT      M=2: SHOALED UNI-DIR      M=3: REFRACTED DIR                                                                 C
C                                                                 C
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC

```

SUBROUTINE TABTIM

```

C  INITIALIZE & DIMENSION VARIABLES/COMMON STATEMENTS
      CHARACTER*30  COMMEN1,COMMEN2,COMMEN3,COMMEN4,COMMEN5
      COMMON/INPUT/H(2),HMO1,TP1,FP1,GAM,SMAX,ALPHA1,SLOPE,IS,IDEEP
      COMMON/OUTPUT/COMMEN1,COMMEN2,COMMEN3,COMMEN4,COMMEN5
      COMMON/TIMEPR/TIMEP(3,12)

C  WRITE TIME PARAMETERS TO (DATA) FILE TIMEP OUT (UNIT=16)

```



```

C  TABIWS
C
C  OUPUTS INDIVIDUAL WAVE STATISTICS
C
C      IN/OUT:
C  H(M).....WATER DEPTHS 1 & 2 (M=1,2) (M)
C  NZ:TIMEP(M,3)...NUMBER OF ZERO-UPCROSSING WAVES
C  HRK(M,NZ).....RANKED WAVE HEIGHTS WITH HRK(1) THE HIGHEST (M)
C  TRK(M,NZ).....WAVE PERIODS FOR RANKED WAVE HEIGHTS (S)
C  HBREAK(M,NZ)...BREAKER HEIGHT (M)
C  IBREAK(M,NZ)...BREAKER INDICATOR: 1-BREAKING 0-NOT BREAKING
C
C  M=1: INCIDENT   M=2: SHOALED UNI-DIR   M=3: REFRACTED DIR
C
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC

```

SUBROUTINE TABIWS

```

C  INITIALIZE & DIMENSION VARIABLES/COMMON STATEMENTS
    PARAMETER (NDZ=500)
    CHARACTER*30 COMMEN1,COMMEN2,COMMEN3,COMMEN4,COMMEN5
    COMMON/INPUT/H(2),HMO1,TP1,FP1,GAM,SMAX,ALPHA1,SLOPE,IS,IDEEP
    COMMON/OUTPUT/COMMEN1,COMMEN2,COMMEN3,COMMEN4,COMMEN5
    COMMON/UPCROS/NZ(3),HRK(3,NDZ),TRK(3,NDZ),NK(3),LRN(3,NDZ)
    COMMON/WAVEBK/HBREAK(3,NDZ),IBREAK(3,NDZ)

C  WRITE WAVE STATISTICS FOR SHOALED UNI-DIR SPECTRUM TO (DATA) FILE
C  UNIBRK OUT (UNIT=17)
    WRITE(17,*) COMMEN1
    WRITE(17,*) COMMEN2
    WRITE(17,*) COMMEN3
    WRITE(17,*) COMMEN4
    WRITE(17,*) COMMEN5
    WRITE(17,*) ' '
    WRITE(17,*) 'WAVE STATISTICS FOR SHOALED SPECTRUM'
    WRITE(17,*) ' '
    WRITE(17,*) '          INC SPECTRUM          SHOALED SPECTRUM'
    WRITE(17,*) '-----'
    WRITE(17,10) H(1),H(2)
    WRITE(17,*) '-----'
    WRITE(17,*) '  RANK   Tr      Hr      Tr      Hr      Hb   Ib'
    WRITE(17,*) '-----'
    IF(NZ(2).GE.NZ(1))THEN
      N=NZ(2)

```



```

C
C      IN/OUT:
C      H(M).....WATER DEPTHS 1 & 2 (M=1,2) (M)
C      NK:TIMEP(M,11)..NUMBER OF RUNS
C      LRN(M,NK).....RUN LENGTH OF WAVE HEIGHTS EXCEEDING HS
C      TIMEP(M,12).....MEAN RUN LENGTH
C
C      M=1: INCIDENT   M=2: SHOALED UNI-DIR   M=3: REFRACTED DIR
C
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC

```

SUBROUTINE TABRUN

```

C INITIALIZE & DIMENSION VARIABLES/COMMON STATEMENTS
  PARAMETER (NDZ=500)
  CHARACTER*30 COMMEN1,COMMEN2,COMMEN3,COMMEN4,COMMEN5
  COMMON/INPUT/H(2),HMO1,TP1,FP1,GAM,SMAX,ALPHA1,SLOPE,IS,IDEEP
  COMMON/OUTPUT/COMMEN1,COMMEN2,COMMEN3,COMMEN4,COMMEN5
  COMMON/UPCROS/NZ(3),HRK(3,NDZ),TRK(3,NDZ),NK(3),LRN(3,NDZ)
  COMMON/TIMEPR/TIMEP(3,12)

C WRITE RUN LENGTH PARAMETERS TO (DATA) FILE RUNLTH OUT (UNIT=19)
  WRITE(19,*) COMMEN1
  WRITE(19,*) COMMEN2
  WRITE(19,*) COMMEN3
  WRITE(19,*) COMMEN4
  WRITE(19,*) COMMEN5
  WRITE(19,*) ' '
  WRITE(19,*) 'RUN LENGTH PARAMETERS'
  WRITE(19,*) ' '
  WRITE(19,*) '          INCIDENT   SHOALED   REFRACTED'
  WRITE(19,*) '  EVENT      WAVES     WAVES     WAVES '
  WRITE(19,*) '-----'
  WRITE(19,10) H(1),H(2),H(2)
  WRITE(19,*) '-----'
  NA=NK(1)
  IF(NK(2).GT.NA)THEN
    NA=NK(2)
  ENDIF
  IF(NK(3).GT.NA)THEN
    NA=NK(3)
  ENDIF
  DO 200 I=1,NA
    WRITE(19,11) I,LRN(1,I),LRN(2,I),LRN(3,I)

```



```
COMMON/DISDIR/DD,THETA(ND)
COMMON/FQSPEC/STMA(NF),SUNI(NF),SDIR(NF),SEQU(NF)
COMMON/DIREC1/S1(NF,ND),D1(ND)
COMMON/DIREC2/S2(NF,ND),D2(ND)
COMMON/SERIES/TS(3,N)
```

```
C WRITE TO (PLOT) FILES (UNITS 20-25)
```

```
WRITE(20,10) (STMA(J),J=1,NF)
WRITE(21,10) (SUNI(J),J=1,NF)
WRITE(22,10) (SDIR(J),J=1,NF)
WRITE(23,10) (SEQU(J),J=1,NF)
WRITE(24,10) (D1(I),I=1,ND)
WRITE(25,10) (D2(I),I=1,ND)
```

```
C WRITE DIRECTIONAL SPECTRA TO (PLOT) FILES FOR 3D PLOTTING
```

```
DO 100 I=1,ND
  DO 200 J=1,NF
    WRITE(26,10) S1(J,I)
    WRITE(27,10) S2(J,I)
```

```
200 CONTINUE
```

```
100 CONTINUE
```

```
C WRITE TO (PLOT) FILES (UNITS 28-30)
```

```
WRITE(28,10) (TS(1,K),K=1,NP)
WRITE(29,10) (TS(2,K),K=1,NP)
WRITE(30,10) (TS(3,K),K=1,NP)
```

```
10 FORMAT(E17.9)
```

```
RETURN
```

```
END
```

Appendix B

ANALYZED RANDOM WAVE DATA: FIELD DATA EXAMPLE

This appendix contains the random wave data for two field data cases corresponding to Run 1 in Kobayashi and Wurjanto (1992) with the predominant incident wave direction $\alpha_p = 0^\circ$ and 45° in (2.20). The following tables are included for each case:

1. Input Parameters.
2. Spectral Parameters.
3. Time Series Parameters.
4. Run Length Statistics.
5. Ranked Wave Heights and Breaker Heights for Incident Versus Shoaled Uni-Directional Frequency Spectra.
6. Ranked Wave Heights and Breaker Heights for Incident Versus Refracted Directional Frequency Spectra.

Also, the following figures are included for each case:

1. Refracted Frequency Spectrum Versus Shoaled Uni-Directional Frequency Spectrum at Depth 2.
2. Refracted Frequency Spectrum at Depth 2 Versus Incident Frequency Spectrum at Depth 1.

2. Refracted Frequency Spectrum at Depth 2 Versus Incident Frequency Spectrum at Depth 1.
3. Equivalent Uni-Directional Frequency Spectrum Versus Incident Frequency Spectrum at Depth 1.
4. Energy Distribution Function at Depth 2 Versus Energy Distribution Function at Depth 1.
5. Time Series Generated From Incident Frequency Spectrum at Depth 1.
6. Time Series Generated From Shoaled Uni-Directional Frequency Spectrum at Depth 2.
7. Time Series Generated From Refracted Frequency Spectrum at Depth 2.
8. Directional Spectrum at Depth 2 as a Function of Frequency and Direction.
9. Directional Spectrum at Depth 1 as a Function of Frequency and Direction.

Also included is the following comparison between the two cases:

10. Refracted Frequency Spectrum, $\alpha_p = 45^\circ$, Versus Refracted Frequency Spectrum, $\alpha_p = 0^\circ$.

Table B.1: INPUT PARAMETERS: $\alpha_p = 0^\circ$

20.00000000		--> H1 (M)
4.14999962		--> H2 (M)
2.15999985	7.00000000	--> HMO1 (M), TP1 (S)
1.00000000		--> GAMMA
1		--> IDEEP
10.00000000		--> SMAX
0.00000000		--> ALPHA1 (DEG)
0.03000000		--> SLOPE
13579		--> IS
2001		--> NO. OF FRQ.
181		--> NO. OF DIR.
0.00000000	1.42857075	--> FMIN (HZ), FMAX (HZ)
-89.99995420	89.99995420	--> THETAMIN (DEG), THETAMAX (DEG)

Table B.2: SPECTRAL PARAMETERS: $\alpha_p = 0^\circ$

SPECTRAL PARAMETERS	INCIDENT SPECTRUM	SHOALED SPECTRUM	REFRACTED SPECTRUM
DEPTH (M)	20.00000	4.15000	4.15000
EP	0.79736	0.81352	0.78299
VU	0.41065	0.42180	0.38918
Qp	2.00051	2.09054	2.21653
ER	0.53947	0.55447	0.51610
HR	1.52586	1.56828	1.45976
HMO	2.16005	2.22010	2.06647
T1	5.40948	5.66035	5.74665
T2	5.00399	5.21538	5.35537
TP	7.00000	7.32985	7.17949
FP	0.14286	0.13643	0.13929
ALPHA	0.00000	0.00000	0.00000
KAPPA	0.42358	0.45513	0.46764

Table B.3: TIME SERIES PARAMETERS: $\alpha_p = 0^\circ$

TIME SERIES PARAMETERS	INCIDENT SPECTRUM	SHOALED SPECTRUM	REFRACTED SPECTRUM
DEPTH (M)	20.00000	4.15000	4.15000
SD	0.00000	0.00000	0.00000
ER	0.53939	0.55439	0.51602
NZ	275.000	267.000	261.000
HB	1.32407	1.34429	1.25851
TB	5.09091	5.24345	5.36399
HV	1.47857	1.50866	1.40865
HS	2.07343	2.12555	1.97799
T3	6.24178	6.49121	6.48353
HT	2.55849	2.63555	2.43927
TT	6.26641	6.43732	6.42614
NK	26.000	24.000	25.000
M.R.L.	1.34615	1.29167	1.32000

Table B.4: RUN LENGTH STATISTICS: $\alpha_p = 0^\circ$

EVENT	INCIDENT WAVES	SHOALED WAVES	REFRACTED WAVES
DEPTH (M)	20.00000	4.15000	4.15000
1	1	1	1
2	1	1	1
3	1	1	1
4	1	2	1
5	2	1	2
6	1	1	1
7	1	1	2
8	1	2	1
9	2	1	2
10	1	2	1
11	1	1	2
12	3	1	1
13	1	1	1
14	1	1	1
15	1	2	1
16	1	2	2
17	2	2	2
18	2	1	2
19	2	2	1
20	1	1	2
21	2	1	1
22	1	1	1
23	1	1	1
24	2	1	1
25	1	0	1
26	1	0	0
MEAN RUN LTH	1.34615	1.29167	1.32000

Table B.5: WAVE STATISTICS: INCIDENT VS. SHOALED: $\alpha_p = 0^\circ$

		INC SPECTRUM		SHOALED SPECTRUM			
DEPTH(M)		20.00000		4.15000			
RANK	Tr	Hr	Tr	Hr	Hb	Ib	
1	5.744	3.516	5.803	3.516	3.089	1	
2	6.138	3.176	7.236	3.407	3.317	1	
3	7.108	3.135	6.211	3.284	3.167	1	
4	6.775	2.951	7.229	3.117	3.316	0	
5	7.187	2.886	6.800	2.888	3.260	0	
6	6.307	2.760	6.435	2.851	3.205	0	
7	5.403	2.684	6.632	2.755	3.236	0	
8	6.029	2.606	6.428	2.690	3.204	0	
9	7.910	2.602	6.322	2.657	3.187	0	
10	6.496	2.577	6.252	2.642	3.174	0	
11	5.102	2.534	6.149	2.616	3.156	0	
12	5.985	2.529	7.797	2.604	3.377	0	
13	5.046	2.526	7.879	2.602	3.385	0	
14	6.776	2.489	6.938	2.596	3.279	0	
15	7.789	2.460	7.113	2.585	3.302	0	
16	5.959	2.457	5.227	2.506	2.951	0	
17	7.040	2.417	5.093	2.418	2.914	0	
18	4.628	2.400	7.014	2.385	3.289	0	
19	5.503	2.366	7.018	2.373	3.290	0	
20	6.940	2.326	7.756	2.342	3.373	0	
21	4.977	2.276	4.862	2.341	2.845	0	
22	5.857	2.274	5.564	2.305	3.036	0	
23	5.477	2.258	5.178	2.280	2.938	0	
24	6.337	2.233	6.086	2.260	3.145	0	
25	5.973	2.225	6.016	2.256	3.131	0	

Table B.6: WAVE STATISTICS: INCIDENT VS. REFRACTED: $\alpha_p = 0^\circ$

INC SPECTRUM		REFRACTED SPECTRUM					
DEPTH(M)	20.00000		4.15000				
RANK	Tr	Hr	Tr	Hr	Hb	Ib	
1	5.744	3.516	5.833	3.330	3.095	1	
2	6.138	3.176	7.183	3.104	3.310	0	
3	7.108	3.135	6.223	3.085	3.169	0	
4	6.775	2.951	7.197	2.906	3.312	0	
5	7.187	2.886	6.752	2.666	3.254	0	
6	6.307	2.760	6.427	2.659	3.204	0	
7	5.403	2.684	6.629	2.539	3.235	0	
8	6.029	2.606	6.222	2.462	3.169	0	
9	7.910	2.602	6.386	2.431	3.197	0	
10	6.496	2.577	6.911	2.430	3.276	0	
11	5.102	2.534	6.215	2.411	3.168	0	
12	5.985	2.529	7.072	2.407	3.297	0	
13	5.046	2.526	7.787	2.404	3.376	0	
14	6.776	2.489	7.832	2.399	3.381	0	
15	7.789	2.460	6.156	2.343	3.157	0	
16	5.959	2.457	5.262	2.312	2.961	0	
17	7.040	2.417	5.182	2.277	2.939	0	
18	4.628	2.400	6.967	2.223	3.283	0	
19	5.503	2.366	6.987	2.197	3.286	0	
20	6.940	2.326	5.618	2.181	3.048	0	
21	4.977	2.276	4.964	2.162	2.876	0	
22	5.857	2.274	7.748	2.153	3.373	0	
23	5.477	2.258	6.017	2.108	3.132	0	
24	6.337	2.233	6.335	2.094	3.189	0	
25	5.973	2.225	5.205	2.083	2.945	0	

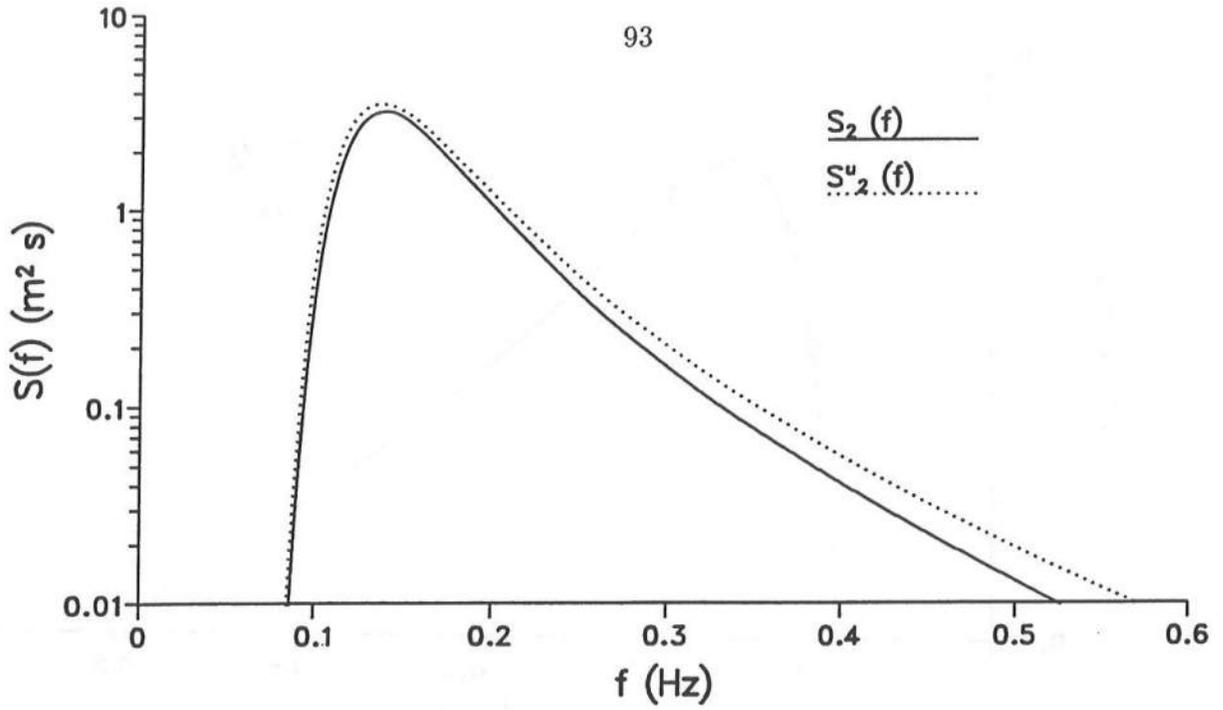


Figure B.1: Refracted Frequency Spectrum Versus Shoaled Uni-Directional Frequency Spectrum at Depth 2, $\alpha_p = 0^\circ$

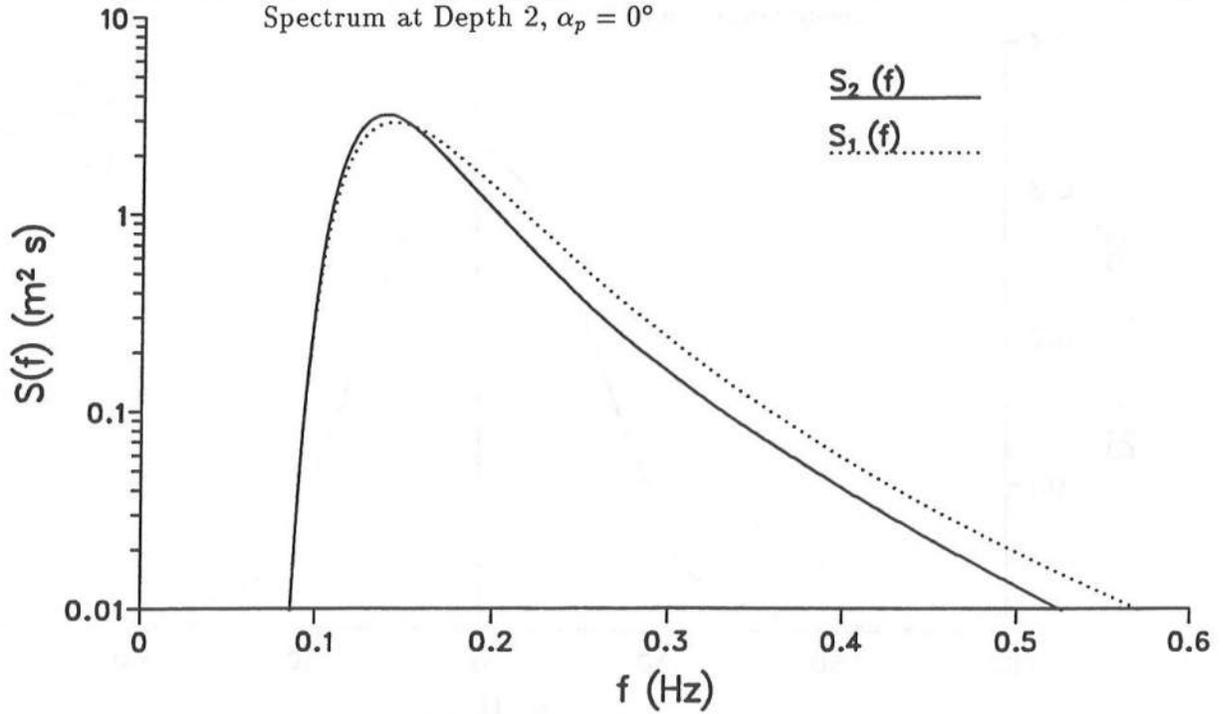


Figure B.2: Refracted Frequency Spectrum at Depth 2 Versus Incident Frequency Spectrum at Depth 1, $\alpha_p = 0^\circ$

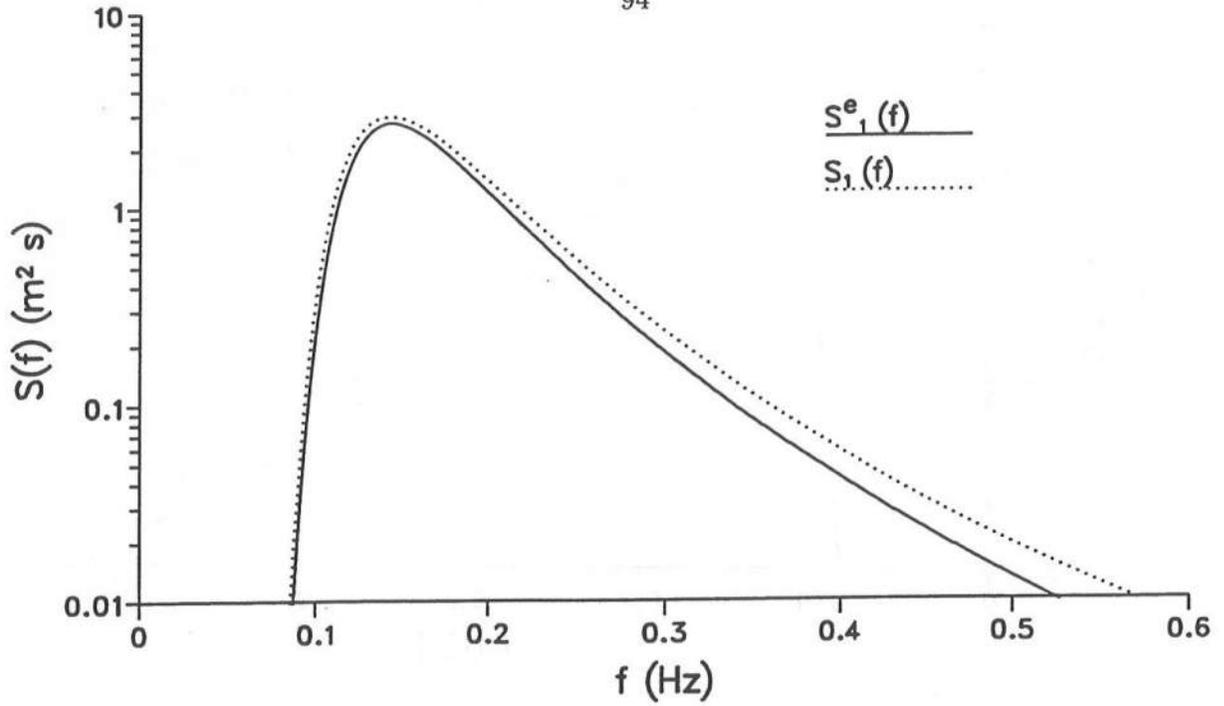


Figure B.3: Equivalent Uni-Directional Frequency Spectrum Versus Incident Frequency Spectrum at Depth 1, $\alpha_p = 0^\circ$

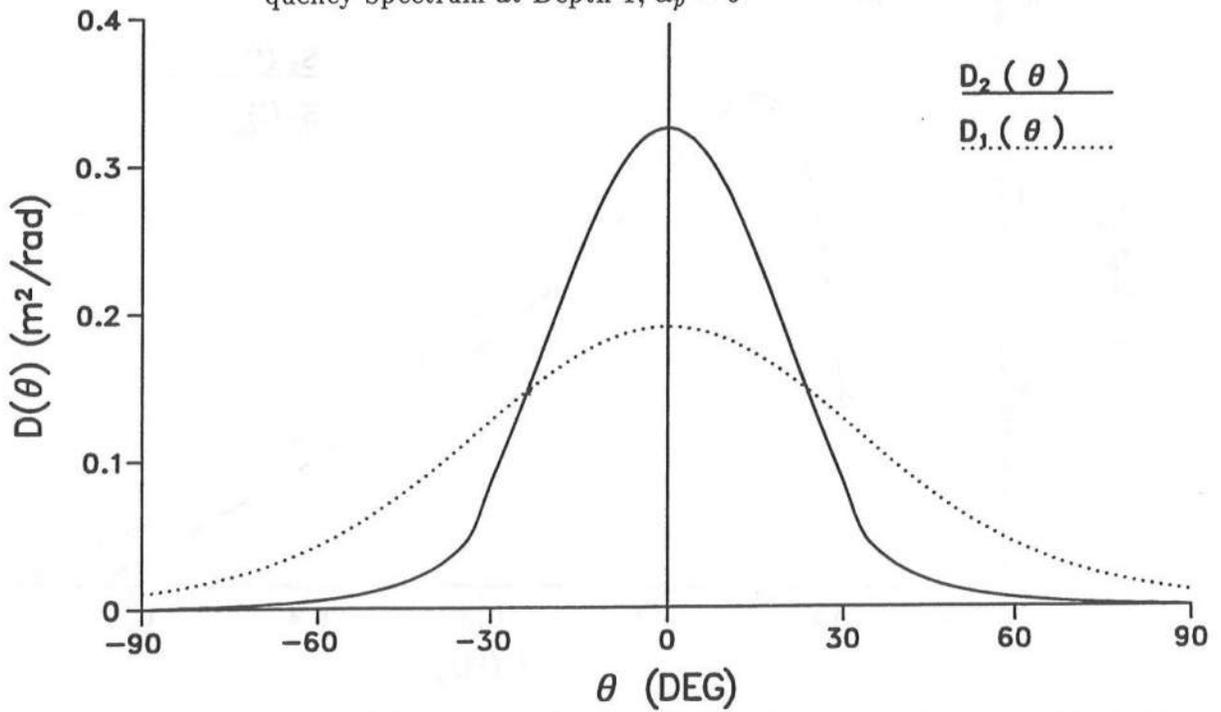


Figure B.4: Energy Distribution Function at Depth 2 Versus Energy Distribution Function at Depth 1, $\alpha_p = 0^\circ$

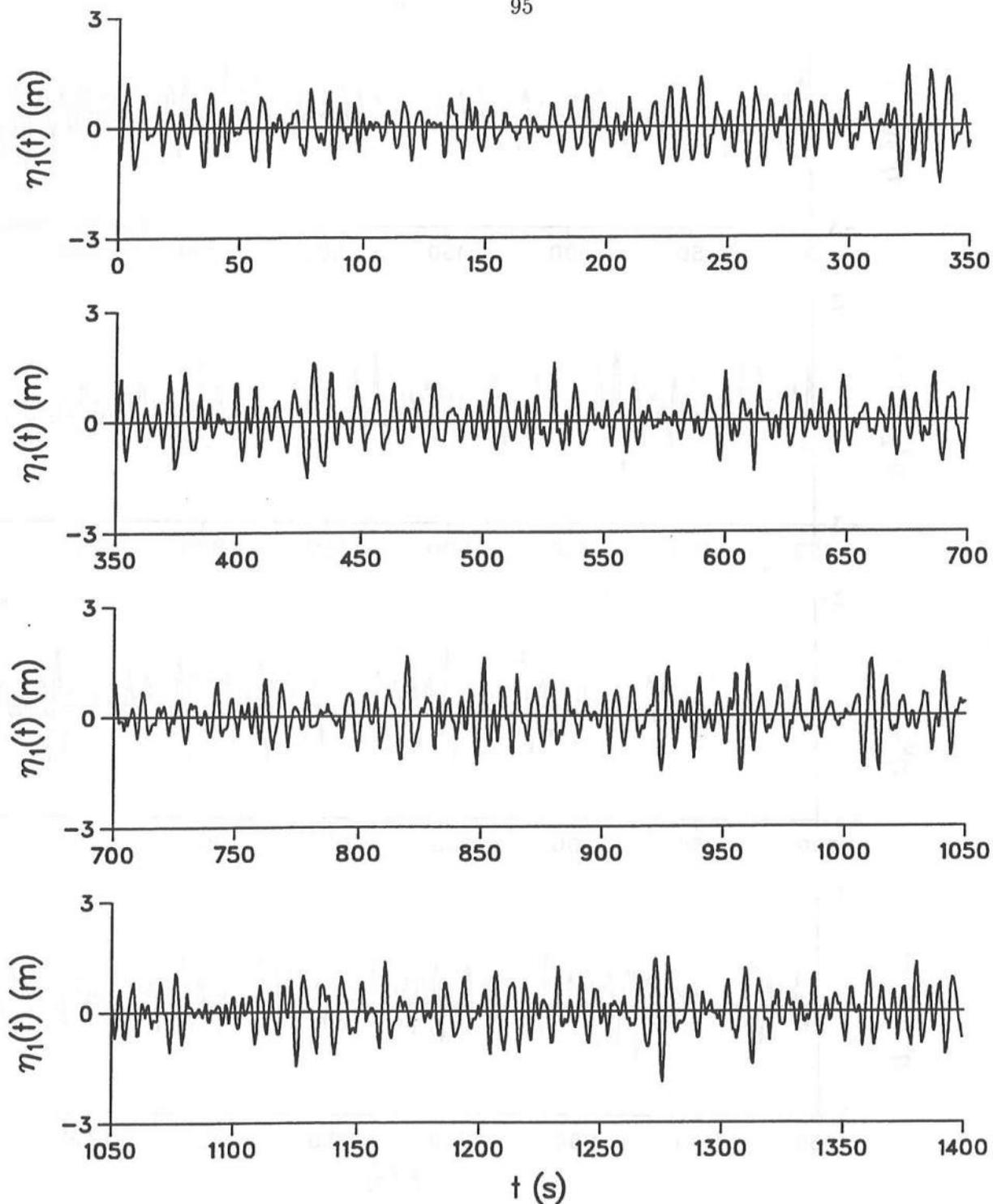


Figure B.5: Time Series Generated From Incident Frequency Spectrum at Depth 1, $\alpha_p = 0^\circ$

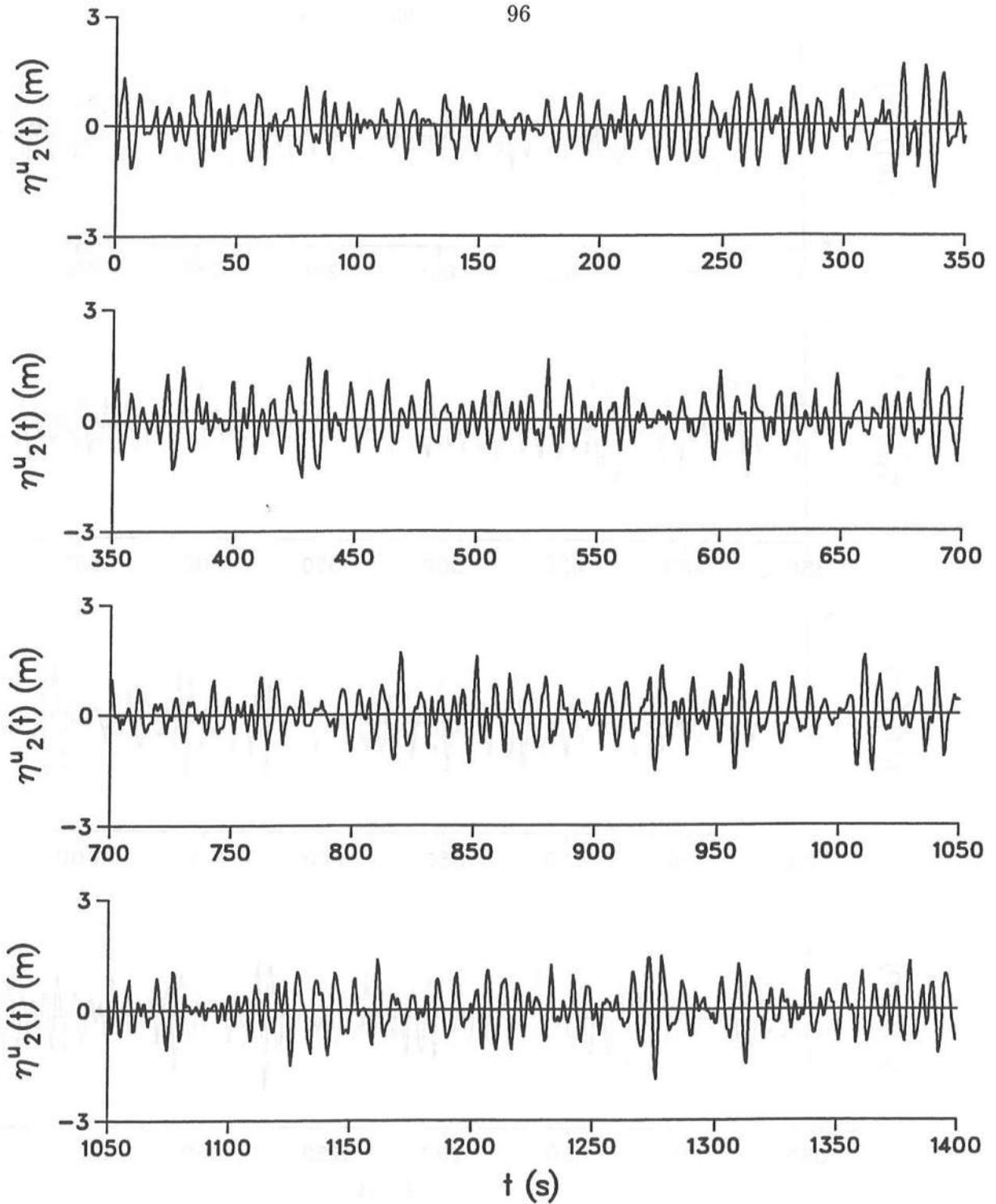


Figure B.6: Time Series Generated From Shoaled Uni-Directional Frequency Spectrum at Depth 2, $\alpha_p = 0^\circ$

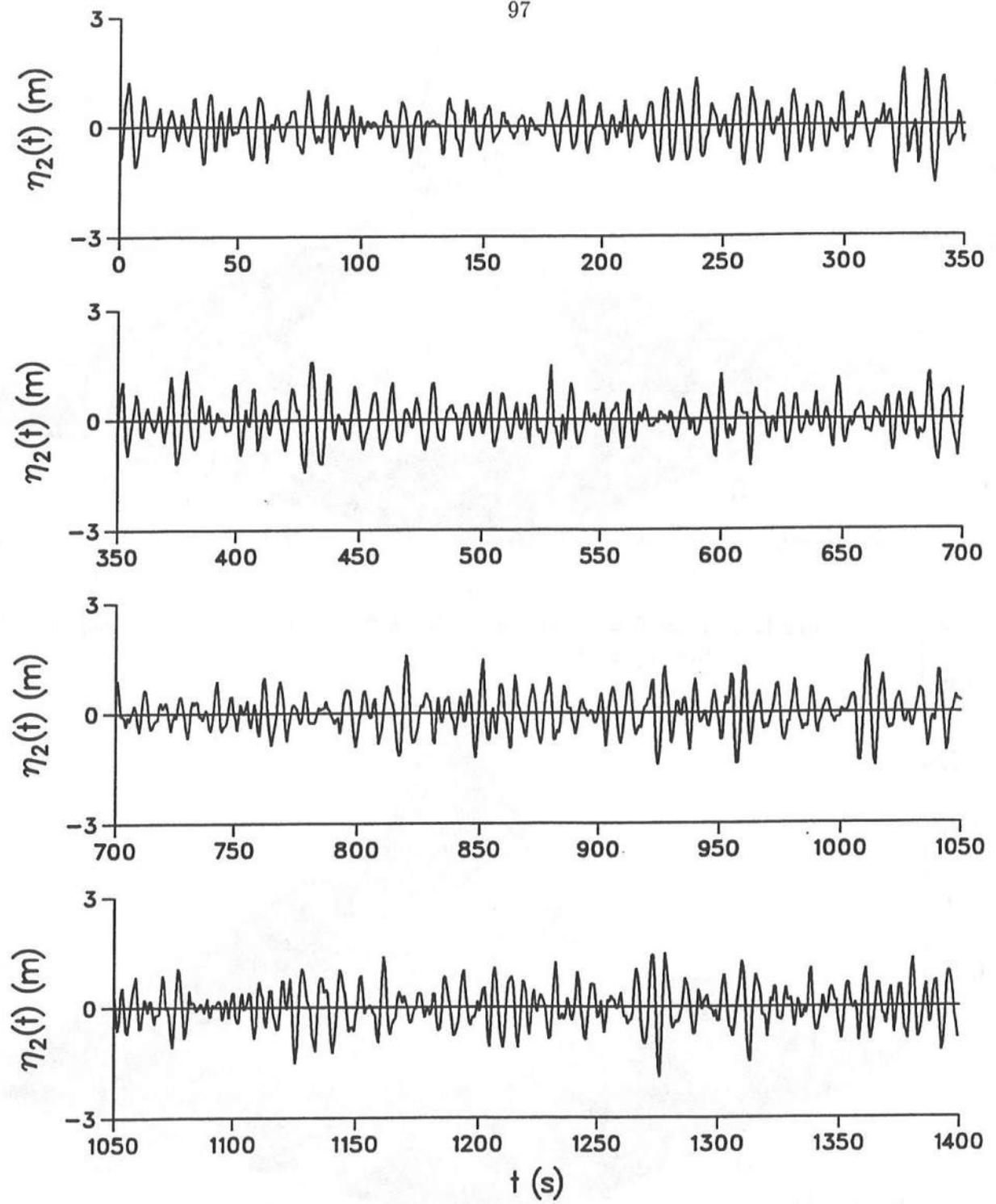


Figure B.7: Time Series Generated From Refracted Frequency Spectrum at Depth 2, $\alpha_p = 0^\circ$

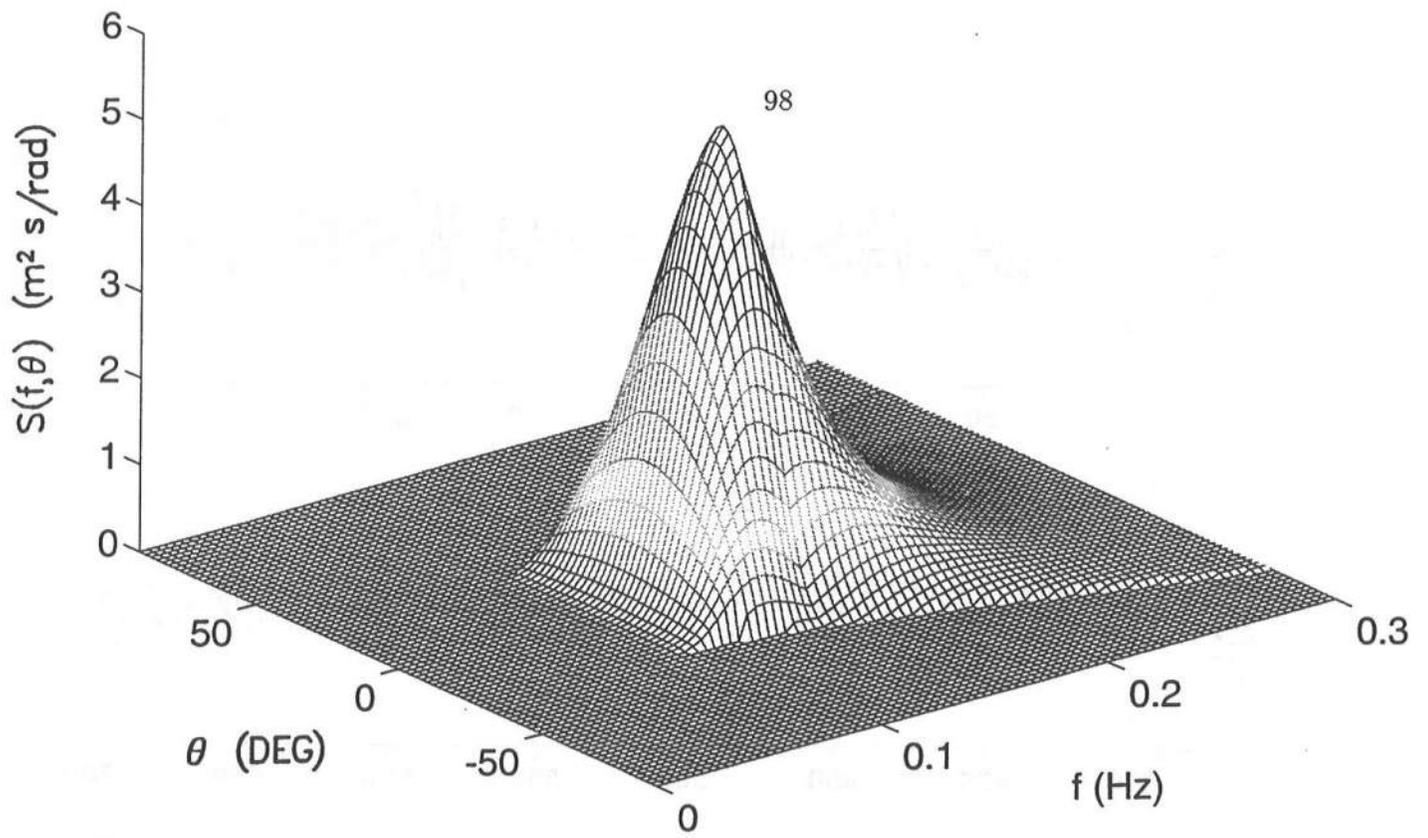


Figure B.8: Directional Spectrum at Depth 2 as a Function of Frequency and Direction, $\alpha_p = 0^\circ$

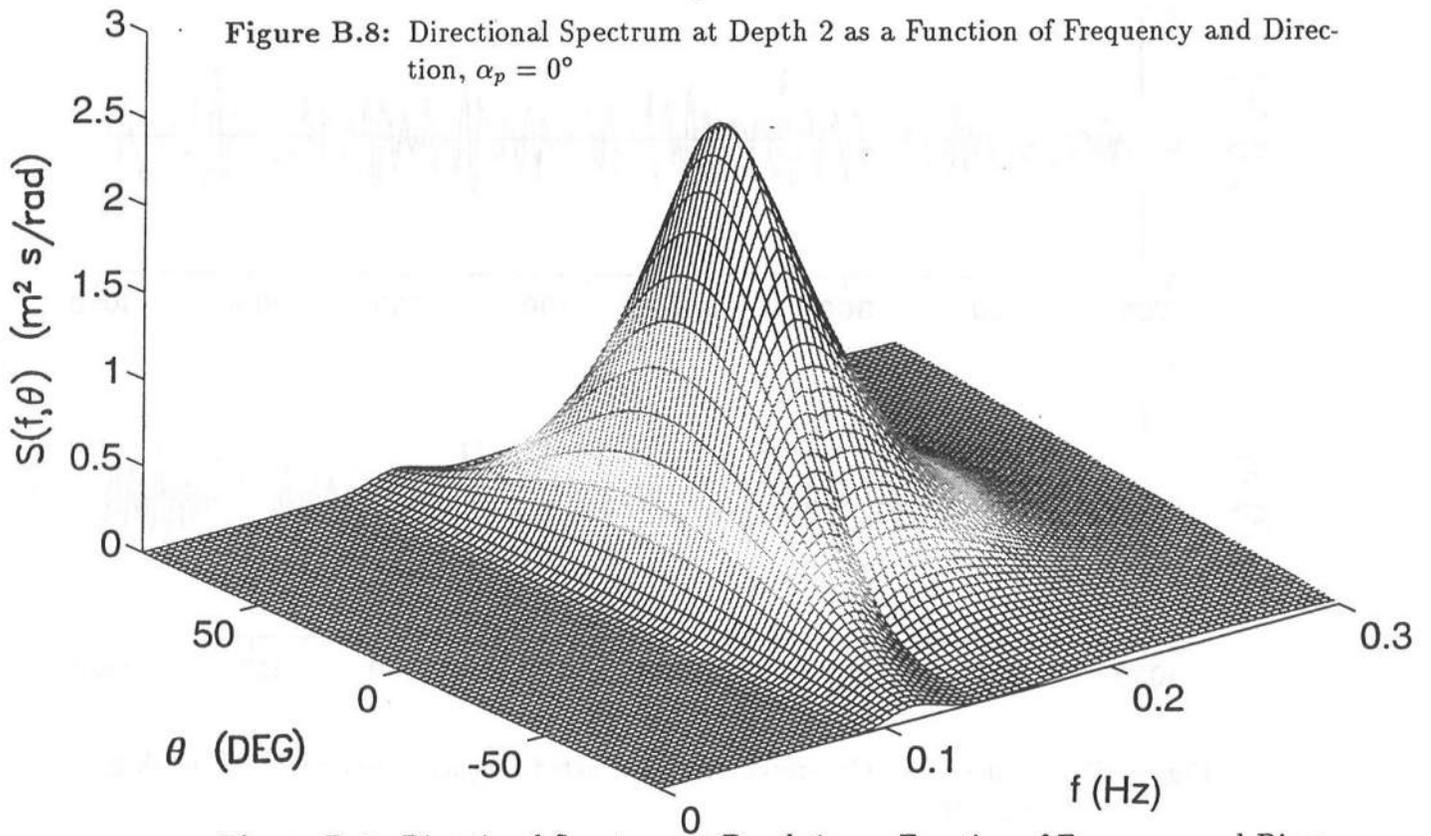


Figure B.9: Directional Spectrum at Depth 1 as a Function of Frequency and Direction, $\alpha_p = 0^\circ$

Table B.7: INPUT PARAMETERS: $\alpha_p = 45^\circ$

20.00000000		--> H1 (M)
4.14999962		--> H2 (M)
2.15999985	7.00000000	--> HM01 (M), TP1 (S)
1.00000000		--> GAMMA
1		--> IDEEP
10.00000000		--> SMAX
45.00000000		--> ALPHA1 (DEG)
0.03000000		--> SLOPE
13579		--> IS
2001		--> NO. OF FRQ.
181		--> NO. OF DIR.
0.00000000	1.42857075	--> FMIN (HZ), FMAX (HZ)
-89.99995420	89.99995420	--> THETAMIN (DEG), THETAMAX (DEG)

Table B.8: SPECTRAL PARAMETERS: $\alpha_p = 45^\circ$

SPECTRAL PARAMETERS	INCIDENT SPECTRUM	SHOALED SPECTRUM	REFRACTED SPECTRUM
DEPTH (M)	20.00000	4.15000	4.15000
EP	0.79736	0.81352	0.79817
VU	0.41065	0.42180	0.40815
Qp	2.00051	2.09054	2.14144
ER	0.53947	0.55447	0.45305
HR	1.52586	1.56828	1.28141
HMO	2.16005	2.22010	1.81399
T1	5.40948	5.66035	5.66500
T2	5.00399	5.21538	5.24496
TP	7.00000	7.32985	7.21650
FP	0.14286	0.13643	0.13857
ALPHA	0.78540	0.00000	0.43633
KAPPA	0.42358	0.45513	0.46152

Table B.9: TIME SERIES PARAMETERS: $\alpha_p = 45^\circ$

TIME SERIES PARAMETERS	INCIDENT SPECTRUM	SHOALED SPECTRUM	REFRACTED SPECTRUM
WATER DH (M)	20.00000	4.15000	4.15000
SD	0.00000	0.00000	0.00000
ER	0.53939	0.55439	0.45294
NZ	275.000	267.000	264.000
HB	1.32407	1.34429	1.10895
TB	5.09091	5.24345	5.30303
HV	1.47857	1.50866	1.23888
HS	2.07343	2.12555	1.73906
T3	6.24178	6.49121	6.47176
HT	2.55849	2.63555	2.14936
TT	6.26641	6.43732	6.41912
NK	26.000	24.000	24.000
M.R.L.	1.34615	1.29167	1.29167

Table B.10: RUN LENGTH STATISTICS: $\alpha_p = 45^\circ$

EVENT	INCIDENT WAVES	SHOALED WAVES	REFRACTED WAVES
WATER DH (M)	20.00000	4.15000	4.15000
1	1	1	1
2	1	1	1
3	1	1	1
4	1	2	2
5	2	1	1
6	1	1	1
7	1	1	1
8	1	2	2
9	2	1	1
10	1	2	2
11	1	1	1
12	3	1	1
13	1	1	1
14	1	1	1
15	1	2	2
16	1	2	2
17	2	2	2
18	2	1	1
19	2	2	2
20	1	1	1
21	2	1	1
22	1	1	1
23	1	1	1
24	2	1	1
25	1	0	0
26	1	0	0
MEAN RUN LTH	1.34615	1.29167	1.29167

Table B.11: WAVE STATISTICS: INCIDENT VS. SHOALED: $\alpha_p = 45^\circ$

INC SPECTRUM		SHOALED SPECTRUM					
DEPTH(M)	20.00000		4.15000				
RANK	Tr	Hr	Tr	Hr	Hb	Ib	
1	5.744	3.516	5.803	3.516	3.089	1	
2	6.138	3.176	7.236	3.407	3.317	1	
3	7.108	3.135	6.211	3.284	3.167	1	
4	6.775	2.951	7.229	3.117	3.316	0	
5	7.187	2.886	6.800	2.888	3.260	0	
6	6.307	2.760	6.435	2.851	3.205	0	
7	5.403	2.684	6.632	2.755	3.236	0	
8	6.029	2.606	6.428	2.690	3.204	0	
9	7.910	2.602	6.322	2.657	3.187	0	
10	6.496	2.577	6.252	2.642	3.174	0	
11	5.102	2.534	6.149	2.616	3.156	0	
12	5.985	2.529	7.797	2.604	3.377	0	
13	5.046	2.526	7.879	2.602	3.385	0	
14	6.776	2.489	6.938	2.596	3.279	0	
15	7.789	2.460	7.113	2.585	3.302	0	
16	5.959	2.457	5.227	2.506	2.951	0	
17	7.040	2.417	5.093	2.418	2.914	0	
18	4.628	2.400	7.014	2.385	3.289	0	
19	5.503	2.366	7.018	2.373	3.290	0	
20	6.940	2.326	7.756	2.342	3.373	0	
21	4.977	2.276	4.862	2.341	2.845	0	
22	5.857	2.274	5.564	2.305	3.036	0	
23	5.477	2.258	5.178	2.280	2.938	0	
24	6.337	2.233	6.086	2.260	3.145	0	
25	5.973	2.225	6.016	2.256	3.131	0	

Table B.12: WAVE STATISTICS: INCIDENT VS. REFRACTED: $\alpha_p = 45^\circ$

		INC SPECTRUM		REFRACTED SPECTRUM			
DEPTH(M)		20.00000		4.15000			
RANK	Tr	Hr	Tr	Hr	Hb	Ib	
1	5.744	3.516	5.815	2.907	3.091	0	
2	6.138	3.176	7.200	2.745	3.312	0	
3	7.108	3.135	6.207	2.697	3.167	0	
4	6.775	2.951	7.209	2.529	3.313	0	
5	7.187	2.886	6.775	2.367	3.257	0	
6	6.307	2.760	6.427	2.334	3.204	0	
7	5.403	2.684	6.614	2.236	3.233	0	
8	6.029	2.606	6.348	2.166	3.191	0	
9	7.910	2.602	6.226	2.163	3.170	0	
10	6.496	2.577	6.233	2.147	3.171	0	
11	5.102	2.534	6.906	2.117	3.275	0	
12	5.985	2.529	7.857	2.116	3.383	0	
13	5.046	2.526	7.785	2.116	3.376	0	
14	6.776	2.489	7.089	2.108	3.299	0	
15	7.789	2.460	6.125	2.108	3.152	0	
16	5.959	2.457	5.230	2.051	2.952	0	
17	7.040	2.417	5.135	2.003	2.926	0	
18	4.628	2.400	6.987	1.947	3.286	0	
19	5.503	2.366	6.996	1.927	3.287	0	
20	6.940	2.326	5.593	1.919	3.043	0	
21	4.977	2.276	4.878	1.916	2.849	0	
22	5.857	2.274	7.750	1.895	3.373	0	
23	5.477	2.258	5.162	1.851	2.934	0	
24	6.337	2.233	6.012	1.850	3.131	0	
25	5.973	2.225	6.325	1.839	3.187	0	

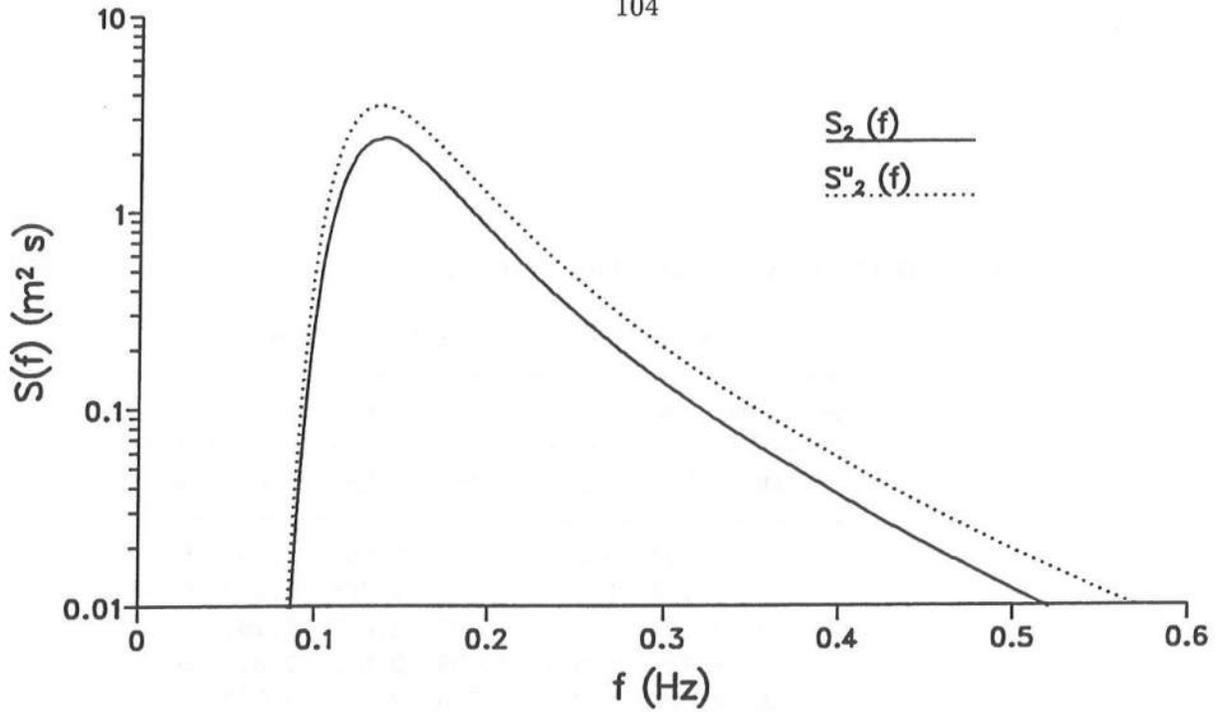


Figure B.10: Refracted Frequency Spectrum Versus Shoaled Uni-Directional Frequency Spectrum at Depth 2, $\alpha_p = 45^\circ$

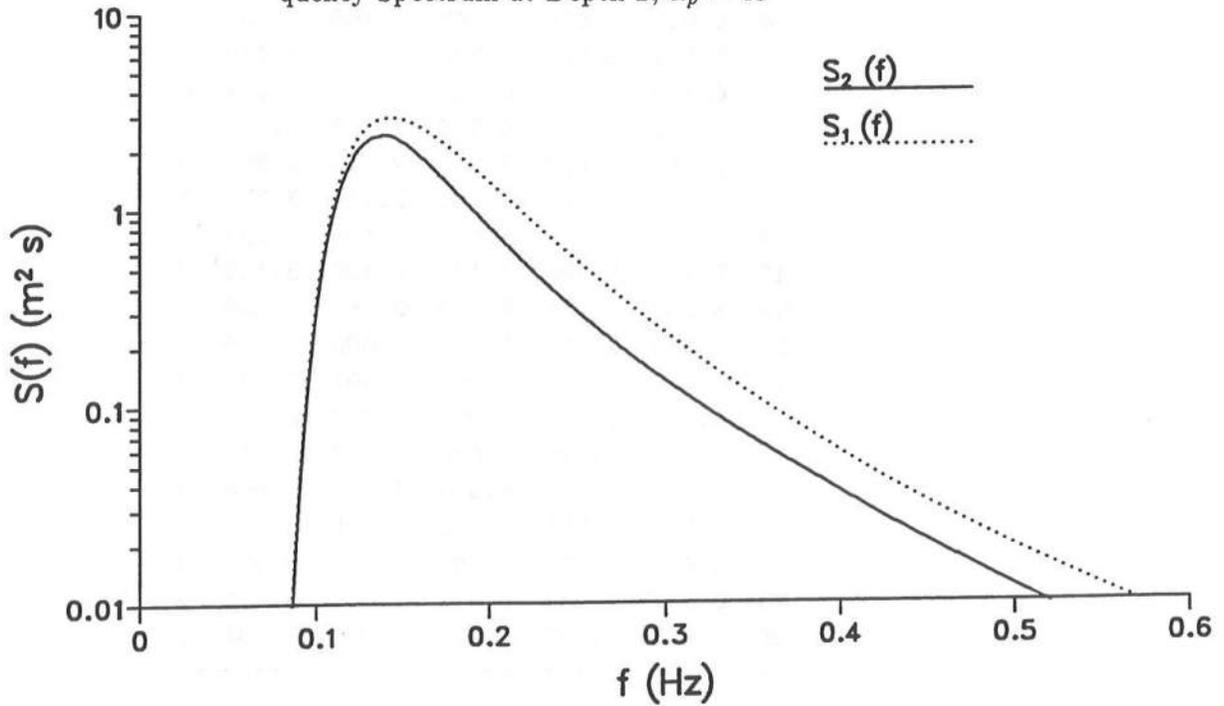


Figure B.11: Refracted Frequency Spectrum at Depth 2 Versus Incident Frequency Spectrum at Depth 1, $\alpha_p = 45^\circ$

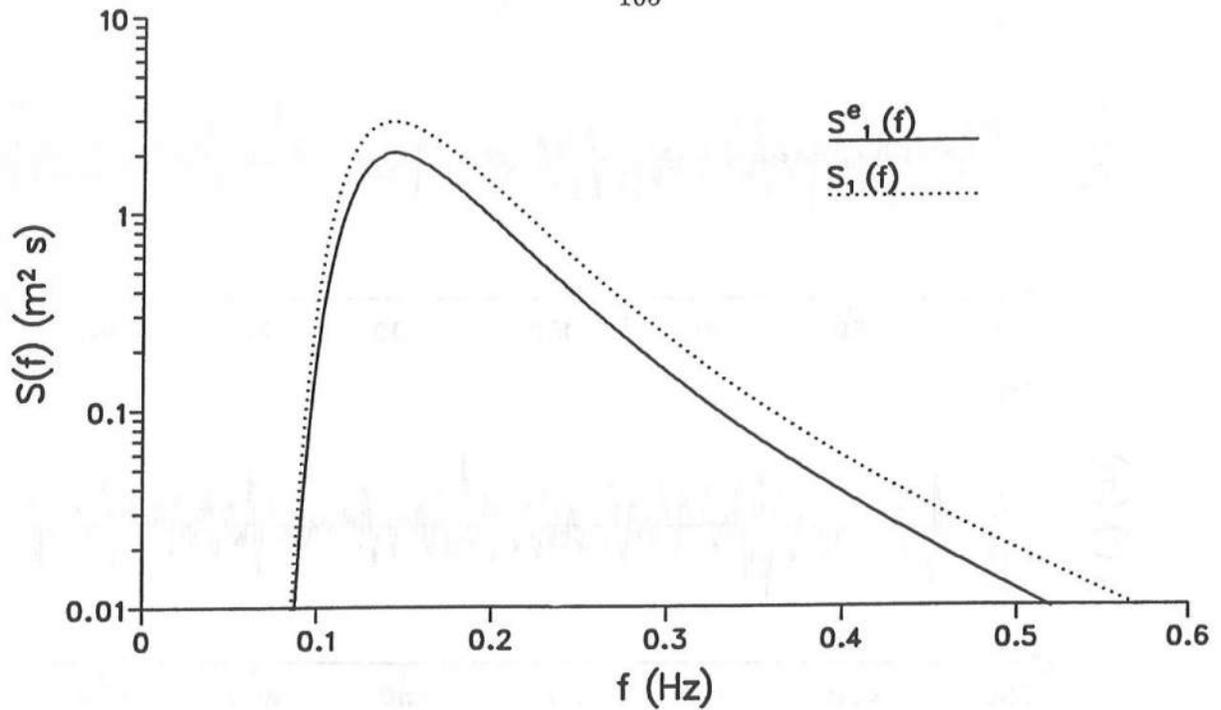


Figure B.12: Equivalent Uni-Directional Frequency Spectrum Versus Incident Frequency Spectrum at Depth 1, $\alpha_p = 45^\circ$

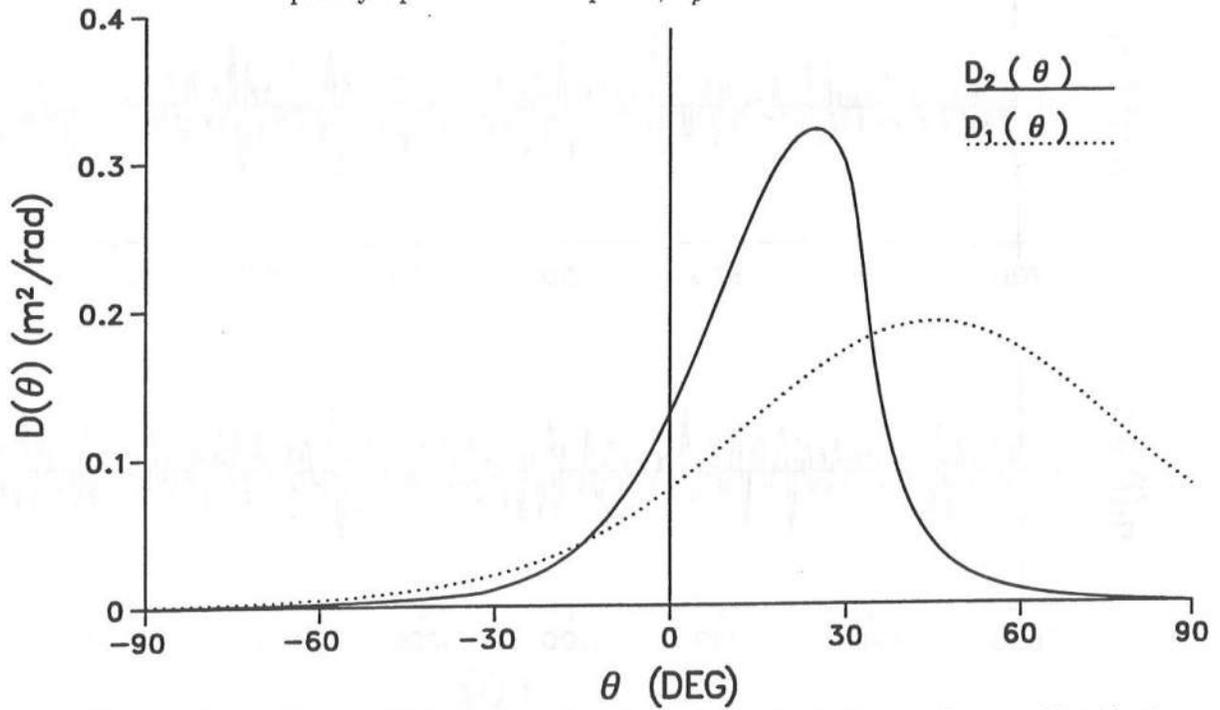


Figure B.13: Energy Distribution Function at Depth 2 Versus Energy Distribution Function at Depth 1, $\alpha_p = 45^\circ$

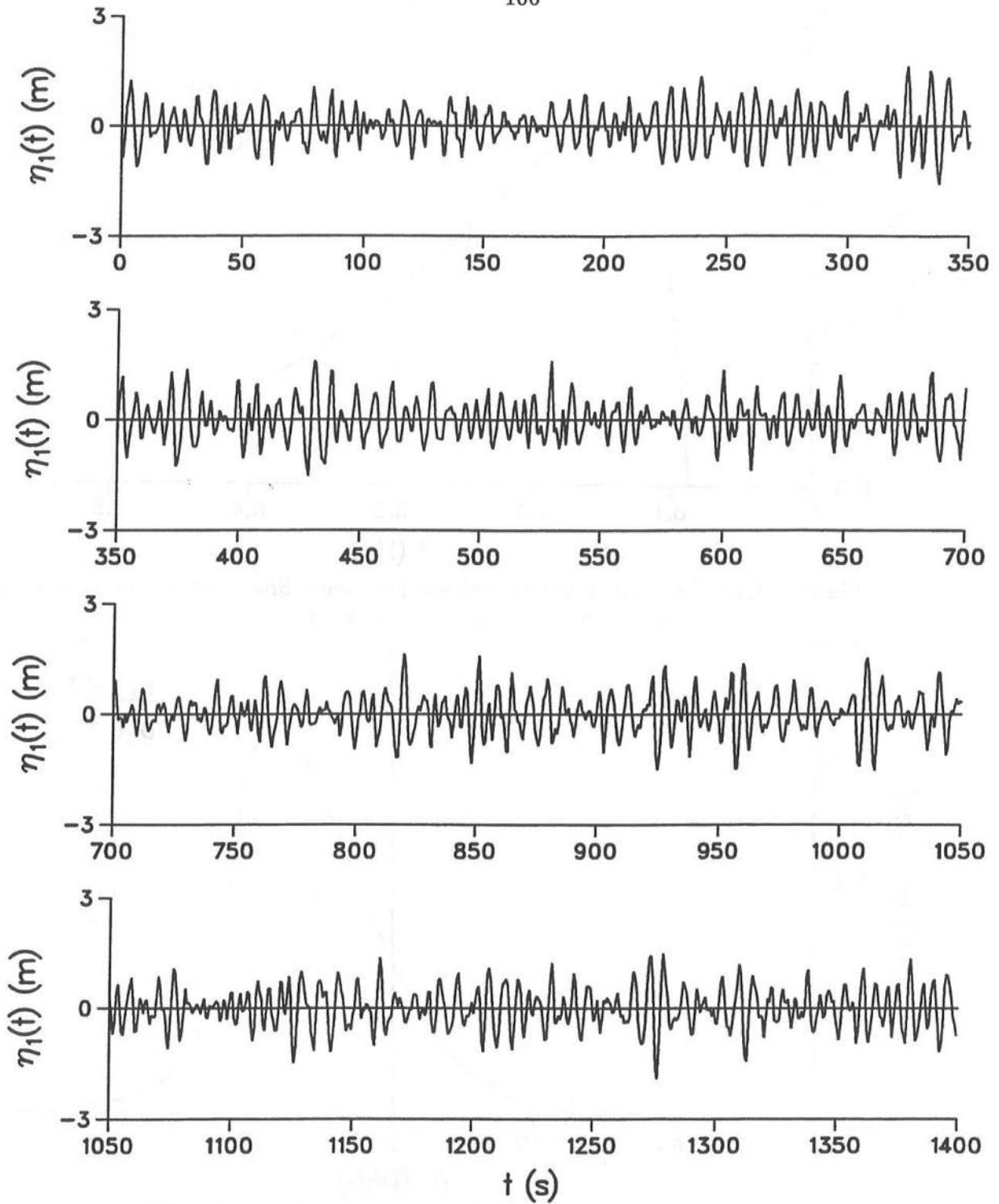


Figure B.14: Time Series Generated From Frequency Spectrum at Depth 1, $\alpha_p = 45^\circ$

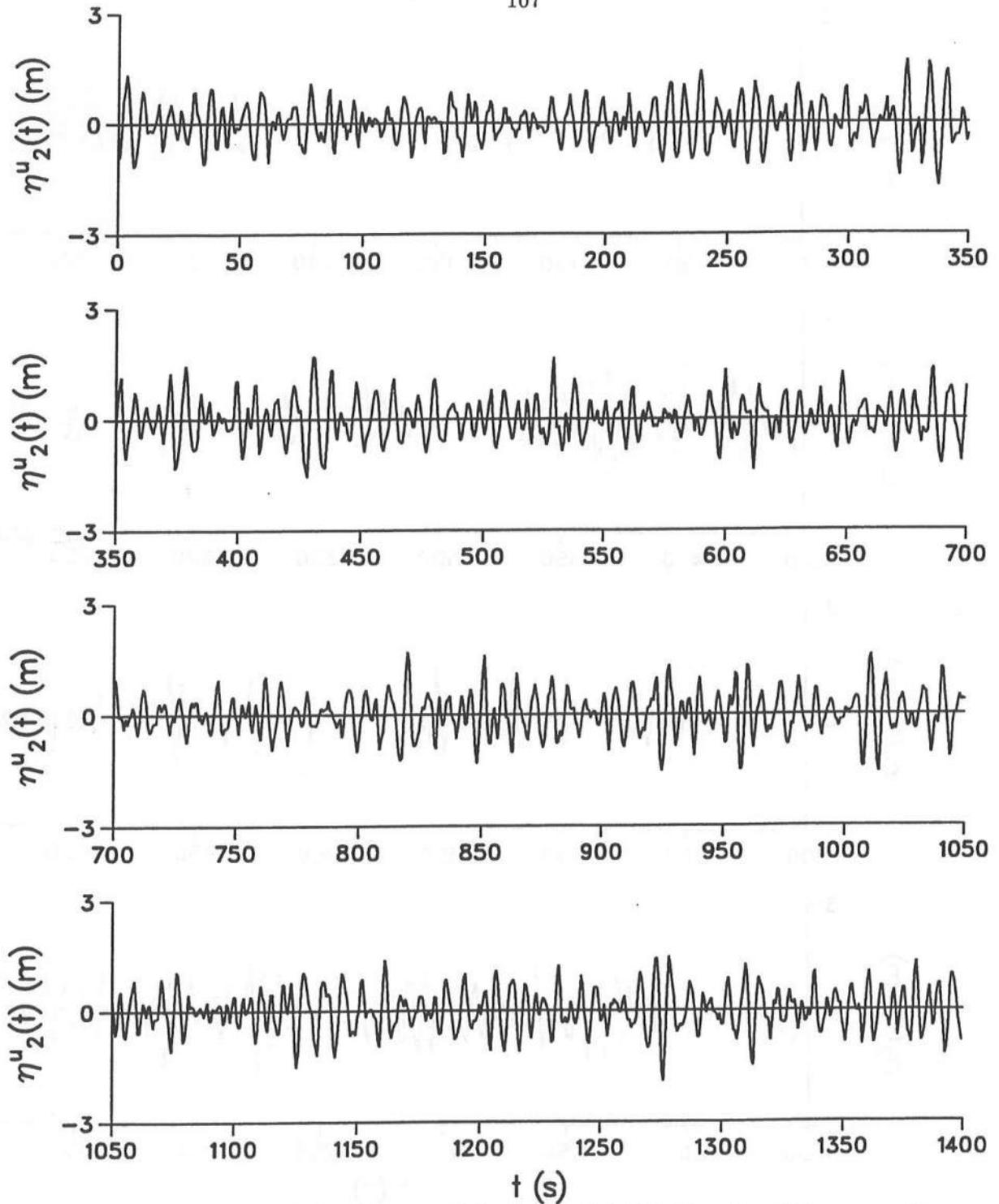


Figure B.15: Time Series Generated From Shoaled Uni-Directional Frequency Spectrum at Depth 2, $\alpha_p = 45^\circ$

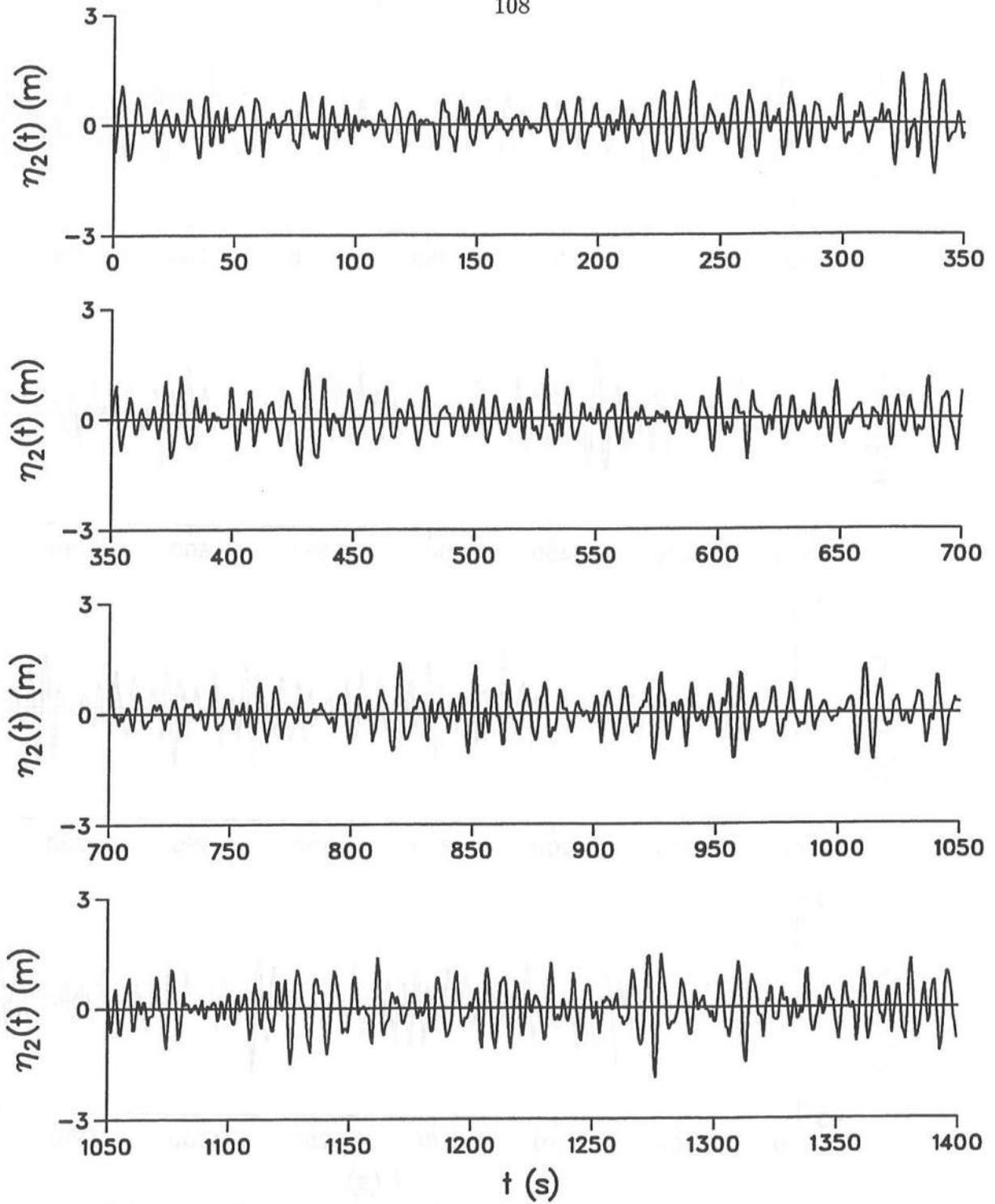


Figure B.16: Time Series Generated From Incident Refracted Frequency Spectrum at Depth 2, $\alpha_p = 45^\circ$

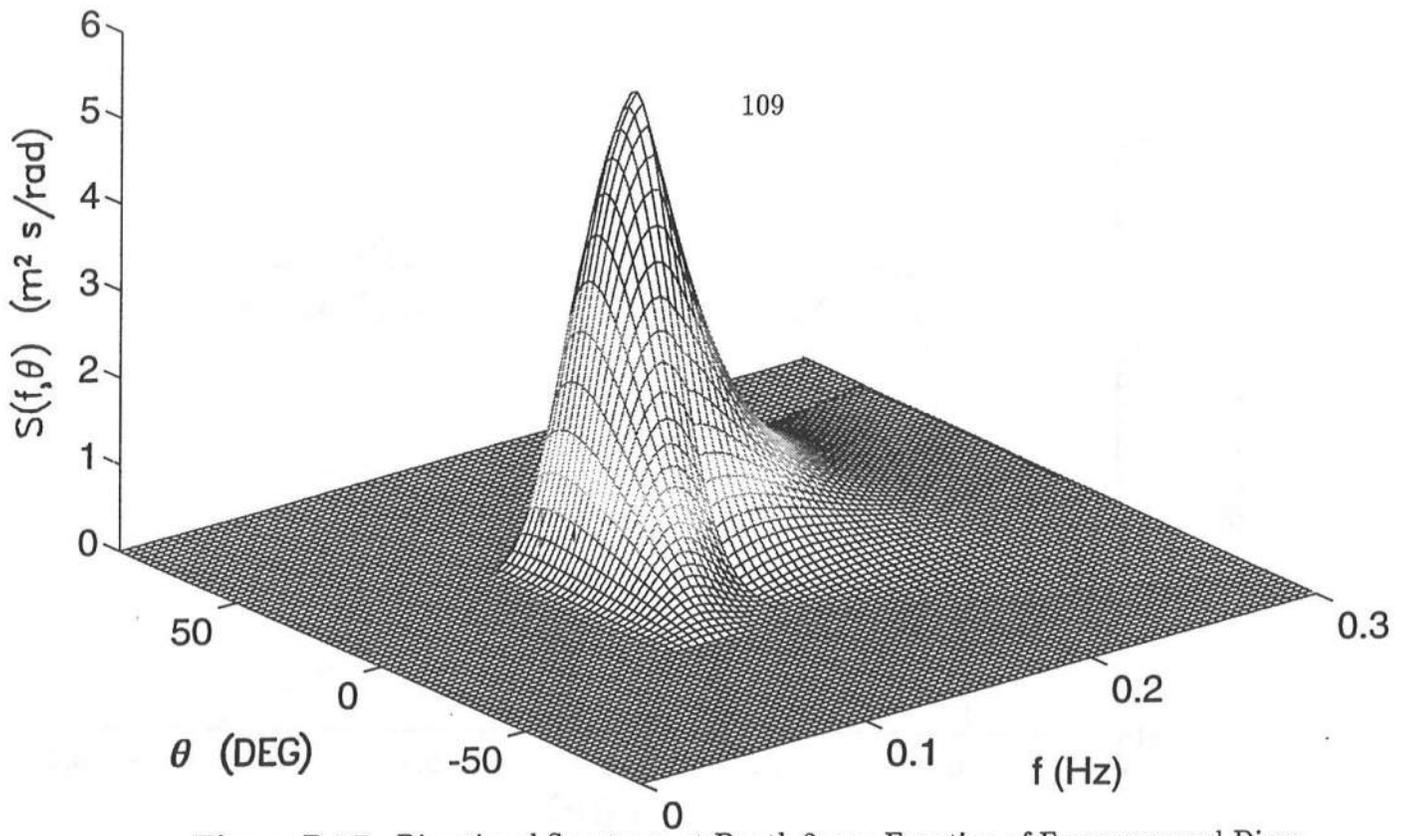


Figure B.17: Directional Spectrum at Depth 2 as a Function of Frequency and Direction, $\alpha_p = 45^\circ$

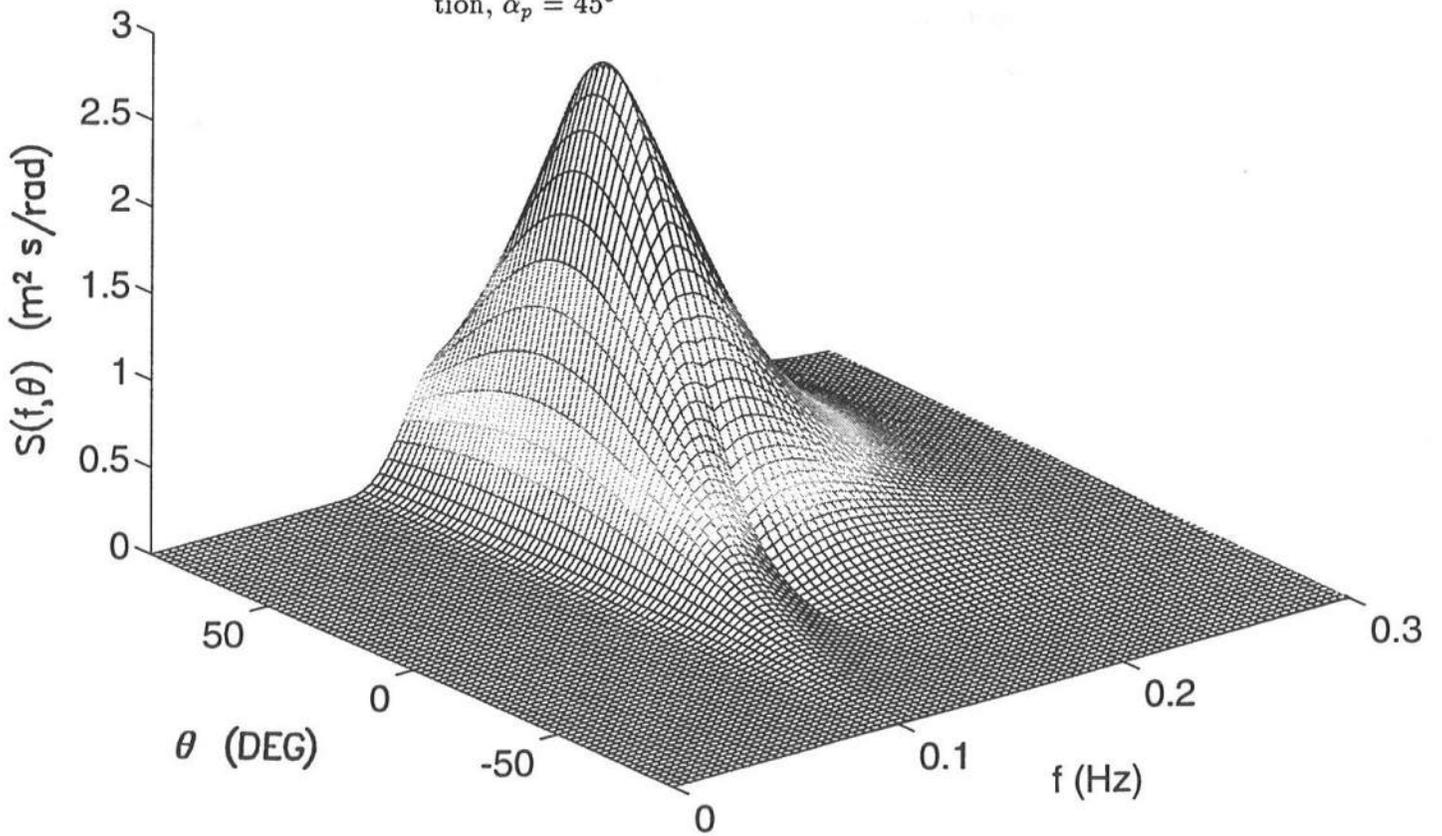


Figure B.18: Directional Spectrum at Depth 1 as a Function of Frequency and Direction, $\alpha_p = 45^\circ$

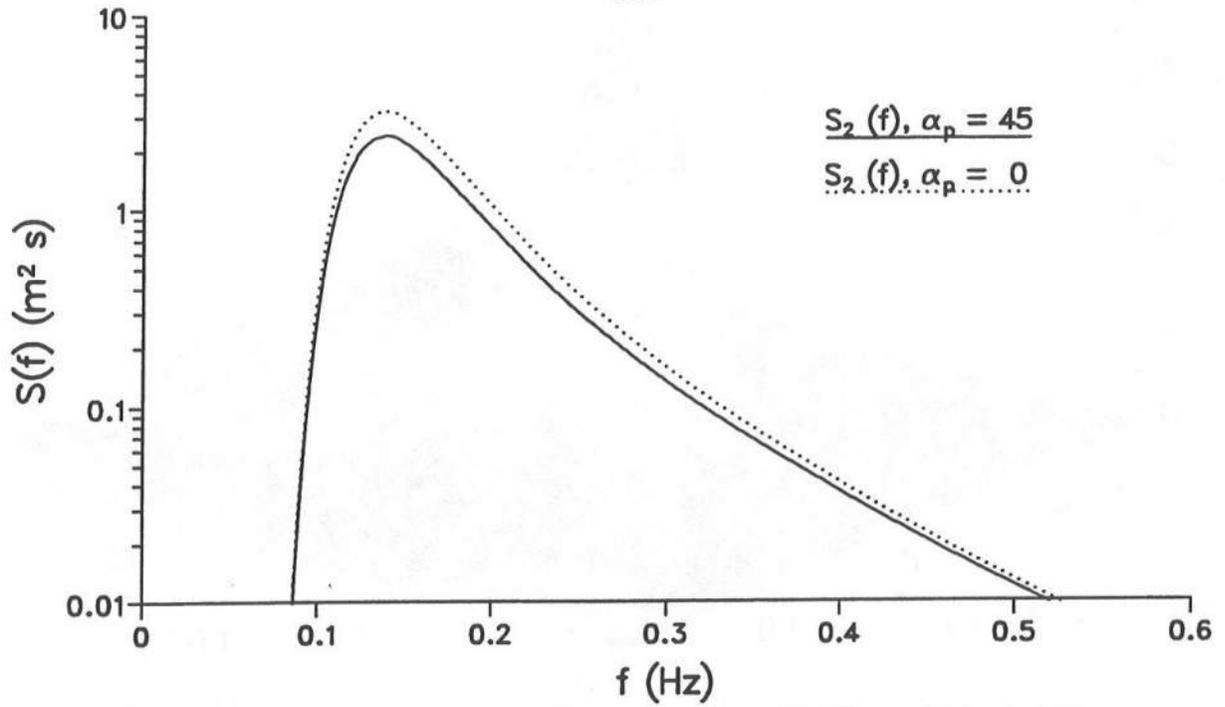


Figure B.19: Refracted Frequency Spectrum, $\alpha_p = 45^\circ$, Versus Refracted Frequency Spectrum, $\alpha_p = 0^\circ$

Appendix C

ANALYZED RANDOM WAVE DATA: LABORATORY EXAMPLE

This appendix contains the random wave data for one laboratory case corresponding to Run SN7 in Poff and Kobayashi (1993). The following tables are included:

1. Input Parameters.
2. Spectral Parameters.
3. Time Series Parameters.
4. Run Length Statistics.
5. Ranked Wave Heights and Breaker Heights for Incident Versus Shoaled Uni-Directional Frequency Spectra.
6. Ranked Wave Heights and Breaker Heights for Incident Versus Refracted Directional Frequency Spectra.

Also, the following figures are included for this case:

1. Refracted Frequency Spectrum Versus Shoaled Uni-Directional Frequency Spectrum at Depth 2.
2. Refracted Frequency Spectrum at Depth 2 Versus Incident Frequency Spectrum at Depth 1.

3. Equivalent Uni-Directional Frequency Spectrum Versus Incident Frequency Spectrum at Depth 1.
4. Energy Distribution Function at Depth 2 Versus Energy Distribution Function at Depth 1.
5. Time Series Generated From Incident Frequency Spectrum at Depth 1.
6. Time Series Generated From Shoaled Uni-Directional Frequency Spectrum at Depth 2.
7. Time Series Generated From Refracted Frequency Spectrum at Depth 2.
8. Directional Spectrum at Depth 2 as a Function of Frequency and Direction.
9. Directional Spectrum at Depth 1 as a Function of Frequency and Direction.

Table C.1: INPUT PARAMETERS

0.42000002		--> H1 (M)
0.30000001		--> H2 (M)
0.12000000	2.00000000	--> HMO1 (M), TP1 (S)
20.00000000		--> GAMMA
0		--> IDEEP
10.00000000		--> SMAX
0.00000000		--> ALPHA1 (DEG)
0.04250000		--> SLOPE
13579		--> IS
2001		--> NO. OF FRQ.
181		--> NO. OF DIR.
0.00000000	5.00000000	--> FMIN (HZ), FMAX (HZ)
-89.99995420	89.99995420	--> THETAMIN (DEG), THETAMAX (DEG)

Table C.2: SPECTRAL PARAMETERS

SPECTRAL PARAMETERS	INCIDENT SPECTRUM	SHOALED SPECTRUM	REFRACTED SPECTRUM
DEPTH (M)	0.42000	0.30000	0.30000
EP	0.82695	0.82575	0.79121
VU	0.41175	0.39998	0.35735
Qp	5.89288	6.13025	6.47609
ER	0.02997	0.03124	0.03021
HR	0.08477	0.08836	0.08545
HMO	0.12000	0.12508	0.12096
T1	1.66130	1.68688	1.72719
T2	1.53617	1.56624	1.62646
TP	2.00000	1.99005	1.99005
FP	0.50000	0.50250	0.50250
ALPHA	0.00000	0.00000	0.00000
KAPPA	0.70083	0.71635	0.73282

Table C.3: TIME SERIES PARAMETERS

TIME SERIES PARAMETERS	INCIDENT SPECTRUM	SHOALED SPECTRUM	REFRACTED SPECTRUM
DEPTH (M)	0.42000	0.30000	0.30000
SD	0.00000	0.00000	0.00000
ER	0.02997	0.03124	0.03021
NZ	254.000	253.000	241.000
HB	0.07425	0.07658	0.07566
TB	1.57480	1.58103	1.65975
HV	0.08289	0.08588	0.08400
HS	0.11550	0.12002	0.11627
T3	1.89689	1.89982	1.90405
HT	0.13959	0.14501	0.13993
TT	1.85849	1.87796	1.87948
NK	19.000	19.000	19.000
M.R.L.	1.73684	1.78947	1.78947

Table C.4: RUN LENGTH STATISTICS

EVENT	INCIDENT WAVES	SHOALED WAVES	REFRACTED WAVES
DEPTH (M)	0.42000	0.30000	0.30000
1	2	2	2
2	2	1	2
3	1	1	1
4	2	3	3
5	1	1	1
6	2	2	2
7	2	2	2
8	1	1	1
9	1	1	1
10	6	6	6
11	1	1	1
12	2	2	2
13	2	2	2
14	1	1	1
15	1	1	1
16	2	2	1
17	2	2	2
18	1	1	1
19	1	2	2
MEAN RUN LTH	1.73684	1.78947	1.78947

Table C.5: WAVE STATISTICS: INCIDENT VS. SHOALED

INC SPECTRUM		SHOALED SPECTRUM					
DEPTH(M)	0.42000		0.30000				
RANK	Tr	Hr	Tr	Hr	Hb	Ib	
1	1.723	0.182	1.731	0.190	0.246	0	
2	1.704	0.160	1.711	0.166	0.245	0	
3	1.810	0.158	1.815	0.165	0.250	0	
4	1.930	0.154	1.932	0.159	0.254	0	
5	1.899	0.149	1.903	0.155	0.253	0	
6	1.928	0.149	1.989	0.153	0.256	0	
7	1.991	0.146	1.924	0.152	0.254	0	
8	1.847	0.146	1.855	0.151	0.251	0	
9	1.842	0.142	1.958	0.146	0.255	0	
10	1.858	0.140	1.860	0.145	0.251	0	
11	1.957	0.139	1.849	0.144	0.251	0	
12	1.712	0.138	2.035	0.143	0.258	0	
13	2.040	0.137	1.723	0.141	0.245	0	
14	1.833	0.135	1.830	0.140	0.250	0	
15	2.148	0.135	2.143	0.139	0.261	0	
16	1.813	0.134	1.828	0.139	0.250	0	
17	1.852	0.132	1.852	0.139	0.251	0	
18	1.965	0.129	1.966	0.135	0.255	0	
19	1.480	0.128	1.744	0.133	0.246	0	
20	1.929	0.128	1.759	0.132	0.247	0	
21	1.756	0.128	1.998	0.132	0.257	0	
22	1.733	0.127	1.933	0.132	0.254	0	
23	2.001	0.126	1.925	0.132	0.254	0	
24	1.926	0.125	1.532	0.131	0.234	0	
25	1.785	0.124	2.155	0.129	0.261	0	

Table C.6: WAVE STATISTICS: INCIDENT VS. REFRACTED

INC SPECTRUM		REFRACTED SPECTRUM					
DEPTH(M)	0.42000		0.30000				
RANK	Tr	Hr	Tr	Hr	Hb	Ib	
1	1.723	0.182	1.739	0.184	0.246	0	
2	1.704	0.160	1.726	0.159	0.245	0	
3	1.810	0.158	1.823	0.159	0.250	0	
4	1.930	0.154	1.936	0.152	0.254	0	
5	1.899	0.149	1.906	0.149	0.253	0	
6	1.928	0.149	1.980	0.148	0.256	0	
7	1.991	0.146	1.915	0.145	0.254	0	
8	1.847	0.146	1.861	0.144	0.251	0	
9	1.842	0.142	1.958	0.142	0.255	0	
10	1.858	0.140	1.854	0.139	0.251	0	
11	1.957	0.139	1.854	0.138	0.251	0	
12	1.712	0.138	2.027	0.138	0.258	0	
13	2.040	0.137	1.851	0.137	0.251	0	
14	1.833	0.135	1.826	0.135	0.250	0	
15	2.148	0.135	1.840	0.133	0.251	0	
16	1.813	0.134	2.137	0.132	0.261	0	
17	1.852	0.132	1.738	0.131	0.246	0	
18	1.965	0.129	1.963	0.130	0.255	0	
19	1.480	0.128	1.926	0.129	0.254	0	
20	1.929	0.128	1.991	0.129	0.256	0	
21	1.756	0.128	1.763	0.128	0.247	0	
22	1.733	0.127	1.755	0.127	0.247	0	
23	2.001	0.126	1.934	0.125	0.254	0	
24	1.926	0.125	1.807	0.125	0.249	0	
25	1.785	0.124	1.583	0.124	0.237	0	

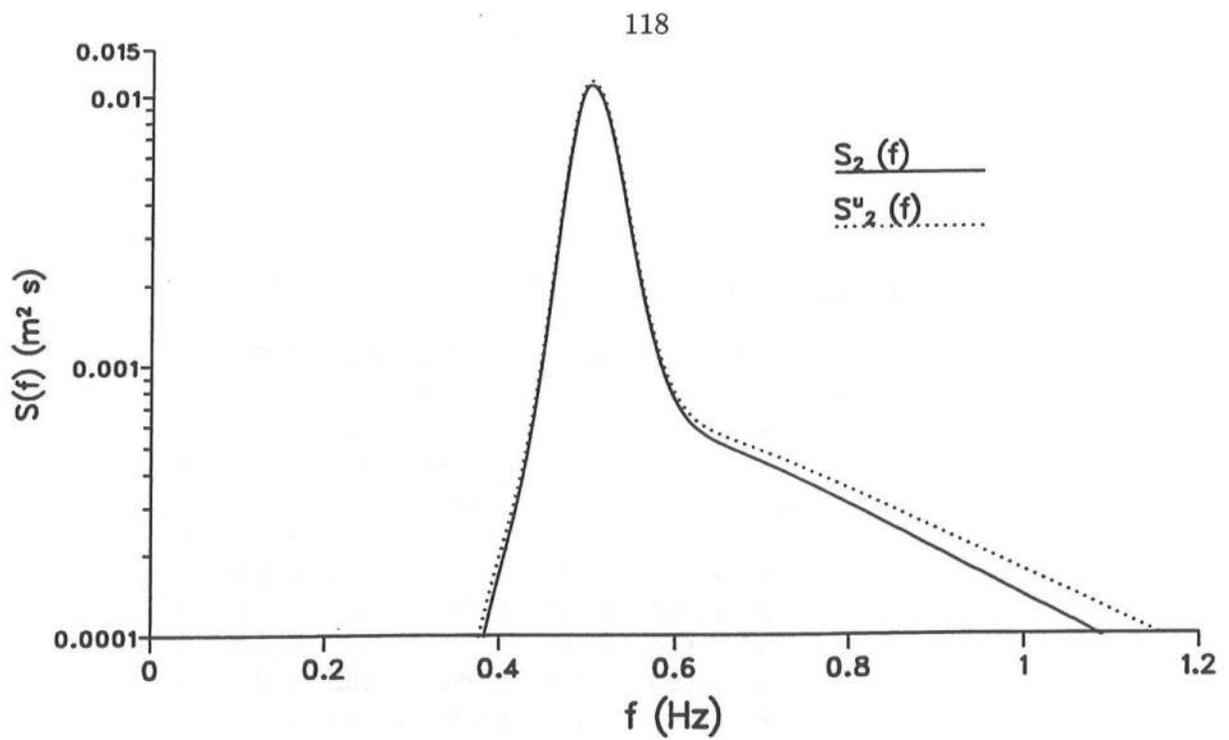


Figure C.1: Refracted Frequency Spectrum Versus Shoaled Uni-Directional Frequency Spectrum at Depth 2

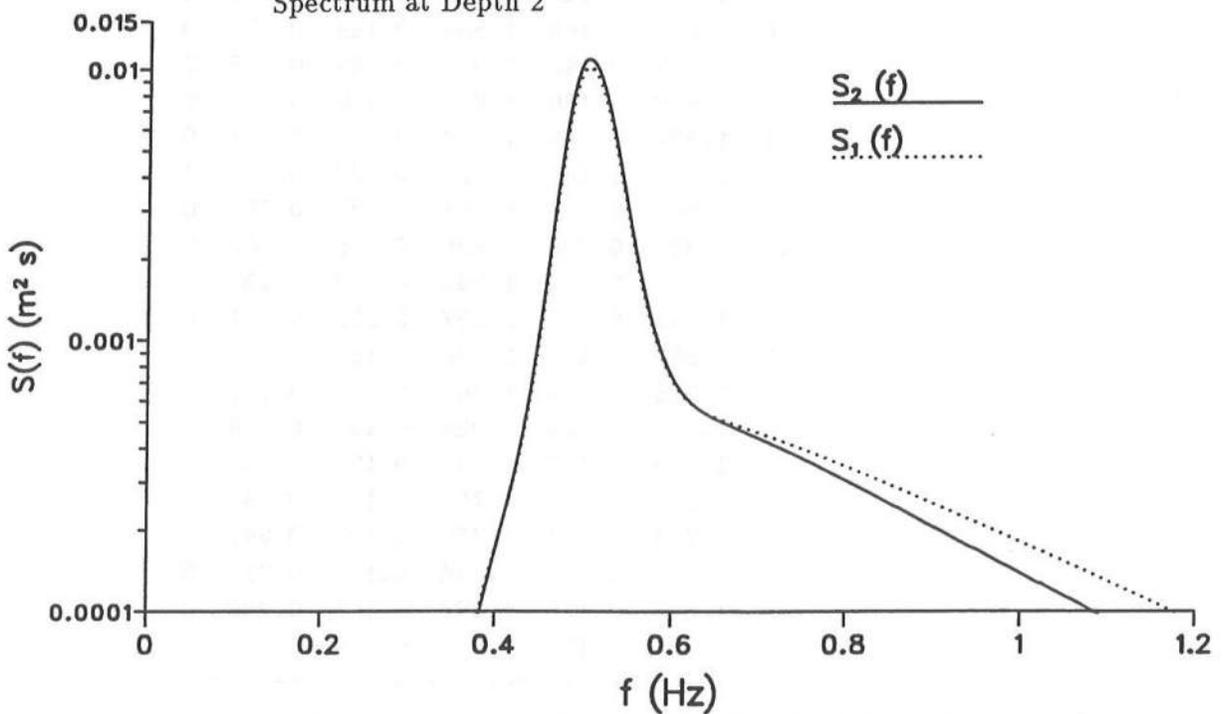


Figure C.2: Refracted Frequency Spectrum at Depth 2 Versus Incident Frequency Spectrum at Depth 1

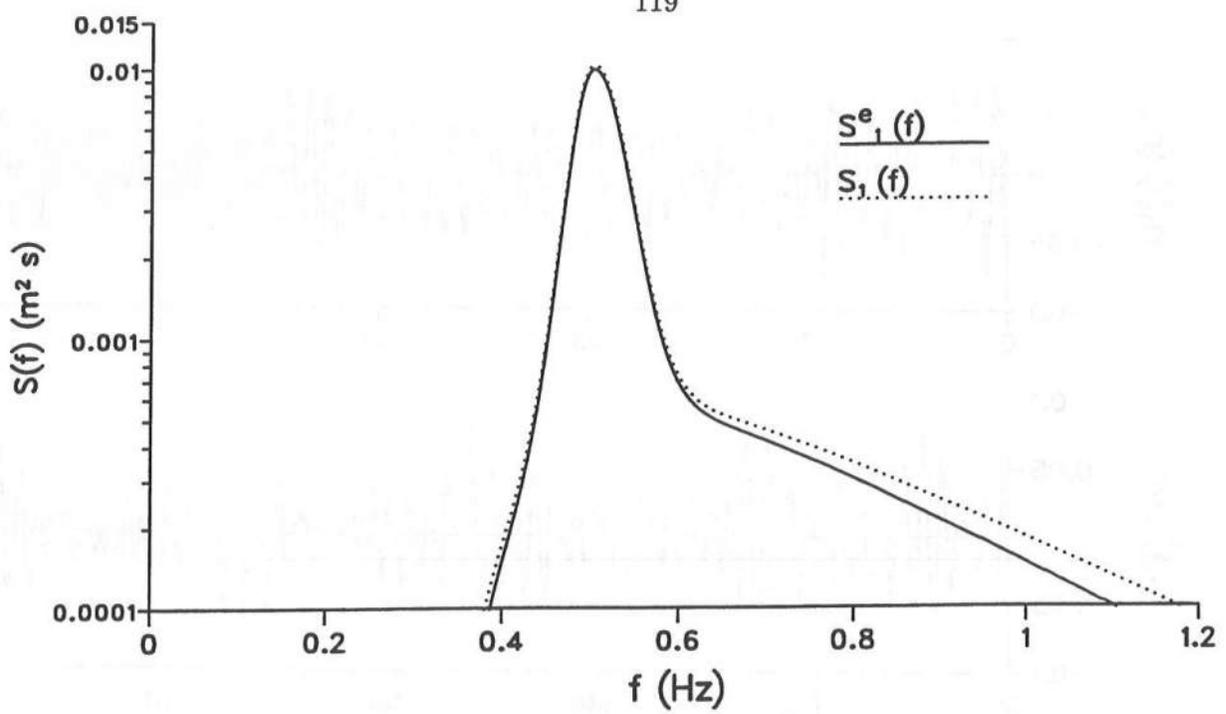


Figure C.3: Equivalent Uni-Directional Frequency Spectrum Versus Incident Frequency Spectrum at Depth 1

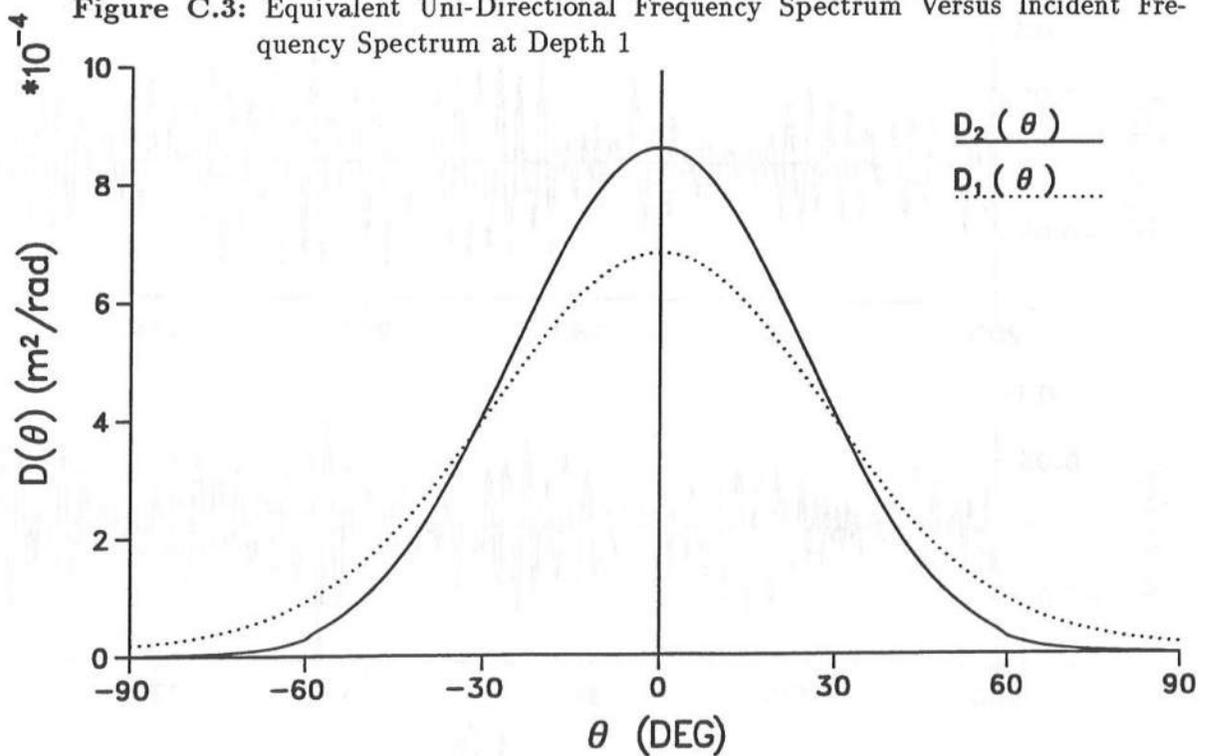


Figure C.4: Energy Distribution Function at Depth 2 Versus Energy Distribution Function at Depth 1

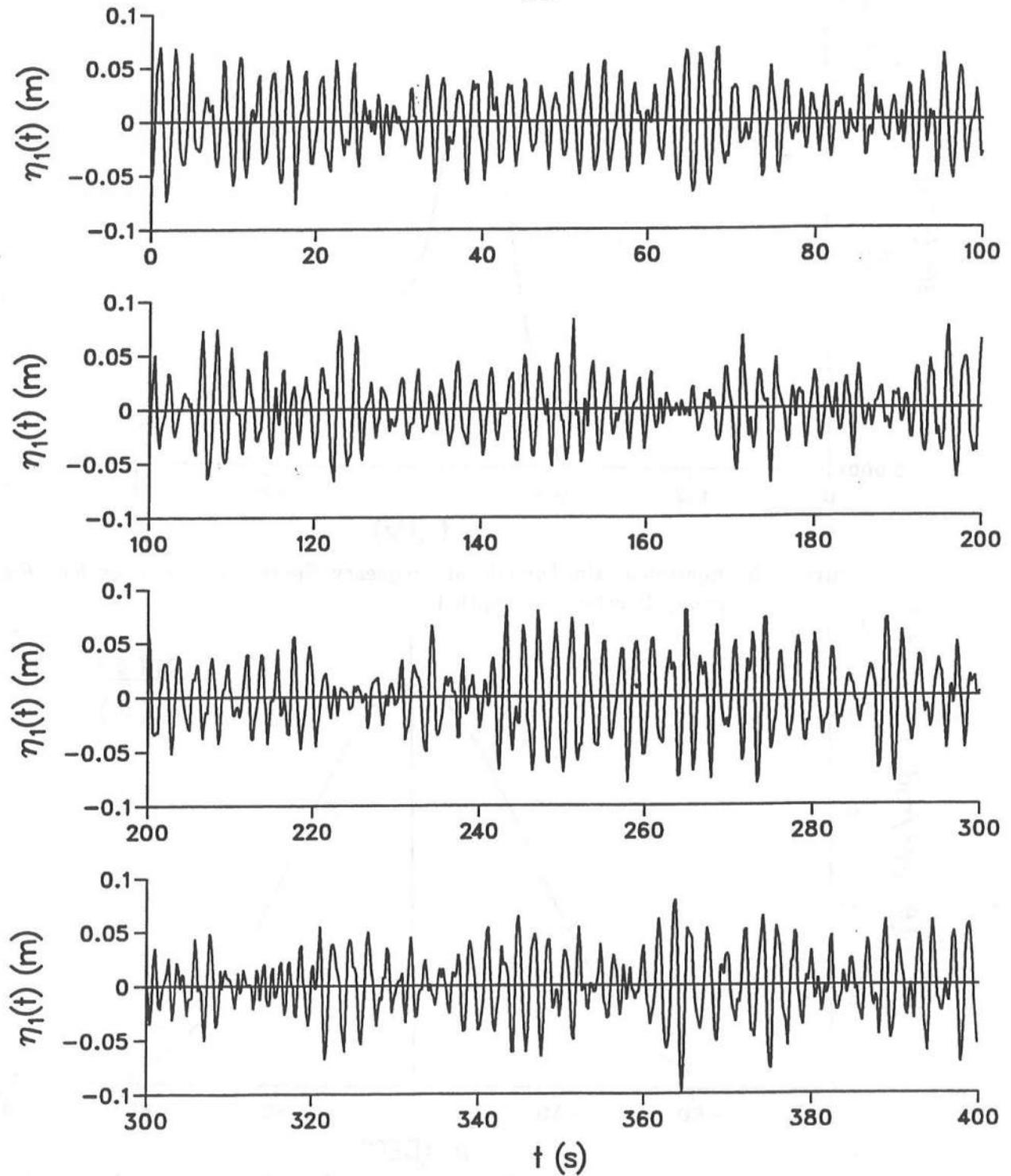


Figure C.5: Time Series Generated From Incident Frequency Spectrum at Depth 1, $\alpha_p = 0^\circ$

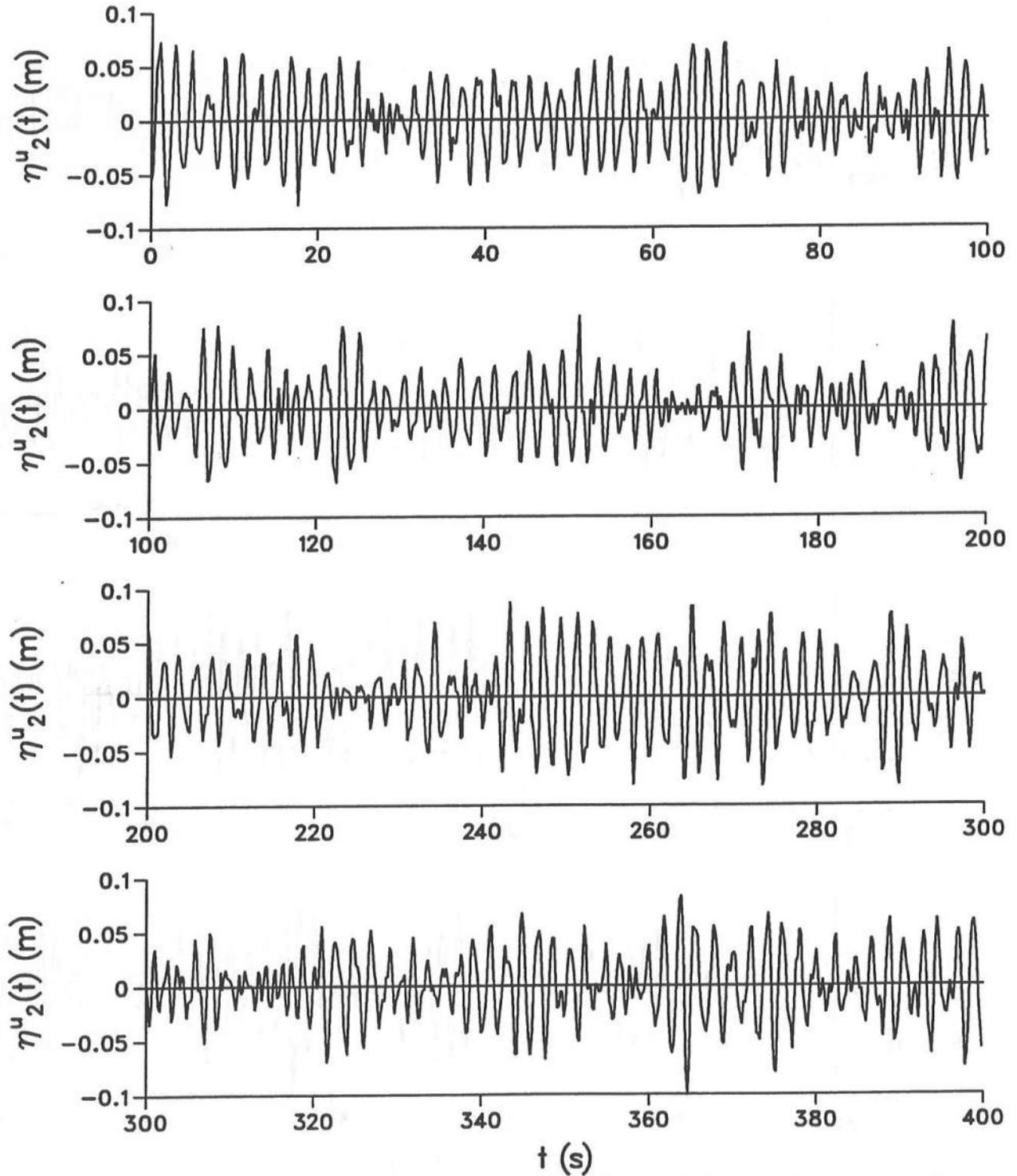


Figure C.6: Time Series Generated From Shoaled Uni-Directional Frequency Spectrum at Depth 2, $\alpha_p = 0^\circ$

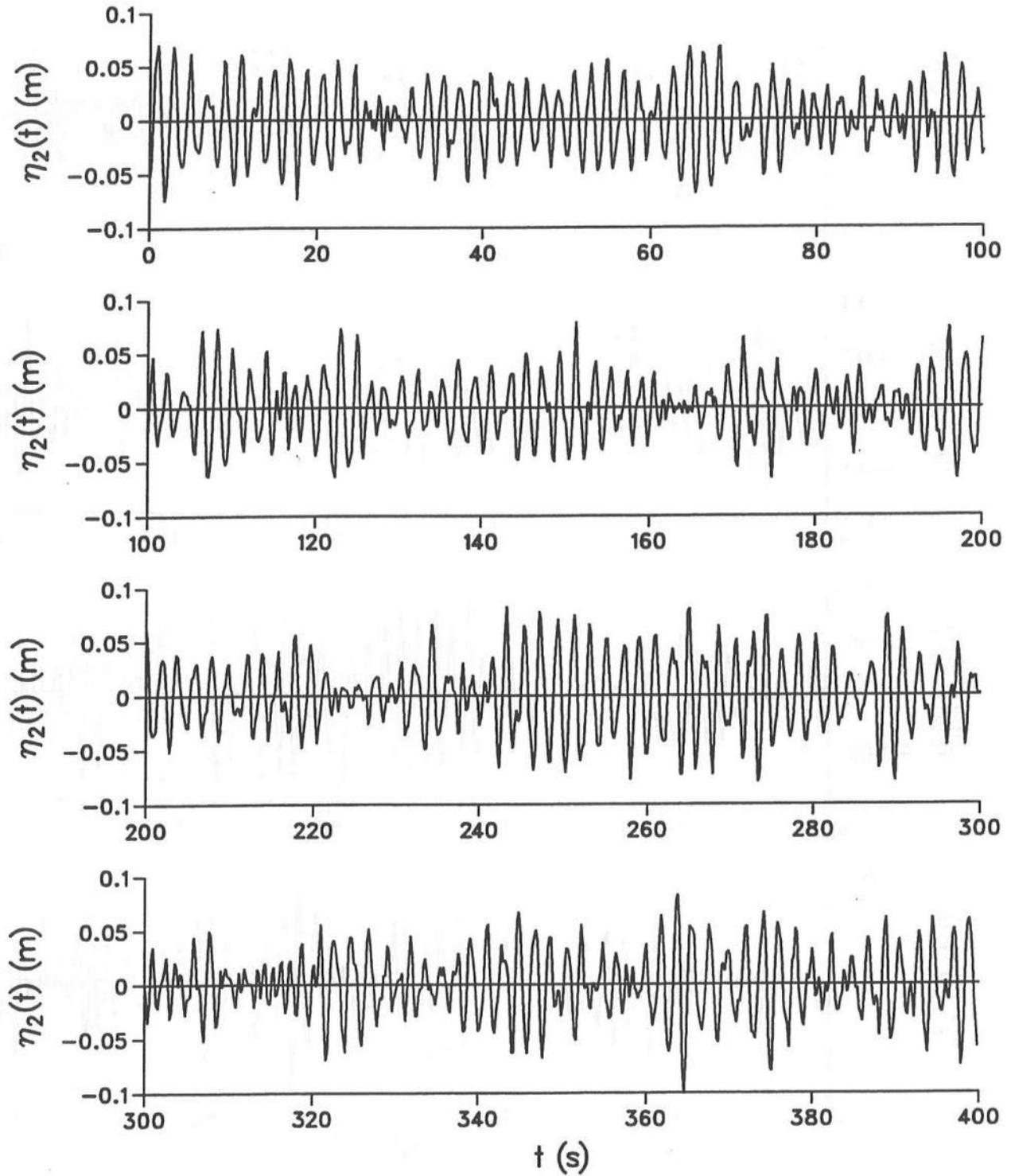


Figure C.7: Time Series Generated From Refracted Frequency Spectrum at Depth 2

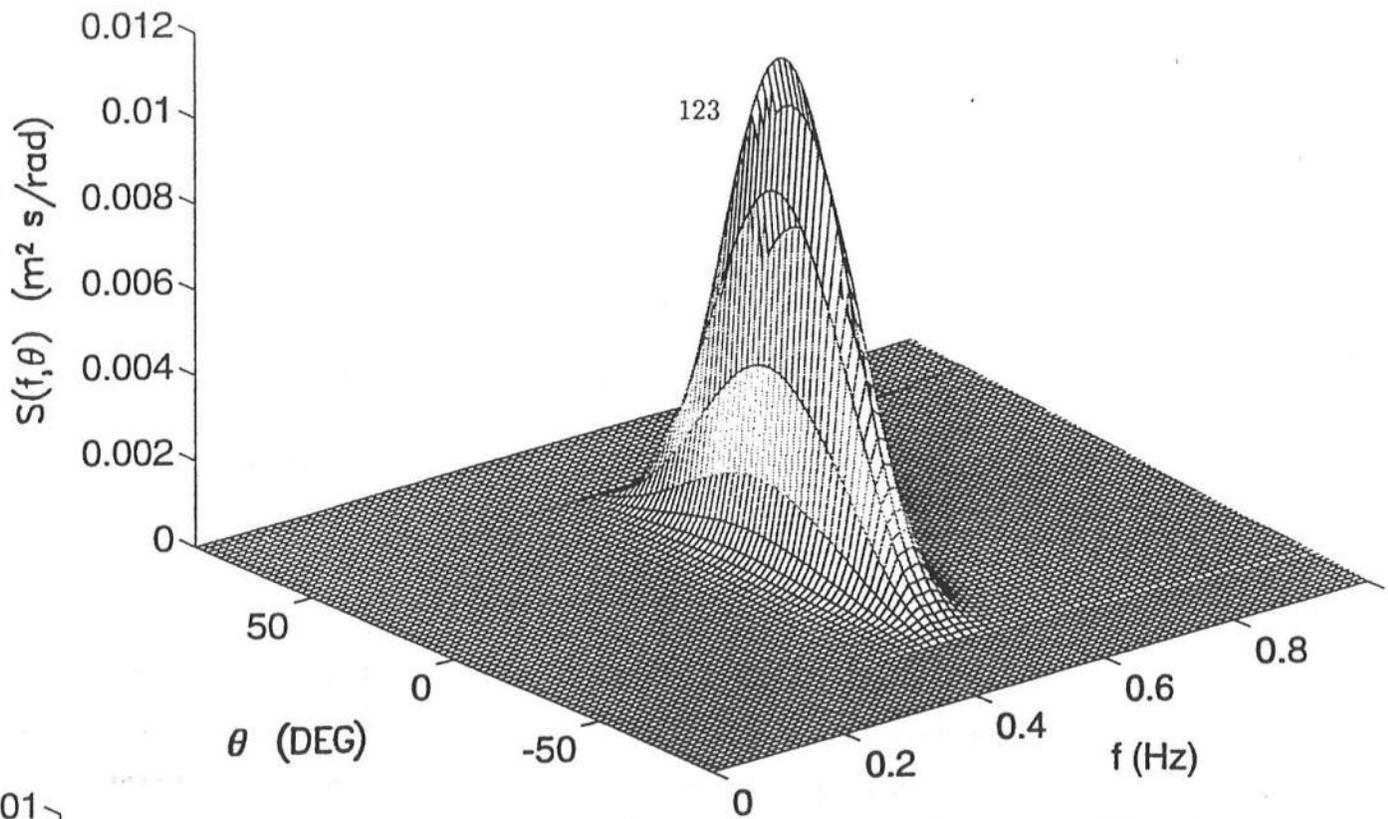


Figure C.8: Directional Spectrum at Depth 2 as a Function of Frequency and Direction

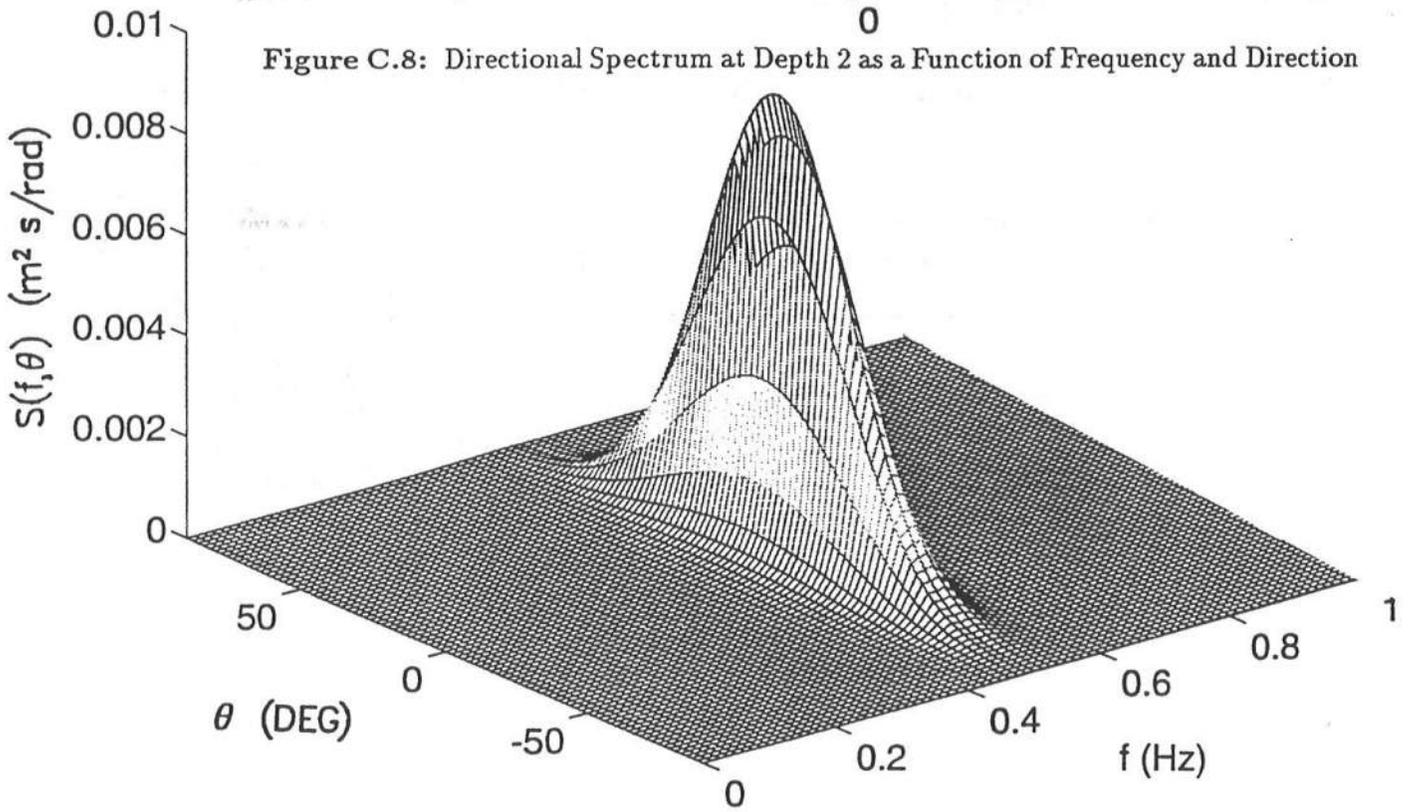


Figure C.9: Directional Spectrum at Depth 1 as a Function of Frequency and Direction

Appendix D

CONTENTS OF ACCOMPANYING DISK

This report is accompanied by a 3.5 inch, IBM-PC-formatted floppy disk containing computer files as listed in Table D.1. The general rule in naming the computer files is as follows: [**.for*] = FORTRAN program and [**.inp*] = the input data file. Also, the approximate computation time for each example is presented.

Table D.1: CONTENTS OF ACCOMPANYING DISK

DIRECTORY	NAME OF FILE ON DISK			REFERENCE
	PROGRAM	INPUT FILES	COMP TIME	
program	reshoal.for			Chapter III & Appendix A
appenb		appenb1.inp	5 min	Appendix B
		appenb2.inp	5 min	Appendix B
appenc		appenc1.inp	5 min	Appendix C